

Learning Objectives

- Separating ions by m/z – basic principles
- Mass analyzers as designed from basic principles
- Types of mass analyzers and their modes of operation
- Guiding, collimating, and focusing ions along a path
- Hybrid instruments including ion mobility-mass spectrometry
- Detectors for mass-analyzed ions
- Vacuum generation for mass spectrometry
- Ability to judge fitness for purpose of commercial instruments

“A modern mass spectrometer is constructed from elements which approach the state-of-the-art in solid-state electronics, vacuum systems, magnet design, precision machining, and computerized data acquisition and processing” [1]. This statement published in 1979 has always been and still is absolutely true in the context of mass spectrometers.

Under the headline of instrumentation we shall mainly discuss the different types of mass analyzers in order to understand their basic principles of operation, their specific properties, and their performance characteristics. The order of treatment in this chapter neither reflects their ever-changing individual predominance in mass spectrometry nor does it follow a strictly historic time line. Rather, an attempt is made to follow a trail of easiest understanding. Of course, this is only one aspect of instrumentation; hence topics such as ion detection and vacuum generation will also be addressed in brief. As a matter of fact, sample introduction is more closely related to particular ionization methods than to the type of mass analyzer employed, and therefore, this issue is treated in the corresponding chapters on ionization methods.

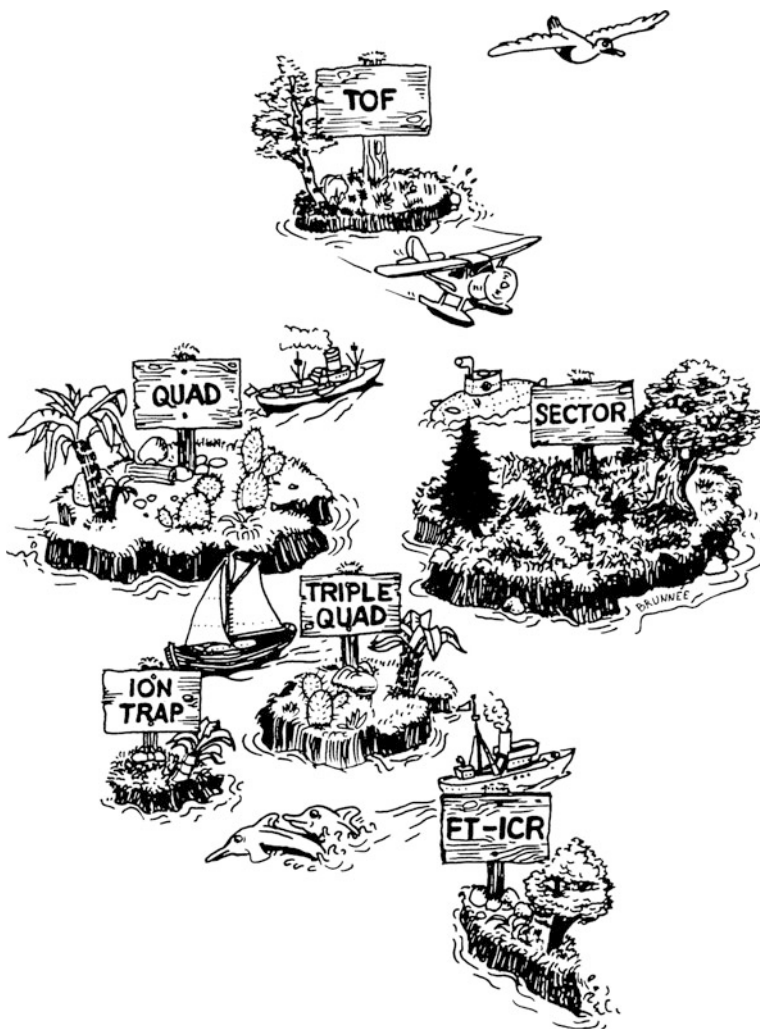


Fig. 4.1 Mass spectrometer islands as presented in a cartoon by C. Brunnée in 1987. The actual situation is quite different, however: much of the cliffs of the sector and quad islands have vanished in the sea while all others have gained new land, and moreover, the Orbitrap island has been given birth in the south east (Reproduced from Ref. [2] with permission. © Elsevier Science, 1987)

From the very beginning to the present almost any physical principle ranging from time-of-flight to cyclotron motion has been employed to construct mass-analyzing devices (Fig. 4.1). Some were extremely successful at the time of their

Table 4.1 Common mass analyzers

Type	Acronym	Principle
Time-of-flight	TOF	Time dispersion of a pulsed ion beam; separation by time-of-flight
Magnetic sector	B	Deflection of a continuous ion beam; separation by momentum in magnetic field due to Lorentz force
Linear quadrupole	Q	Continuous ion beam in linear radio frequency quadrupole field; s due to instability of ion trajectories
Linear quadrupole ion trap	LIT	Continuous ion beam delivers ions for trapping; storage, and eventually separation in linear radio frequency quadrupole field by resonant excitation
Quadrupole ion trap	QIT	Trapped ions; separation in three-dimensional radio frequency quadrupole field by resonant excitation
Fourier transform-ion cyclotron resonance	FT-ICR	Trapped ions in magnetic field (Lorentz force); separation by cyclotron frequency, image current detection and Fourier transformation of a transient signal
Orbitrap	Orbitrap	Axial oscillation in inhomogeneous electric field; detection of frequency after Fourier transformation of a transient signal

invention, for others it took decades until their potential had fully been recognized. The basic types of mass analyzers employed for analytical mass spectrometry are summarized in Table 4.1.

A comparison of Brunnée's cartoon with Table 4.1 reveals that linear ion traps and Orbitraps had not yet been invented at the time of his writing said review. An "updated version" of Brunnée's map was presented 2014 in Geneva at the International Mass Spectrometry Conference (IMSC) during the Brunnée Award lecture by Dimitris Papanastasiou (Fig. 4.2).

The properties of an ideal mass analyzer are well described [2], but despite the tremendous improvements made, still no mass analyzer is perfect. There is a wealth of articles and books that are highly recommended for those seeking a deeper look at the evolution of mass spectrometers [3–13]. In recent years, there has been a growing interest in employing miniature mass analyzers for *in situ* analysis [14, 15], for instance in environmental [16] and biochemical applications [17], for process monitoring, for detection of chemical warfare agents, and for space missions [18, 19]. The most recent completely new type of mass analyzer, the Orbitrap, was introduced in 2005 by Makarov [20].

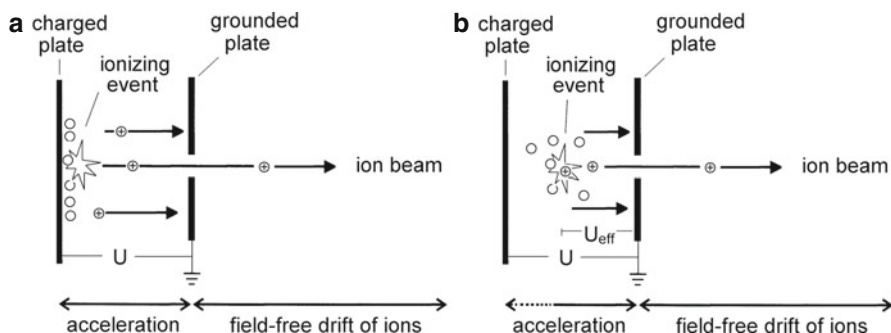


Fig. 4.3 Simple single-stage ion sources. (a) Ionization from a surface or probe where the ionizing event is located on the charged plate; in reality ionizing events in a spatially confined volume above the surface have to be taken into account. (b) Gas phase ionization, where the effective accelerating voltage U_{eff} depends on the actual position of the ion between the plates. After a neutral has been ionized (positive in this illustration), it is attracted by the opposite grounded plate. Those ions passing through a hole of the grounded electrode create an ion beam emerging into the field-free region behind. The ion beam produced by such a primitive ion source is not parallel, but has some angular spread

more successive stages instead of a single one and if ion optical lenses are part of the ion acceleration assembly.

Keep it grounded

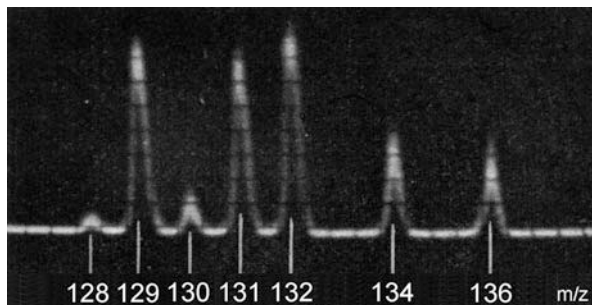
Apart from a few exotic exceptions, all mass spectrometers are – and always have been – constructed in a way to ensure that most parts are electrically grounded. Voltage, especially because this often means high voltage, is only applied to comparatively small parts inside. This ensures safety of operation, and in addition, low capacitive load simplifies rapid DC voltage changes, enables high RF frequencies, and allows for quick polarity switching.

4.2 Time-of-Flight Instruments

4.2.1 Time-of-Flight: Basic Principles

The first *time-of-flight* (TOF) analyzer was constructed and published in 1946 by W. E. Stephens [22]. The principle of TOF is quite simple: ions of different m/z are dispersed in time during their flight along a field-free drift path of known length. Provided all the ions start their journey at the same time or at least within a sufficiently short time interval, the lighter ones will arrive earlier at the detector than the heavier ones. This demands that they emerge from a pulsed ion source

Fig. 4.4 Oscilloscope output of the electron ionization TOF spectrum of xenon on a Bendix TOF-MS. The dark horizontal lines are a grid on the oscilloscopic screen. (For the isotopic pattern of Xe cf. Fig. 3.2.) (Adapted from Ref. [26] with permission. © Pergamon Press, 1959)



which can be realized either by pulsing ion packages out of a continuous beam or more conveniently by employing a true pulsed ionization method.

Soon, other groups embarked on Stephens' concept [23] and increasingly useful TOF instruments were designed and constructed [21, 24, 25] leading to their first commercialization by Bendix in the mid-1950s. These first-generation TOF instruments were designed for gas chromatography-mass spectrometry (GC-MS) coupling [26, 27]. Resolution-wise, their performance was poor as compared to modern TOF analyzers, but the specific advantage of TOFs over magnetic sector instruments was the rate of spectral acquisition, i.e., the number of spectra per second they provided (Fig. 4.4). In GC-MS the TOF analyzer soon became superseded by linear quadrupole analyzers and it was not until the late 1980s that development of TOF analyzers encountered a revival [28, 29] – the success of pulsed ionization methods, especially of matrix-assisted laser desorption/ionization (MALDI), made this possible (Chap. 11). Therefore, we will repeatedly refer to MALDI in our discussion of TOF analyzers.

MALDI generated a great demand for mass analyzers which are suitable to be used in conjunction with a naturally pulsed ion source and capable of transmitting ions of extremely high mass up to several 10^5 u [30]. Since then, the performance of TOF instruments has tremendously increased [31, 32]. TOF analyzers have been adapted for use with other ionization methods and – together with Orbitraps and FT-ICR instruments – have superseded the established magnetic sector instruments in most applications [31, 33].

The main advantages of TOF instruments are:

- In principle, the m/z range of a TOF analyzer is unlimited [34, 35].
- Complete mass spectra are obtained of ions created during a short (nanoseconds) ionizing event, e.g., from a laser shot in LDI or MALDI.
- TOF analyzers offer high ion transmission and thus contribute to high sensitivity.
- The mass spectral acquisition rate of TOFs is very high, essentially $>10^3$ Hz.
- TOF instrument design and construction is comparatively straightforward.
- Modern TOF instruments allow for accurate mass measurements and tandem MS experiments [36].

4.2.2 TOF Instruments: Velocity of Ions and Time-of-Flight

Independent of the ionization method, the electric charge q of an ion of mass m_i is equal to an integer number z of electron charges e , and thus $q = ez$. The energy uptake E_{el} by moving through a voltage U is given by

$$E_{\text{el}} = qU = ezU \quad (4.1)$$

Thereby, the former potential energy of a charged particle in an electric field is converted into kinetic energy E_{kin} , i.e., into translational motion

$$E_{\text{el}} = ezU = \frac{1}{2}m_iv^2 = E_{\text{kin}} \quad (4.2)$$

Assuming that the ion was initially at rest, which holds by first approximation, the velocity attained is calculated by rearranging Eq. (4.2) into

$$v = \sqrt{\frac{2ezU}{m_i}} \quad (4.3)$$

i.e., v is inversely proportional to the square root of mass.

A racing soccer ball The velocity of the [60]fullerene molecular ion, C_{60}^{+} , after acceleration by 19.5 kV is obtained from Eq. (4.3) as

$$v = \sqrt{\frac{2 \cdot 1.6022 \times 10^{-19} \text{C} \times 19,500 \text{V}}{1.1956 \times 10^{-24} \text{kg}}} = 72,294 \text{ m s}^{-1}$$

An ion velocity of $72,294 \text{ m s}^{-1}$ appears rather high, but merely is 0.0024% of the speed of light. The acceleration voltages and thus, the ion velocities are the highest in TOF-MS, although magnetic sector instruments are operated with kilo-electron-volt ion beams, too (Sect. 4.3). The other types of mass analyzers require ions to enter at much lower kinetic energies.

Valid for any mass analyzer

Equation (4.3) describes the velocity of any ion after acceleration in an electric field, and therefore it is valid not only for TOF-MS, but for any part of a mass spectrometer handling beams of ions.

One now can quite easily imagine measuring the time for an ion of unknown m/z in traveling a distance s after being accelerated by a voltage U . The relationship between velocity and time t needed for traveling the distance s is

$$t = \frac{s}{v} \quad (4.4)$$

which upon substitution of v by Eq. (4.3) becomes

$$t = \frac{s}{\sqrt{\frac{2ezU}{m_i}}} \quad (4.5)$$

Equation (4.5) yields the time needed for the ion to travel the distance s at constant velocity, i.e., in a *field-free* environment after the process of acceleration has been completed. Rearrangement of Eq. (4.5) reveals the relationship between the instrumental parameters s and U , the experimental value of t and the ratio m_i/z

$$\frac{m_i}{z} = \frac{2eUt^2}{s^2} \quad (4.6)$$

It is also obvious from Eq. (4.5) that the time to drift through a fixed length of field-free space is proportional to the square root of m_i/z

$$t = \frac{s}{\sqrt{2eU}} \sqrt{\frac{m_i}{z}} \quad (4.7)$$

and thus, the time interval Δt between the arrival times of ions of different m/z is proportional to $s \times ((m_i/z_1)^{1/2} - (m_i/z_2)^{1/2})$.

Mass, not m/z

Here, the ratio m_i/z denotes ion mass [kg] per number of electron charges. The index i at the mass symbol is used to avoid confusion with the *mass-to-charge ratio*, m/z , as used to specify the position of a peak on the abscissa of a mass spectrum (Sect. 1.4.3).

Small differences in time-of-flight According to Eq. (4.7) the C_{60}^{+} ion, m/z 720, dealt with in the preceding example will travel through a field-free flight path of 2.0 m in 27.665 μ s, while it takes slightly longer for its isotopolog $^{13}C^{12}C_{59}^{+}$, m/z 721. The proportionality to the square root of m/z gives (use of m_i/z values yields identical results as the dimension is cancelled):

$$\frac{t_{721}}{t_{720}} = \frac{\sqrt{721}}{\sqrt{720}} = 1.000694$$

Thus, $t_{721} = 27.684 \mu$ s. This corresponds to a difference in time-of-flight of 19 ns under these conditions (cf. Fig. 4.9).

The proportionality of time-of-flight to the square root of m/z causes Δt for a given $\Delta(m/z)$ to decrease with increasing m/z : under otherwise the same conditions Δt per 1 u is calculated as 114 ns at m/z 20, 36 ns at m/z 200, and just 11 ns at m/z 2000. Therefore, the realization of a time-of-flight mass analyzer depends on the ability to measure short time intervals with sufficient accuracy [37–39]. At this point it becomes clear that the performance of the early TOF analyzers – among other reasons – suffered from the low-efficiency electronics of their time. It took until the mid-1990s to overcome this barrier [32].

“Compressed” isotopic patterns of multiply charged ions The time-of-flight of multiply charged ions ($z > 1$) explains the position and appearance of signals caused by ions of higher charge states (Sect. 3.8). As z increases to 2, 3 etc., the numerical value of m/z is reduced by a factor of 2, 3 etc., i.e., the ion will be detected at lower m/z than the corresponding singly charged ion of the same mass. According to Eq. (4.7), the time-of-flight is reduced by a factor of 1.414 (the square root of 2) for doubly charged ions which is the same time-of-flight as for a singly-charged ion of half of its mass. Accordingly, the time-of-flight is reduced by a factor of 1.732 (the square root of 3), for triply charged ions corresponding to a single-charged ion of one third of its mass, and so on for higher charge states.

Inferring the charge state

For multiply charged ions, the m/z scale is compressed by a factor of z equal to the charge state of the ion. Isotopic patterns remain unaffected as far as the relative intensities are concerned. As $\Delta(m/z)$ between isotopic peaks is reduced inversely proportional to z , the charge state can readily be assigned, e.g., doubly charged ions cause isotopic peaks at $\Delta(m/z) = 0.5$, triply charged ions cause them at $\Delta(m/z) = 0.333$, and so on.

4.2.3 Linear Time-of-Flight Analyzer

Restricting its use to laser desorption/ionization (LDI) and matrix-assisted laser desorption/ionization (MALDI, Chap. 11), a simple TOF instrument can be set up as follows (Fig. 4.5): The analyte is supplied as a thin layer on a *sample holder* or *target* upon which a pulsed laser is focused. The acceleration voltage U is applied between this target and a grounded counter electrode. Ions formed and desorbed during the laser pulse are continuously extracted and accelerated as they emerge from the target into the gas phase. When leaving the acceleration region s_0 the ions should possess equal kinetic energies. They drift down a field-free flight path s in the order of 1–2 m and finally hit the detector. Typically, *microchannel plate* (MCP) detectors are employed to compensate for the angular spread of the ion beam (Sect. 4.12). A fast *analog-to-digital converter* (8 bit or 10 bit ADC)

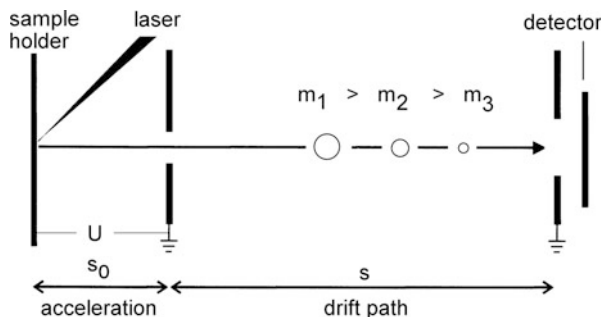


Fig. 4.5 Scheme of a linear TOF instrument designed for use in combination with a laser desorption ion source. Once created during a laser pulse onto the sample layer, ions are continuously accelerated by a voltage U . While drifting along the field-free drift path s , they are dispersed in time. Lighter ions reach the detector first

transforms the analog output of the detector for computer-based data storage and data processing. Such an instrumental setup where the ions are traveling on a straight line from the point of their creation to the detector is called *linear TOF*.

In principle, any other ionization method can be combined with a TOF analyzer even if it is not an intrinsically pulsed technique, provided there are means to extract ions in a pulsed manner from such an ion source (Sect. 4.2.6).

The drift time t_d as calculated by means of Eq. (4.7) is not fully identical to the total time-of-flight. Obviously, the time needed for acceleration of the ions t_a has to be added. Furthermore, a short period of time t_0 may be attributed to the laser pulse width and the process of desorption/ionization, which is typically in the order of a few nanoseconds. Thus, the total time-of-flight t_{total} is given by

$$t_{\text{total}} = t_0 + t_a + t_d \quad (4.8)$$

A rigorous mathematical treatment of the TOF analyzers as needed for the construction of such instruments of course has to include all contributions to the total time-of-flight [32, 36–38, 40–42].

The transmittance of a linear TOF analyzer approaches 90% because ion losses are solely caused by collisional scattering due to residual gas or by poor spatial focusing of the ion source. With a sufficiently large detector surface located at a short distance from the ion source exit, a very high fraction of the ions will be collected by the detector.

Even metastable decompositions during the flight do not reduce the intensity of a molecular ion signal, because the fragments formed conserve the velocity of the fragmenting ion and are therefore detected simultaneously with their intact precursors. In such a case, the ionic *and* the neutral fragment cause a response at the detector. These properties make the linear TOF analyzer the ideal device for analyzing easily fragmenting and/or high-mass analytes [43].

Detection of neutrals

In linear TOF analyzers, neutrals formed by metastable fragmentation also give rise to a signal. This is because they impinge on the detector after having travelled down the flight tube side-by-side with the ionic product of ion dissociation. As a result, nonfragmenting intact precursor ions plus both ionic and neutral products of the metastable dissociation of precursor ions will hit the detector simultaneously. Therefore, linear TOF analyzers are best suited for the analysis of large and labile molecules, e.g., oligonucleotides (Sect. 11.5). This presents a rare case where neutrals contribute to a useful signal in mass spectrometry.

The example in Sect. 4.2.2 demonstrates that the differences in time-of-flight of ions differing by 1 u in mass are in the order of about 10 ns at about m/z 1000. The time elapsing during desorption/ionization is roughly 10–50 ns in case of standard UV lasers, but can be longer with IR lasers. Consequently, the variation in starting times for ions of the same m/z value is often larger than the difference in time-of-flight of neighboring m/z values, thereby limiting the resolution.

4.2.4 Better Vacuum Improves Resolving Power

The mass resolution of a TOF analyzer is directly proportional to its total flight path length [44]. Improved vacuum conditions result in an elongated mean free path for the ions and thus reduce the risk of collisions in transit through the analyzer. The resolving power of a TOF analyzer clearly depends on the background pressure [45]. Despite improvements of resolving power in the order of a factor of two can be realized (Fig. 4.6), enhanced pumping systems alone are not able to effect a breakthrough in resolving power.

Only QITs use buffer gas

The quadrupole ion trap (Sect. 4.5) is the only type of mass analyzer that uses buffer gas to damp ion trajectories. All other mass analyzers require the highest possible vacuum for optimum performance.

4.2.5 Energy Spread of Laser-Desorbed Ions

Laser-desorbed ions possess comparatively large initial kinetic energies of some 10 eV that are superimposed on the kinetic energy provided by the acceleration voltage, which is typically in the order of 10–30 kV. Obviously, higher acceleration

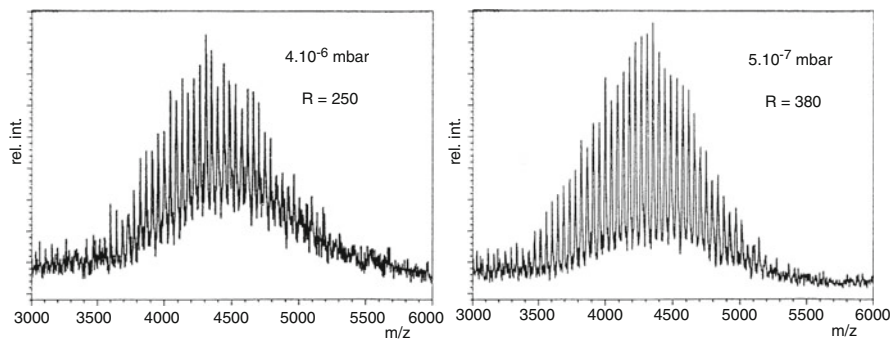


Fig. 4.6 Dependence of resolution on analyzer pressure: linear MALDI-TOF spectra of polyethylene glycol 4000 recorded at a pressure of 4×10^{-4} Pa (*left*) and 5×10^{-5} Pa (*right*) (Adapted from Ref. [45] with permission. © John Wiley & Sons, 1994)

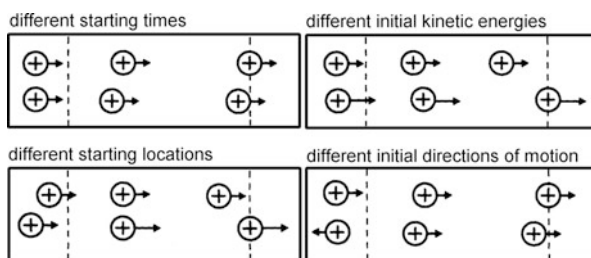


Fig. 4.7 Effects of initial time, space, and kinetic energy distributions on mass resolution in TOF-MS (Adapted from Ref. [39] with permission. © American Chemical Society, 1992)

voltages are advantageous in that they diminish the relative contribution of the energy distribution caused by the ionization process. Figure 4.7 illustrates the possible effects of deviations from the assumption that ions initially are at rest on an equipotential surface [39]. All these effects together limit resolution to $R \approx 500$ for continuous extraction linear TOF analyzers.

Bothersome energy spread

The spread in ion kinetic energies from thermal energy as well as from inhomogeneous acceleration presents a general problem in the construction of mass analyzers. Accordingly, there are numerous approaches to narrow down the kinetic energy distributions of ions or to compensate for their effects.

4.2.6 Reflector Time-of-Flight Analyzer

The *reflector* or *reflectron* was devised by Mamyryn in 1994 [46]. In the reflector TOF analyzer – often abbreviated *ReTOF* – the reflector acts as an ion mirror that focuses ions of different kinetic energies in time. Its performance is improved by using two-stage or even multistage reflector designs.

Commonly, reflector instruments are also equipped with a detector behind the reflector allowing linear mode operation simply by switching off the reflector voltage. A complete mathematical treatment of single-stage and two-stage reflectors is found in the literature [36–38, 42]. Here, we will restrict ourselves to a qualitative explanation of the reflector.

A simple reflector consists of a retarding electric field located behind the field-free drift region opposed to the ion source. In practice, a reflector is comprised of a series of ring-shaped electrodes at increasing potential. The reflection voltage U_r is set to about 1.05–1.10 times the acceleration voltage U in order to ensure that all ions are reflected within the homogeneous portion of the electric field of the device

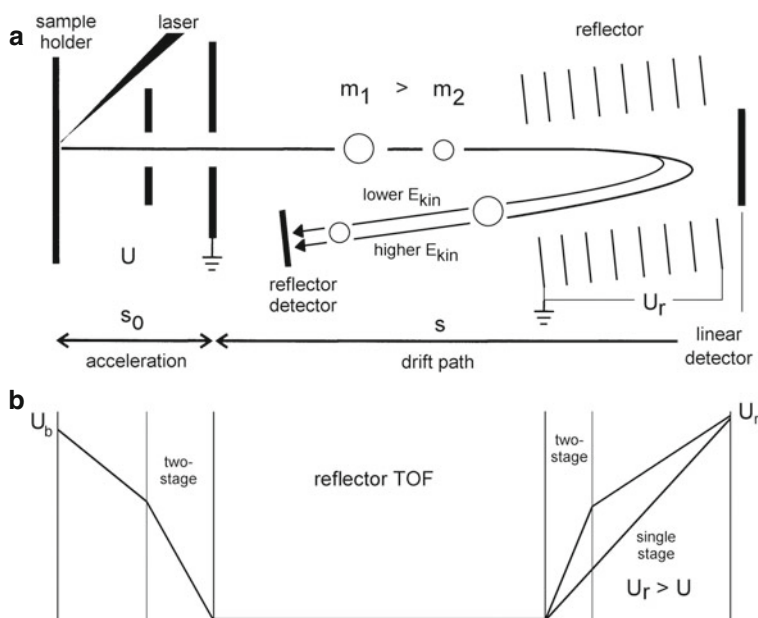


Fig. 4.8 ReTOF analyzer. (a) Principle of operation, (b) potentials along the instrument. Ions of different kinetic energy penetrate the reflector to different depths before they come to a halt and get ejected into the opposite direction. Faster ions have to travel a longer path than slower ones, and thus, time focus is achieved at some point on the return path. There, the detector receives ions of the same mass at (about) the same time. A small angle between the axis of the flight path and the reflector allows the detector to be placed beside the ion source

(Fig. 4.8). The ions penetrate the reflectron until they reach zero kinetic energy and are then expelled from the reflector in opposite direction. The kinetic energy of the leaving ions remains unaffected, however their flight paths vary according to their differences in kinetic energy. Ions carrying more kinetic energy will fly deeper into the decelerating field, and thus spend more time within the reflector than less energetic ions. Thereby, the reflector achieves a correction in time-of-flight that substantially improves the resolving power of the TOF analyzer [32, 37–39]. In addition, the reflector provides (imperfect) focusing with respect to angular spread of the ions leaving the source and it corrects for their spatial distribution [37, 46]. Adjusting the reflector at a small angle with respect to the ions exiting from the source allows the reflector–detector to be placed adjacent to the ion source (Mamyrin design). Alternatively, a detector with a central hole to transmit the ions leaving the ion source has to be used in *coaxial reflectrons* (cf. Sect. 9.5).

Although the reflector elongates the flight path and hence the dispersion in time-of-flight, this effect is of lower importance than its capability to compensate for initial energy spread. Simple elongation of the flight path can also be achieved with longer flight tubes in linear instruments. However, too long flight paths may even decrease the overall performance of TOF analyzers due to loss of ions by angular spread of the ion beam and scattering of ions after collisions with residual gas.

Nonetheless, the remarkable improvements of resolving power delivered by TOF analyzers with their very long flight paths have more recently led to the development of TOF analyzers with folded ion paths and sophisticated ion optics (Sect. 4.2.11).

The ability of the ReTOF to compensate for the initial energy spread of ions largely increases the resolving power of TOF instruments. While a typical continuous extraction TOF instrument in linear mode cannot resolve isotopic patterns of analytes above about m/z 500, it will do when operated in reflector mode (Fig. 4.9). At substantially higher m/z , the ReTOF still fails to resolve isotopic patterns, even though its resolution is still better than that of a linear TOF analyzer.

Metastable ions in a ReTOF

In case of metastable fragmentations, ReTOF analyzers behave differently from linear TOF analyzers. If fragmentation occurs between ion source and reflector, the ions will be lost by the reflector due to their change in kinetic energy. Transmission occurs only for fragments still having kinetic energies close to that of the precursor due to the energy tolerance of the reflector, as, for instance, $[M + H - NH_3]^+$ in case of a peptide of about m/z 2000. However, such ions are not detected at correct m/z , thereby giving rise to a “tailing” of the signal. Ions fragmenting in transit from reflector to detector are treated the same way as ions in the linear TOF. Thus, the elongated flight path of the ReTOF analyzer also allows more time for fragmentation. This can complicate the detection of very labile analytes in reflector mode.

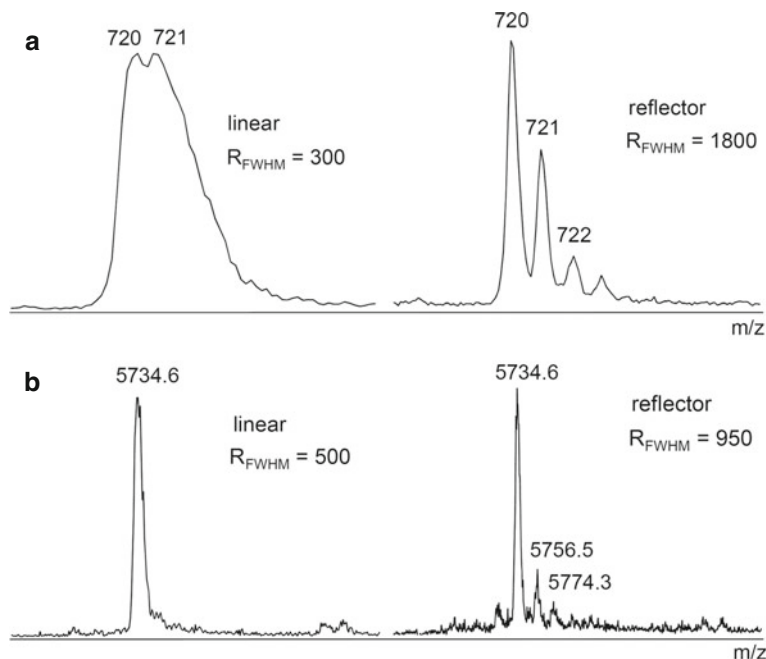


Fig. 4.9 C_{60} molecular ion signal of at m/z 720 (a) and the $[M + H]^+$ ion signal of bovine insulin, m/z 5734.6 (b), as obtained on a TOF instrument in linear mode (left) and reflector mode (right). All other experimental parameters remained unchanged

4.2.7 Delay Before Extraction to Improve Resolving Power

In MALDI-TOF-MS, the energy spread of the emerging ions is of significant magnitude as a result of the MALDI process, which in addition, creates a temporal distribution of ion formation. The most successful approach of handling such conditions is presented by ion sources allowing a delay between generation and extraction/acceleration of the ions. *Time-lag focusing* dates back to 1955 [21] and since then has been adapted to the needs of MALDI-TOF-MS by several groups [47–50].

The advantage of pulsed acceleration is its capability to focus the ions in time thereby reducing the effect of initial position and initial velocity on resolution. In addition, the delay permits the plume generated upon laser irradiation to disperse while still in a field-free region prior to acceleration. This avoids collisions of energetic ions with neutrals in the initially dense plume that could broaden the translational energy distribution and cause fragmentation due to CID (Sect. 9.3). Continuous extraction MALDI ion sources had to be operated with laser fluences

close to the threshold for ion formation in order not to sacrifice the limited resolution any further. With pulsed acceleration, this effect is greatly reduced.

After allowing the ions to separate in space according to their different initial velocities during a delay of some hundreds of nanoseconds the acceleration voltage is switched on with a fast pulse. This procedure also ensures that laser-induced reactions have terminated before ion acceleration begins. A delay of about 200 ns was empirically found to be required to realize the desired effect [36, 42].

Longer delays allow to achieve very high resolving power at the focused mass, but outside the optimized m/z range resolution remains limited. More recently, the so-called *panoramic pulsed ion extraction* (PAN) was introduced (Bruker Daltonik) that makes use of a time-modulated extraction pulse to stretch the optimum resolution over a wide m/z range.

Many names

Unfortunately, establishing patents and trademarks has caused redundant names for almost the same thing: *time lag focusing* (TLF, Micromass); *delayed extraction* (DE, Applied Biosystems); *pulsed ion extraction* (PIE), and more recently *panoramic pulsed ion extraction* (PAN, Bruker Daltonik).

Using a two-stage acceleration ion source allows the electric field between target (repeller) and extraction plate P_1 to be varied. The remaining fraction of the acceleration voltage is applied in the second stage. At the onset of extraction, ions with high initial velocities have traveled farther than slower ones, and therefore experience only a fraction of the extraction voltage dV between target and extraction plate P_1 . The voltage of the second stage is the same for all ions. As a result, the fastest ions receive less energy from the accelerating field than the slowest. Thereby, such ion sources compensate for the initial energy distribution [50].

The optimum settings of the delay time and of the ratio of pulsed to fixed voltage (V_1/V_2) depend on m/z with a tendency towards longer delays and/or a larger V_1/V_2 ratio for heavier ions. In practice, the variation of potentials in pulsed ion extraction with time can be handled as follows (Fig. 4.10): target and extraction plate P_1 are maintained at the same potential during the delay time, thereby creating a field-free region d_1 . After the delay has passed, P_1 switches from V_1 by a variable value dV to V_2 causing extraction of the ions.

Impressive gain in resolving power Regardless of the manufacturer of the hardware, the effect of a time lag on resolution is quite dramatic. The resolving power of linear instruments is improved by a factor of 3–4 and reflector instruments become better by a factor of about 2–3 [50]. The advantages are obvious by comparison of MALDI-TOF spectra of substance P, a low mass peptide, as obtained in continuous extraction mode and after PIE upgrade of the same instrument (Fig. 4.11). Modern mid-class MALDI-TOF instruments easily deliver twice that resolution.

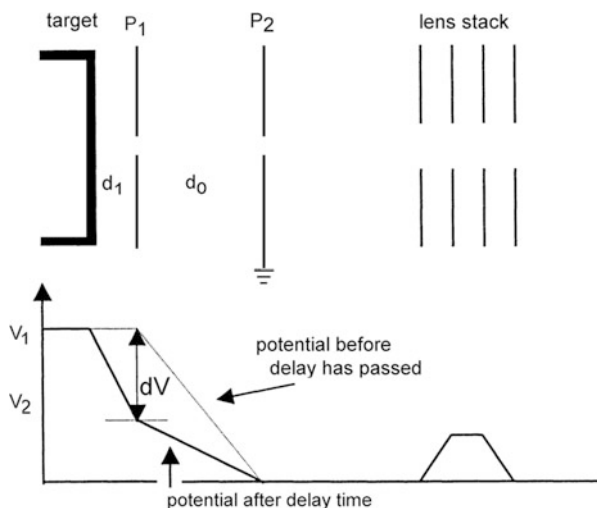


Fig. 4.10 Variation of potentials in pulsed ion extraction with time. The lens stack acts as angular focusing device for the ion beam (By courtesy of Bruker Daltonik, Bremen)

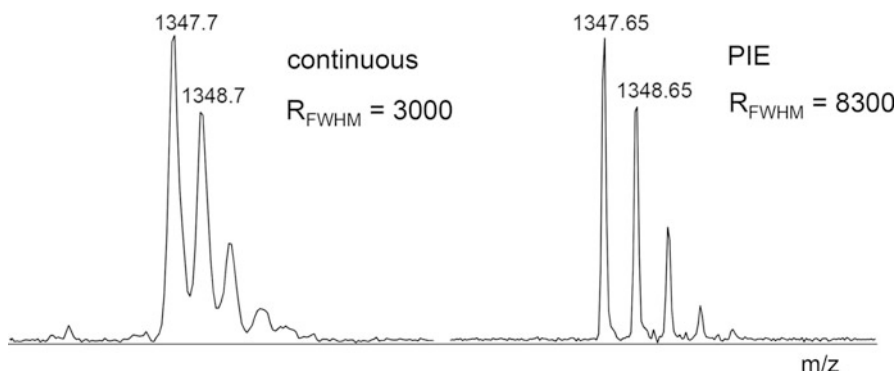


Fig. 4.11 MALDI-TOF spectra of substance P, a low-mass peptide, as obtained from a Bruker Biflex ReTOF in continuous extraction reflector mode (in 1995, *left*) and after PIE upgrade of this instrument (in 2001, *right*)

4.2.8 Orthogonal Acceleration TOF Analyzers

Up to here, the TOF analyzer has been under consideration bearing MALDI-TOF equipment in mind, just because MALDI as a pulsed ionization method delivers ions to a TOF analyzer in an ideal manner. In fact, MALDI initiated such tremendous improvements of TOF analyzers that it became attractive to combine these compact but powerful analyzers with other, inherently nonpulsed, ionization methods. The major breakthrough for generalized use of TOF analyzers arose from the design of the *orthogonal acceleration* TOF analyzer (oaTOF). In an

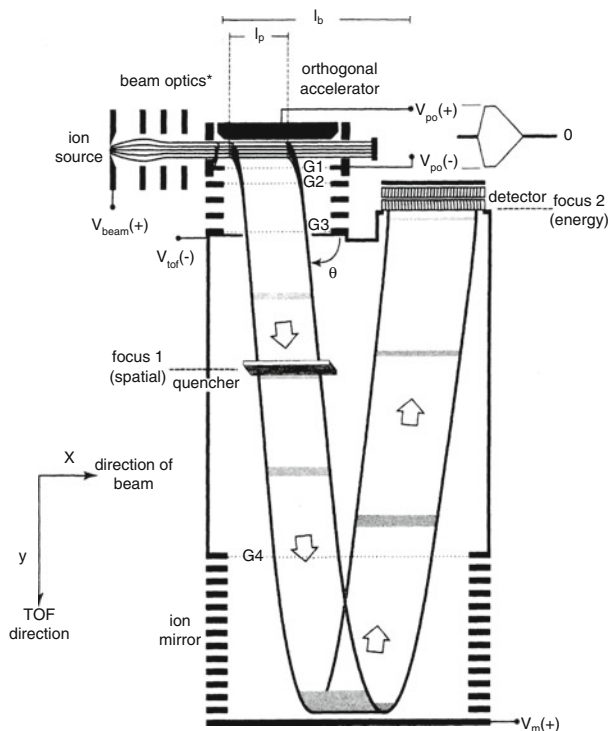


Fig. 4.12 An orthogonal acceleration reflector TOF instrument. See text for discussion (Reproduced from Ref. [55] by permission. © John Wiley & Sons, 2000)

oaTOF analyzer, pulses of ions are extracted orthogonally from a continuous ion beam (Fig. 4.12) [51, 52]. The oaTOF analyzer can be of linear or ReTOF type. Although different problems have to be overcome for each ionization method, the oaTOF analyzer is in principle suited for any of them [29, 53–55].

The main advantages of oaTOF analyzers are:

- High sensitivity due to good duty cycle and high transmission of TOF analyzers.
- High spectral acquisition rate (spectra per second) even after pre-averaging.
- High mass-resolving power.
- Mass accuracies as good as 1 ppm for formula determination.
- Compact design and small footprint.

Therefore, it is not astonishing that oaTOF instruments are currently widespread in use for numerous kinds of applications. Electrospray ionization (ESI) oaTOF instruments with accurate mass capabilities represent the majority of these systems [56–58], but gas chromatography–mass spectrometry (GC-MS) instruments are

also available. In particular for *fast GC* applications [59, 60] and for HR-GC-MS [61] oaTOF systems are advantageous. Today, a large portion of the instruments incorporating oaTOF analyzers are hybrids mostly of the quadrupole-oaTOF type. We will therefore deal with them in the section on hybrid instruments.

4.2.9 Operation of the oaTOF Analyzer

Ions leaving the ion source are focused to form an almost parallel ion beam, i.e., to minimize ion motion orthogonal to the ion beam axis. Then, the ion beam enters the orthogonal accelerator (x -axis) [29, 53, 55]. The ion kinetic energy in this beam is only in the range of 10–20 eV. A package of ions of length l_p is pushed out orthogonally from its initial direction by a sharp pulse, and is thus accelerated into the TOF analyzer (y -axis) by a voltage of 5–10 kV. From the TOF analyzer's point of view the orthogonal acceleration unit can be regarded as the ion source. Usually, ions are accelerated through a two-stage setup analogous to the Wiley-McLaren ion source [21].

The design of the TOF analyzer itself is similar to those discussed before, but its diameter is much wider because the velocity of the ions in x -direction, v_{beam} , is not affected by the orthogonal push-out process. Therefore, the detector needs to be comparatively wide in x -direction to enable ions extracted anywhere from the whole path l_p to hit its surface. In practice, the detector needs to be several centimeters in length. The angle θ between the x -direction and the flight axis into the TOF analyzer is given by

$$\theta = \tan^{-1} \sqrt{\frac{-V_{\text{tof}}}{V_{\text{beam}}}} = \tan^{-1} \left(\frac{v_{\text{tof}}}{v_{\text{beam}}} \right) \quad (4.9)$$

where V_{tof} and V_{beam} are the acceleration voltages for ion beam and orthogonal accelerator, respectively, and v_{tof} and v_{beam} are the corresponding ion velocities.

While one ion package travels through the TOF analyzer and is being dispersed in time, the accelerator is refilled with new ions from the ion source (the time-of-flight to cover an m/z range up to about 5000 by the oaTOF is about 100 μs). During the drift time of an ion through the oaTOF, it travels a distance l_b . The ratio of the length of the orthogonal accelerator l_p to l_b , determines the efficiency of the mass analyzer in terms of the ratio of ions used to ions created. This efficiency is known as the *duty cycle* of an instrument (next paragraph). The duty cycle of an oaTOF instrument is at an optimum if the time-of-flight to pass the TOF analyzer is slightly longer than the time needed for the continuous ion beam to refill the orthogonal accelerator. As soon as the heaviest ions have reached the detector, the next package is pulsed into the analyzer, giving rise to 10,000 complete mass spectra per second. In order to reduce the amount of data and to improve the signal-to-noise

ratio, summation of several single spectra is done by an acquisition processing unit before the spectra are passed to a computer for data storage and post-processing.

4.2.10 Duty Cycle

In mass spectrometry the term *duty cycle* is used to specify the fraction of time of an ion current as continuously delivered from an ion source that is finally used for mass analysis. The duty cycle of scanning instruments is intrinsically low as only ions of one m/z value hit the detector at a time while all others are discarded by the analyzer, e.g., at $R = 1000$ only a fraction of 10^{-3} of the m/z range reaches the detector corresponding to a duty cycle of just 10^{-3} . Linear and ReTOF analyzers, on the other side, are capable of using almost all ions that are created from a pulsed ionizing event, and thus, these allow duty cycles in the order of 0.9. Although the oaTOF analyzer is by far better than scanning devices, it has to deal with a batch operation of the ion pulser. Fast (low-mass) ions traverse the orthogonal accelerator in a shorter time span than slow (high-mass) ions, thereby causing discrimination of low-mass ions. This behavior poses limitations on the mass range that can be simultaneously pulsed into the TOF analyzer. Depending on the axial velocity distribution of the ions and on the m/z range to be analyzed, the duty cycle of oaTOF analyzers is in the 3–30% range.

Determination of the duty cycle In oaTOF operation, the frequency between acceleration pulses is selected as to avoid spectral overlap due to mixing of subsequent ion packages traveling along the TOF analyzer. The slowest ions arrive at the detector at a time that is determined by the ratio of the length of the ion entrance window, l_p , to the distance between the midpoints of this window and the detector, l_b . The duty cycle (Du) for the heaviest ion at m/z_{\max} is therefore given by $Du = l_p / l_b$, (Fig. 4.12) [62]. Furthermore, as the velocity of ions is proportional $(m/z)^{-2}$ (Eq. 4.3) the duty cycle for low-mass ions at m/z_{low} is given by

$$Du = \frac{l_p}{l_b} \sqrt{\frac{m/z_{\text{low}}}{m/z_{\max}}} \quad (4.10)$$

In practice, the ratio l_p / l_b is about 0.25, and thus, for $m/z_{\text{low}} = 100$ and $m/z_{\max} = 2000$ we obtain $Du = 0.056$ for the low-mass ion.

Nonetheless, it is not the duty cycle alone that defines the transmission of oaTOF analyzers. Actually, the overall sensitivity of instruments is also influenced by ion losses during entrance into the orthogonal accelerator, divergence of ions prior to pulsing, eventual grids in the flight path, etc.

4.2.11 TOF Analyzers with a Folded Eight-Shaped Flight Path

It should have become clear that elongated flight paths could provide an effective means of increasing the resolving power of a TOF analyzer if it were not for the ion losses due to spreading of the beam by Coulombic repulsion and by scattering of ions upon collision with residual gas. Apart from these considerations, a flight tube of say 10 m in length would be impracticable for any commercial instrument. On the next few pages we will therefore take a – hopefully instructive – view of some extraordinary TOF analyzer designs to get a perspective on what can be done.

Folding the flight path into compact dimensions presents an elegant concept to build a TOF analyzer featuring a very long flight path. An approach by M. Toyoda makes use of four electrostatic sectors that enable eight-shaped ion optical geometries for multi-turn and multi-passage ion paths [44]. While electrostatic sectors enable curved ion paths, they still cannot provide angular focusing of the ion beam to a level required for multiple passages through the analyzer. Therefore, additional ion optical elements such as electrostatic lenses and/or DC quadrupoles are incorporated, leading to a rather complex ion optical system. Additionally, ion injection from an external ion source into this “race track” has to be incorporated into the design if the final instrument is intended to be of practical use.

One representative of this TOF geometry is the MULTUM Linear plus instrument [44, 63], which consists of four cylindrical electrostatic sectors and 28 DC quadrupole lenses. The setup of this TOF analyzer is shown in Fig. 4.13 and the corresponding ion trajectories as visualized by a computer simulation are depicted in Fig. 4.14. The ions are injected at moderate kinetic energy of 1.5 keV and one cycle, a “full eight”, corresponds to 1.284 m. Thus, the analyzer fits into a suitcase-sized housing ($60 \times 70 \times 20$ cm).

Outstanding resolving power The mass resolving power of the MULTUM Linear plus instrument increases as more repetitive cycles are employed. This has been demonstrated for the doublet of CO^{++} and N_2^{++} ions at m/z 28 (Fig. 4.15). It is remarkable that the time interval to the neighboring peak increases while the peak width in the spectra corresponding to 25.5, 101.5, 301.5, and 501.5 cycles or about 33, 130, 387, and 644 m path length, respectively, remains almost constant at 8 ± 1 ns. Finally, a mass resolution of $R_{\text{FWHM}} = 350,000$ is achieved after 501.5 cycles equaling a flight path of 644 m and a flight time of 6.3 ms.

It is an inherent weakness of this design that the next injection of ions has to wait until the preceding ion package has completed its journey through the TOF analyzer. Otherwise, fast ions of the following ion injection could overtake the slower ones of the previous one. The design does, however, not permit to distinguish this sort of interference, and thus, suffers from very low duty cycle as it takes several milliseconds to complete a single run. The m/z range per analysis is also limited due

Fig. 4.13 Complex but compact ion optical design of the MULTUM Linear plus TOF analyzer. The eight-shaped path is realized by electrostatic sectors and numerous DC quadrupole lenses (SQ , Q , and CQ) (Reproduced from Ref. [63] by permission. © IM Publications, 2010)

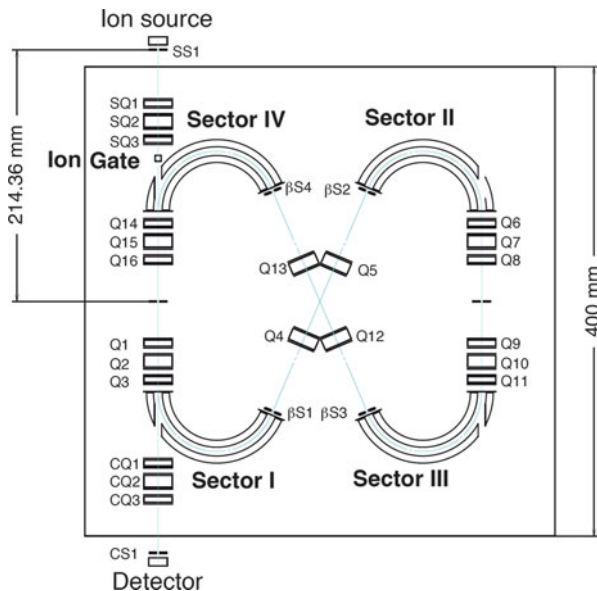


Fig. 4.14 Simulated ion trajectories in the MULTUM Linear plus (cf. Fig. 4.13). The arrows indicate the direction of ion motion (Adapted from Ref. [44] by permission. © John Wiley & Sons, 2003)

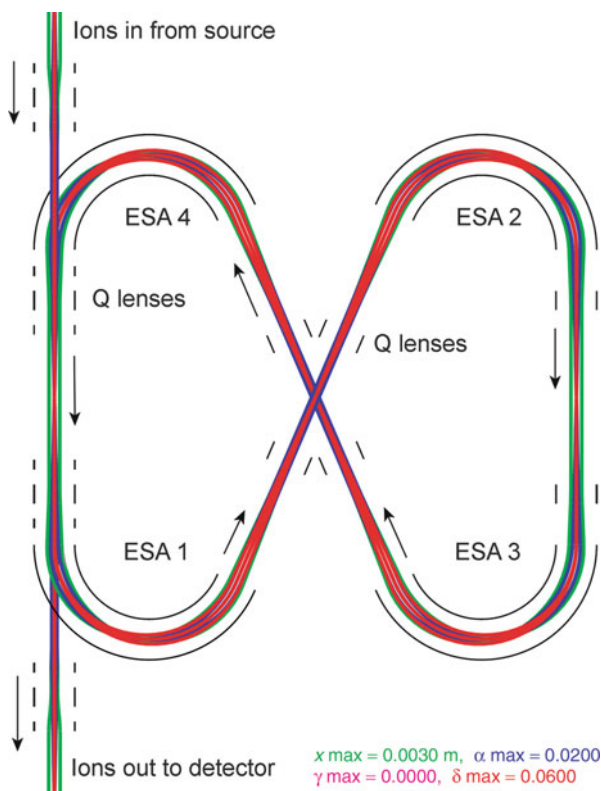
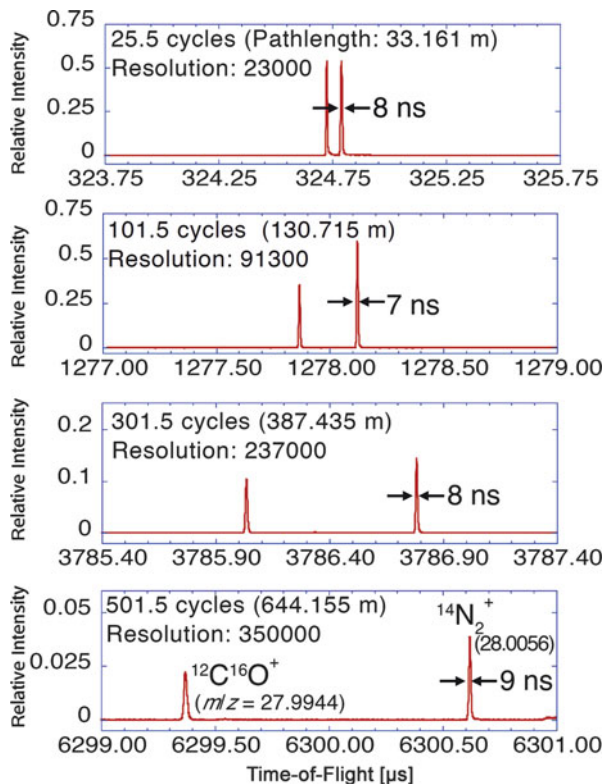


Fig. 4.15 Gain of resolution upon increasing ion flight path through the MULTUM Linear plus as demonstrated for the doublet of $\text{CO}^{+\bullet}$ and $\text{N}_2^{+\bullet}$ at m/z 28. From top to bottom the spectra correspond to 25.5, 101.5, 301.5, and 501.5 cycles or about 33, 130, 387, and 644 m path length, respectively (Reproduced from Ref. [63] by permission. © IM Publications, 2010)

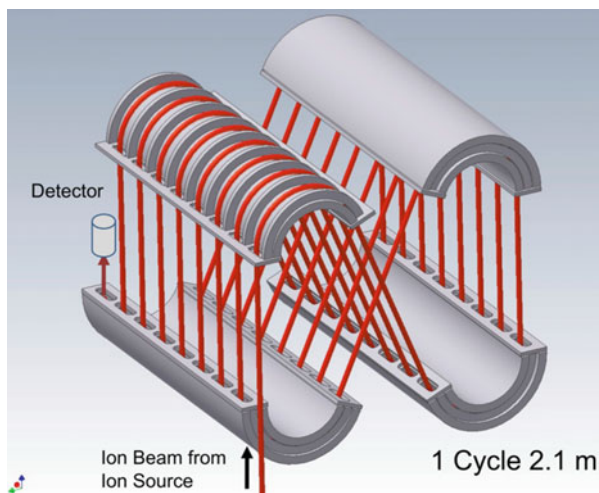


to this phenomenon: lighter ions would overtake the heavier ones after some cycles. In other words, only ions traveling the same number of cycles can be reliably analyzed.

Space mission From the commercial point of view, this unconventional yet impressive design still possesses some prototype character. Nonetheless, it has seen an application on the ROSETTA space mission. In fact, the lander Philae carried a miniature instrument of this design for the COSAC project [64, 65]. The lander was dropped on the surface of the comet 67P/Churyumov-Gerasimenko on November 12, 2014 after a 10-year journey of some seven billion kilometers. After some difficulties due to an unlucky touch down, it finally managed to acquire a mass spectrum on the comet's surface [66].

The problems of indistinguishable ion packages and of overtaking lighter ions can be resolved by tilting the axis of ion injection out of the x,y plane to introduce a translational motion in z direction. This way, ions are moving through a stack of eight-shaped paths. While the number of cycles is then defined by the analyzer hardware, the design allows to cover a large m/z range as required in analytical mass spectrometry [67–69].

Fig. 4.16 SpiralTOF analyzer using four arrays of electrostatic analyzers (*gray*). The outer electrode of the top left ESA has been omitted. The ion flight path is visualized as a *red line* (Reproduced with permission from Ref. [71] © Mass Spectrometry Society of Japan, 2014)



JEOL has developed a MALDI-TOF instrument incorporating the so-called “SpiralTOF” analyzer. The geometry comprises eight loops of 2.1 m each resulting in a total flight path of about 17 m (Fig. 4.16). While not actually flat, the entire analyzer fits into a compact almost cubic housing. As the ion source uses delayed extraction (Sect. 4.2.7) to minimize the translational energy spread of the ions prior to entering the SpiralTOF assembly, this instrument can deliver 80,000 resolving power [70–72]. An application of this instrument to MALDI analysis of a synthetic polymer is shown in Sect. 11.5.

4.2.12 Multi-reflecting TOFs

Alternatively, TOF analyzers can be compacted by folding the flight path via multiple reflection of the ions. The concept of multi-pass and multi-reflecting TOF analyzers has been explored by H. Wollnik [73, 74]. Following the line of thought that leads from the MULTUM design to the SpiralTOF, it appears logical to employ an array of reflectors and some tilt of the direction of motion to avoid overtaking of lighter ions. Rather than using the same pair of reflectors to oscillate ion packages back and forth as many times as possible, such a multi-reflector design with a defined number of cycles offers free selection of the m/z range to be covered. The setup that has finally been commercialized employs an array of multi-stage reflectors that are aligned in a way as to effect a “zig-zag” or “jig-saw” ion path [75]. To avoid ion loss by scattering, a set of electrostatic lenses is positioned halfway between the opposed reflectors. It requires carefully tuned spatial focusing of both reflector stages and lenses to keep ions on track along such a flight path.

Ions leaving the source are injected into the first reflector at an angle and then pass a switchable deflector electrode. With the deflector electrode switched on, ions are sent into the second reflector stage and leave from there to hit the detector after

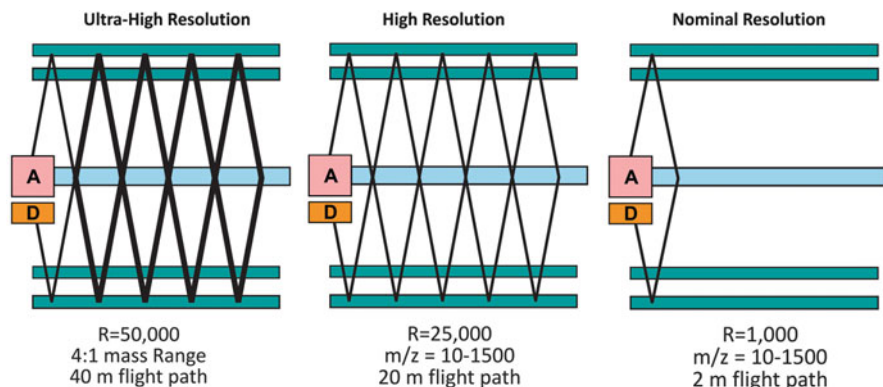


Fig. 4.17 Scheme of multi-reflecting TOF operational modes (A ion source, D detector). By using a switchable deflector ions can either be passed through one double reflection to deliver $R = 1000$, to five double reflection to achieve $R = 25,000$, or even to have a second full passage enabling $R = 50,000$ (Courtesy of LECO, Germany)

having gone through a rhombic flight path of just 2 m (Fig. 4.17). In this mode, the instrument can deliver $R = 1000$. When no potential is applied to the deflector, ions move on to start their zig-zag journey until they are reflected at the end of the array to send them back on a path leading to the detector. Providing a flight path of 20 m, this mode delivers $R = 25,000$. By using the deflector to send ions back, the ions are going for second passage through the mass analyzer to enable $R = 50,000$ after 40 m of flight. The latter mode limits the m/z range to a ratio of 1:4, e.g., m/z 200–800, because ions of the first and second passage are simultaneously traveling on the track.

A better idea of the dimensions of this compact analyzer and of the penetration depth of the multi-stage reflectors is conveyed by Fig. 4.18. This multi-reflecting TOF analyzer is commercialized by LECO as Pegasus HRT series of instruments [76, 77].

Multi-reflecting TOF at CERN At CERN, the online precision mass spectrometer ISOLTRAP uses a dedicated multi-reflecting TOF analyzer between the linear RF ion trap and two Penning traps for precision mass measurement of exotic nuclei [78]. The MR-TOF analyzer comprises two ion-optical mirrors between which oscillating ions are separated according to their different mass-to-charge ratios. By the multiple reflections, the analyzer of less than 1 m in length allows for total ion flight paths of several hundreds of meters. Tests of an offline version of this device delivered a resolving power of up to $R = 80,000$ [79]. As part of the highly specialized setup of ISOLTRAP at CERN, the MR-TOF serves for purification of contaminated ion beams. Furthermore, the MR-TOF can be operated as a mass spectrometer on its own, in particular for precision mass measurements of nuclides that are shorter-lived or that have lower yields than those accessible for Penning trap mass spectrometry [78–80].

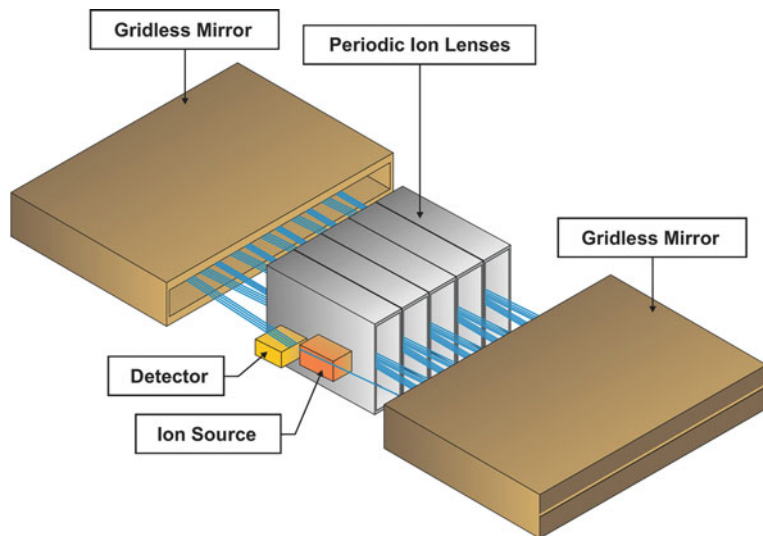


Fig. 4.18 Schematic of the multi-reflecting TOF analyzer. During the most part of their journey, ions are traveling either within reflectors or are passing electrostatic lenses (Courtesy of LECO, Germany)

4.2.13 Essence of TOF Instruments

Principle of Operation

Ions of equal kinetic energy but different in mass are moving at different velocities. When such ions are traveling down a field-free drift path of given length, their flight times depend on mass, more precisely on the square root of m/z . Measuring the time-of-flight (TOF) allows to calculate the ionic mass. The mass resolving power of a TOF analyzer is proportional to its length.

TOF Configurations

The simplest form of a TOF analyzer is presented by the linear TOF with continuous ion extraction from the source. The reflector TOF (ReTOF) design offers 2–4-fold improved resolving power that can be further boosted by implementation of a delay between ion creation and onset of ion acceleration. Typically, such TOF analyzers, generally of reflector design, are attached on-axis to MALDI sources featuring some sort of pulsed ion extraction.

Continuous ion sources can be used in combination with orthogonal-acceleration (oaTOF) analyzers. For m/z analysis in oaTOFs, ions are deflected from an ion beam orthogonal to its direction. Commonly, the TOF analyzer of these instruments is also of reflector design. Furthermore, oaTOFs are well-suited for combination with other mass-analyzing devices.

Performance Characteristics

The performance of TOF analyzers in terms of mass range, resolving power, and mass accuracy varies widely in accordance with their design (on-axis TOF versus oaTOF), mode of operation (linear or reflector mode), and intended use (MALDI versus ESI, APCI versus EI, CI) of the instrument. Thus, TOFs may cover ranges of up to m/z 1000 (GC-MS), to m/z 5000 (ESI, APCI sources), and even to far beyond m/z 100,000 (MALDI). TOFs can deliver resolving power of $R = 1000$ (GC-MS, GC \times GC-MS) to $R > 30,000$. Accordingly, mass accuracies range from just 0.2 u to 0.001 u.

TOF Analyzers in the Laboratory

TOF analyzers are widely used in modern instrumentation. Their success is based on a balance between performance in terms of resolving power, mass accuracy, mass range, speed, and sensitivity on the one side and of reasonable investment on the other. Their compact footprint in the laboratory and moderate power consumption also contribute to their success. On-axis TOF and oaTOF analyzers make up the majority of today's TOF instrumentation, while the more complex folded ion path layouts are less common.

4.3 Magnetic Sector Instruments

4.3.1 Evolution of Magnetic Sector Instruments

Magnetic sector instruments paved the road to organic mass spectrometry. "Whereas mass spectrometry was still very an art rather than a science in 1940, the picture changed drastically during the war years. Vacuum and electronic techniques had matured" [81]. It took until the 1950s for magnetic sector instruments to become commercially available [7, 8]. These pioneering instruments were fairly bulky and not very easy to use [81–83]. Nevertheless, they provided analytical information of a kind that chemists had long been seeking for. They continuously became faster, more accurate, with higher resolving power [3, 5, 9, 84]. The first instruments used a single magnetic sector (symbol B) to effect separation of the ions. Later, the introduction of *double-focusing instruments* which in addition were equipped with an *electrostatic sector* or *electrostatic analyzer* (ESA, symbol E) in addition defined a standard which is still valid. With few exceptions, magnetic sector instruments are comparatively large devices capable of high resolution and accurate mass determination, and suited for a wide variety of ionization methods.

Trends in instrumentation

Two decades ago, double-focusing sector instruments were commonly used with a large chemical diversity of samples. Within the last decade, however, there has been a strong tendency to replace sector instruments with TOF, Orbitrap, or FT-ICR instruments, and moreover, to even substitute classical ionization methods such as EI, CI, or FAB with APCI or ESI just to redirect the stream of samples to those preferable modern mass analyzers. Recently, manufacturers have “rediscovered” the utility of EI and CI and started to offer TOF and Orbitrap analyzers adapted to these ionization methods. These instruments often are dedicated to gas chromatography-mass spectrometry (GC-MS), but direct insertion probes are also having a renaissance (Sect. 5.2).

4.3.2 Principle of the Magnetic Sector

The *Lorentz Force Law* can be used to describe the effects exerted onto a charged particle entering a constant magnetic field. The Lorentz force F_L depends on the velocity v , the magnetic field B , and the charge q of an ion. In the simplest form the force is given by the scalar equation [3, 4, 85, 86]

$$F_L = qvB \quad (4.11)$$

which is valid if v and B (both are vectors) are perpendicular to each other. Otherwise, the relationship becomes

$$F_L = qvB (\sin \alpha) \quad (4.11a)$$

where α is the angle between v and B . Figure 4.19 demonstrates the relationship between the direction of the magnetic field, the direction of the ionic motion, and the direction of the resulting Lorentz force. Each of them is at right angles to the others. An ion of mass m and charge q traveling at a velocity v in a direction perpendicular to an homogeneous magnetic field will follow a circular path of radius r_m that fulfills the condition of equilibrium of F_L and centripetal force F_c

$$F_L = qvB = \frac{m_i v^2}{r_m} = F_c \quad (4.12)$$

Upon rearrangement we obtain the radius r_m of this circular motion

$$r_m = \frac{m_i v}{qB} \quad (4.13)$$

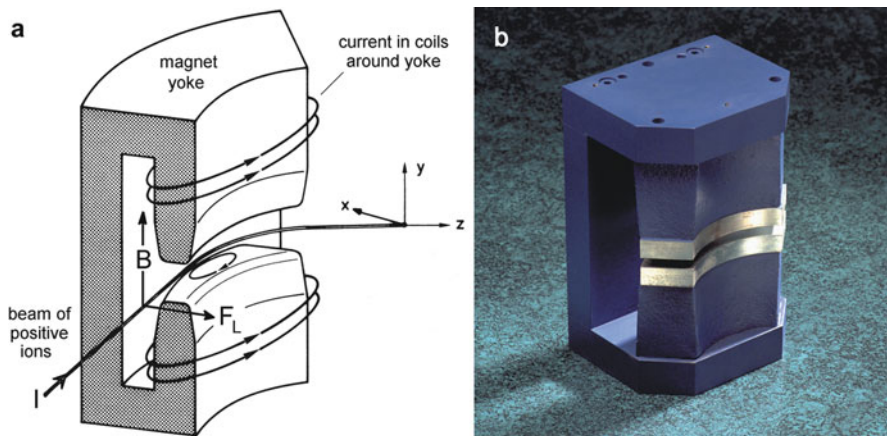


Fig. 4.19 The Right Hand Rule (I thumb, B index finger, F_L middle finger) to determine the direction of the Lorentz force (a), where the current corresponds to the direction where positive charges move, i.e., the figure directly applies for positive ions. (b) A real magnet yoke without coils and flight tube. With kind permission of Thermo Electron (Bremen) GmbH, (left) and Waters Corporation, MS Technologies, Manchester, UK (right)

This shows the working principle of a magnetic sector where the radius r_m depends on the momentum $m\nu$ of an ion, which itself depends on m/z .

Momentum analyzer

The magnetic sector does not directly separate ions by mass. Rather it effects ion separation by their momentum and this feature can be used as a measure of mass provided all ions possess equal kinetic energy.

Finally, dispersion in momentum causes a dependence of r_m on the square root of mass becoming obvious by substitution of ν from Eq. (4.3) and $q = ez$

$$r_m = \frac{m_i}{ezB} \sqrt{\frac{2ezU}{m_i}} = \frac{1}{B} \sqrt{\frac{2m_i U}{ez}} \quad (4.13a)$$

Alternatively, the ratio m_i/q can be expressed by rearranging Eq. (4.13)

$$\frac{m_i}{q} = \frac{r_m B}{\nu} \quad (4.14)$$

which upon substitution of ν as performed above becomes

$$\frac{m_i}{q} = \frac{r_m B}{\sqrt{\frac{2qU}{m_i}}} \Rightarrow \frac{m_i}{q} = \frac{r_m^2 B^2}{2U} \quad (4.14a)$$

For singly charged ions ($z = 1, q = e$) we obtain the more widespread form

$$\frac{m_i}{e} = \frac{r_m^2 B^2}{2U} \quad (4.14b)$$

Basic equation of MS

Equation (4.14b) has become known as the *basic equation of mass spectrometry*. Nowadays, there is no more justification for a single basic equation of mass spectrometry because of the large variety of mass analyzers employed.

4.3.3 Focusing Action of the Magnetic Field

The focusing action of an homogeneous magnetic field on a beam of ions having the same m/z and the same kinetic energy can best be illustrated by a 180° sector (Fig. 4.20). If the beam is divergent by a half-angle α , the collector slit must be $\alpha^2 r_m$ wide to pass all ions after suffering 180° deflection. This is because the ions come to a first order, i.e., imperfect, focus as they all traverse the magnetic field at the same radius but not all of them entered the field at right angles. Ions of different m/z fly at a different radius, e.g., the lighter ions of m/z_1 hit the wall while ions of m/z_2 reach the collector slit. To allow for detection of various masses, such an analyzer could either be equipped with a photographic plate in the focal plane to become a so-called *mass spectrograph*, or it could be designed with variable magnetic field to detect different masses at the same point by bringing them subsequently to the collector slit. Indeed, such a 180° geometry with *scanning* magnetic field has been used by Dempster [87]. Later, the term *mass spectrometer* was coined for this type of instruments [83].

Among other complications, the 180° design requires large and heavy magnetic sectors. It is by far more elegant to employ magnetic sectors of smaller angles (Fig. 4.21). An optimized magnetic sector alone can provide a resolving power of $R = 2000\text{--}5000$ depending on its radius. The limitation arises from the fact that ions emerging from the ion source are not really monoenergetic. This way, ions of different m/z can have equal momentum and thus cause overlap of adjacent ion beams at the detector.

Energy spread limits resolving power Equation (4.13a) describes the radius r_m in the magnetic field. Obviously, the value r_m remains constant as long as $m_i U = \text{const.}$ If the instrument is set to pass an ion of say m/z 500 and 3000 eV kinetic energy, it

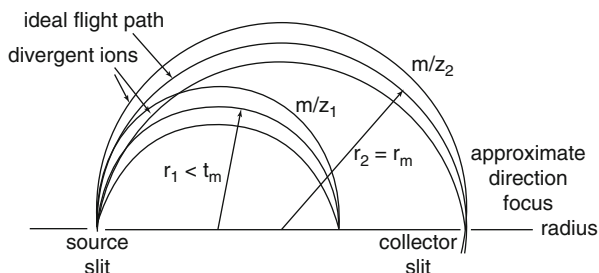


Fig. 4.20 Direction focusing properties of a 180° magnetic sector on a diverging beam of ions of the same m/z and the same kinetic energy and effect on ions of different m/z . In this illustration, B has to come out of the plane towards the reader for positive ions

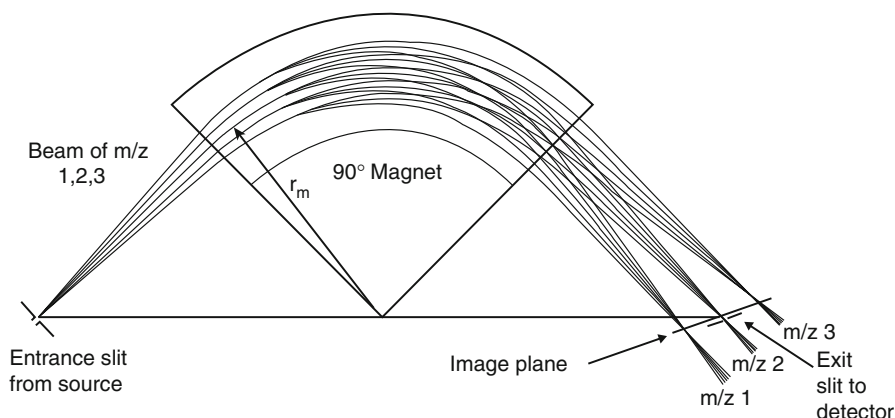


Fig. 4.21 Ion separation and direction focusing in a plane by a 90° magnetic sector. A divergent beam of ions of m/z 1, 2, 3 is separated into three beams and focused to a point on the image plane (divergence shown exaggerated). Only ions of m/z 2 are passing the exit slit and eventually hit the detector (Adapted from Ref. [88] with permission. © Wiley-VCH, 1999–2014)

will simultaneously allow the passage for ions of m/z 501 having 2994 eV or of m/z 499 having 3006 eV of kinetic energy. This is why high resolving power demands narrow kinetic energy distributions.

4.3.4 Double-Focusing Sector Instruments

The *electrostatic sector* or *electrostatic analyzer* (ESA) produces a radial electric field between two oppositely charged plates extending over the ESA angle ϕ (Fig. 4.23). An ion passes the ESA midway on a circular path if

$$F_e = qE = \frac{m_i v^2}{r_e} = F_c \quad (4.15)$$

where F_e represents the electric force, E the electric field strength, and r_e the radius of the ESA. Rearrangement of Eq. (4.15) demonstrates that the ESA acts as an energy dispersive device

$$r_e = \frac{m_i v^2}{qE} = \frac{m_i v^2}{ezE} \quad (4.16)$$

Energy filter

The ESA effects energy dispersion. Thus, the kinetic energy distribution of an ion beam can be reduced. The ESA does not allow for mass separation among monoenergetic ions.

Upon substitution of Eq. (4.3) for v one obtains the simple relationship

$$r_e = \frac{2U}{E} \quad (4.17)$$

to describe the radius of the ESA. As with the magnetic sector before, the ESA has direction-focusing properties in one plane (Fig. 4.22). Ions entering the ESA in the middle and at right angles to the field boundaries pass through on a path of equipotential, whereas ions with a velocity component towards one of the capacitor

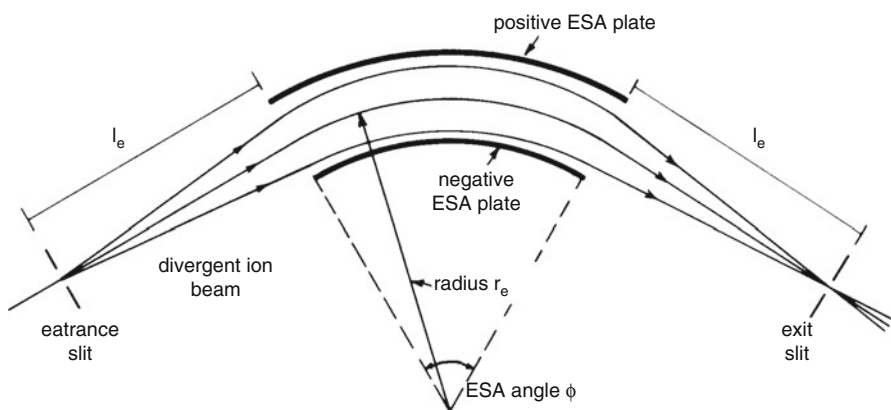


Fig. 4.22 Direction focusing of a radial electric field. Ions of appropriate kinetic energy are focused at the exit slit. Divergent ions pass the ESA close to either plate. Here, the electric potentials are set to transmit positive ions. The image distance l_e depends on the ESA angle

plates are brought into focus at the focal length l_e . To understand this, imagine an ion drifting towards the outer plate having the same charge sign as the ion. As it approaches the plate it is decelerated by the opposed electric field and finally reflected towards the center of the beam. With its radial component of v inverted it crosses the ideal path at l_e . In an analogous fashion an ion approaching the inner plate becomes accelerated by the attractive force. The resulting higher velocity causes an increase in centripetal force, and thereby effects a correction of the flight path in the appropriate sense.

Energy focusing is achieved by combining a magnetic sector and an electric sector in a way that the energy dispersion of the magnetic field is just compensated by the energy dispersion of the electric field. Additional direction focusing is obtained if the radii and angles of these fields and their mutual alignment does not diminish the focusing properties of each of them. Then, an ion optical system is obtained that is able to focus ions onto a single image point, although these were emerging from the ion source in (slightly) different directions and with (slightly) different kinetic energies. This is called *double focusing*. Double focusing can improve the resolving power of a magnetic sector instrument more than ten times.

4.3.5 Geometries of Double-Focusing Sector Instruments

The following passages present examples of particular double-focusing geometries that either have been milestones in instrument design [3, 5] or still are incorporated in modern mass spectrometers.

The EB design by Mattauch and Herzog combines a $31^\circ 50'$ ESA with a 90° magnetic sector producing an image plane that allows for simultaneous photographic detection of a comparatively large m/z range [89]. This mass spectrograph attains double-focusing over the total image plane resulting in resolving powers of $R > 10,000$. Thus, it became the basis for numerous commercial instruments (Fig. 4.23). The *Mattauch-Herzog geometry* has survived until today in dedicated instruments for spark source (SS)-MS and isotope ratio (IR)-MS (Sect. 15.2) [90].

An EB design effecting an image plane of 140 mm in length with a linear mass scale for detection on a photographic plate has been published by Bainbridge and Jordan (*Bainbridge-Jordan geometry*) [92]. Their paper is especially recommended as it also nicely illustrates the use of photographic plates in those days.

The third famous type of EB arrangement has become known as *Nier-Johnson geometry* (Fig. 4.24) [93]. Here, the ion beam first passes through the electrostatic analyzer producing energy-resolved beams without mass dispersion in the plane of an intermediate slit located at the focal point of the ESA. It then passes through a magnetic analyzer to achieve mass dispersion of the ions. Different from the *Mattauch-Herzog mass spectrograph*, the *Nier-Johnson mass spectrometer* was constructed to be used in conjunction with a *scanning magnet* to focus one specific m/z after the other onto a point detector. This presented a major advantage for the use of UV recorders or electronic data acquisition as well as for the achievement of better ion optics.

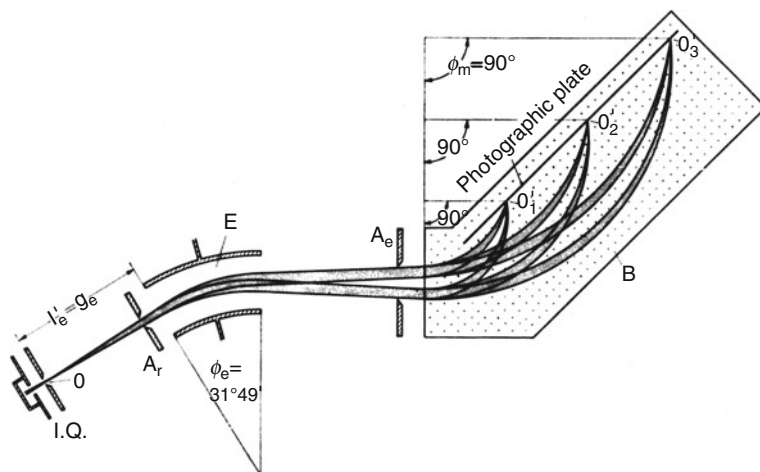


Fig. 4.23 Mattauch-Herzog double-focusing mass spectrograph providing direction and momentum focusing of ions on a plane [89]. The ESA precedes the magnet. Placing a photographic plate in the image plane allows simultaneous recording of a m/z range (Reproduced from Ref. [91] with kind permission of Curt Brunnée)

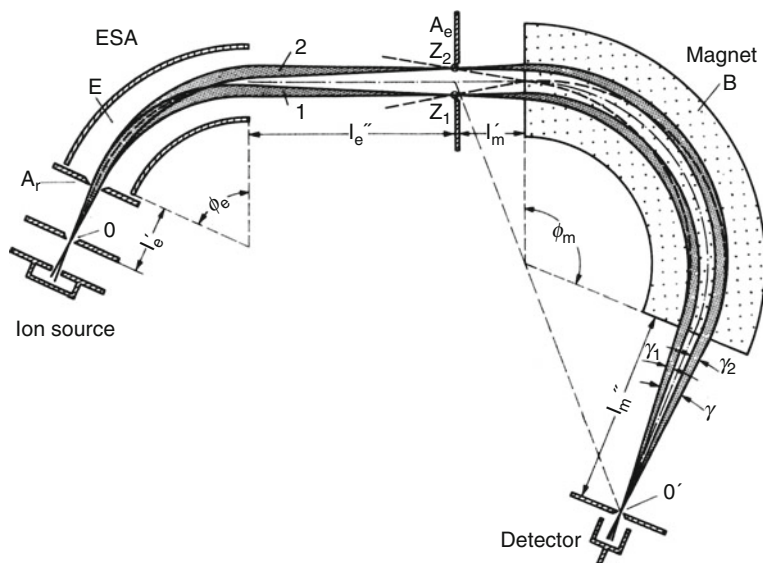


Fig. 4.24 Double-focusing mass spectrometer of EB geometry, basically a Nier-Johnson type instrument. Direction and velocity focusing are shown exaggerated. After exiting the ESA, the energy-resolved beam passes through a wide intermediate slit into the magnetic sector. The large aperture ensures good overall transmission (Reproduced from Ref. [91] with kind permission of Curt Brunnée)

Scan

Typically, on magnetic sector mass spectrometers a spectrum is produced by varying the strength of the magnetic field to successively pass through ions of different m/z . This is termed *magnetic field scan* [94]. For scans *linear in time*, the *scan rate* is given in units of $m/z \text{ s}^{-1}$, e.g., 500 m/z s^{-1} . For scans *exponential in time*, the *scan rate* is reported in units of s per decade, e.g., 10 s/decade means 10 s from m/z 30 to 300 or from m/z 100 to 1000.

Some later EB instrument models were constructed to be used in combination with an (optional) array detector, e.g., the JEOL HX-110 (EB), the Thermo Finnigan MAT 900 (EB), and the Micromass Autospec (EBE) instruments could be equipped in that way. The array detector was located at the focus plane of the magnet.

Successful constructions of *reversed geometry*, i.e., BE instead of *forward* EB design, have been presented in the form of the MAT 311 in the mid-1970s and shortly after by the VG Analytical ZAB-2F instrument [95] based on a proposal by Hintenberger and König [96].

More recent BE geometry instruments are presented by the Thermo Finnigan MAT 90 and 95 series (Fig. 4.25), the JEOL JMS-700, and although not strictly due to its EBE geometry [97], the Micromass Autospec. However, the only instrument of this millennium incorporating a redesigned BE geometry has been the Thermo Scientific DSF introduced in 2005. In contrast to organic and biomedical MS, double-focusing designs are still highly relevant in inorganic MS (Chap. 15) [90].

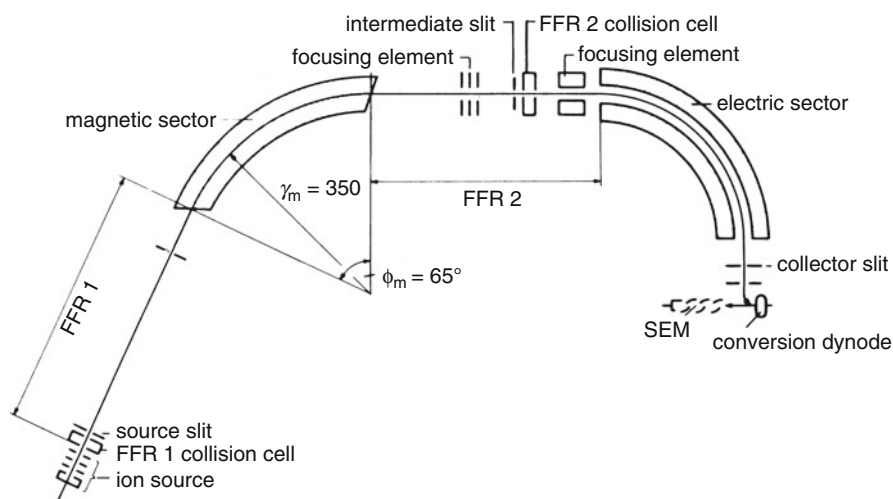


Fig. 4.25 The Finnigan MAT 90 double-focusing mass spectrometer with rotated pole faces of the magnetic sector (Reproduced from Ref. [2] with permission. © Elsevier Science, 1987)

4.3.6 Adjusting the Resolving Power of a Sector Instrument

The ion optics of a sector instrument are the analog to a cylindrical lens in light optics. Accordingly, the reduction of an aperture can be used to obtain a sharper image, i.e., to increase resolving power (Sect. 3.4). Slits are used instead of circular apertures to comply with the cylindrical properties of the ion optical system. Most important are the settings of the *object slit* (*source slit*, *entrance slit*) and the *image slit* (*collector slit*, *exit slit*, *detector slit*). Intermediate slits may be used in addition. Unfortunately, closing slits also means cutting off ions from the beam, and thus reduction of the transmission of the mass analyzer. In the ideal case, the improvement of resolution by a factor of 10 goes along with a reduction in transmission to 10%, in reality the effect is often worse.

Setting the slits The influence of relative slit width on peak shape and resolution is demonstrated on the second isotopic peak of toluene molecular ion, $^{13}\text{C}_2\text{ }^{12}\text{C}_5\text{H}_8^+$, m/z 94 (Fig. 4.26). With the entrance slit at 50 μm and the exit slit at 500 μm the peak is flat-topped (*left*), because a narrow beam from the entrance sweeps over the wide open detector slit keeping the intensity constant as the scan proceeds until the beam passes over the other edge of the slit. Closing the exit slit to 100 μm increases resolution to 2000 without affecting the peak height (*center*), but reduces the peak area by a factor of 4 in accordance with an increase in resolution by the same factor. Further reduction of the exit slit width to 30 μm improves resolution at the cost of peak height (*right*). (Any sector instrument must behave alike, otherwise, cleaning or other maintenance are required.)

Operate to fit your needs

The ultimate resolution of a magnetic sector mass spectrometer is reached when the slits are closed to a width of a few micrometers. Often, the slit height is also reduced, e.g., from 5 to 1 mm. In daily work, the resolution will be set to fit the actual task, e.g., $R = 1000\text{--}2000$ for low-resolution work, $R = 3000\text{--}5000$ if accurate mass determination at high scan rates is needed (GC-MS, Chap. 14) or isotopic patterns of high mass analytes have to be resolved, or $R = 7000\text{--}15,000$ in slow-scanning accurate mass measurements.

4.3.7 Optimization of Sector Instruments

To improve the performance of sector instruments in terms of scan speed, resolving power, transmission, and mass range, the construction, in particular that of the magnet, needs some additional refining.

The rapid change of a magnetic field suffers from hysteresis, i.e., the magnetic flux does not exactly follow the change of the electric current through the coils in

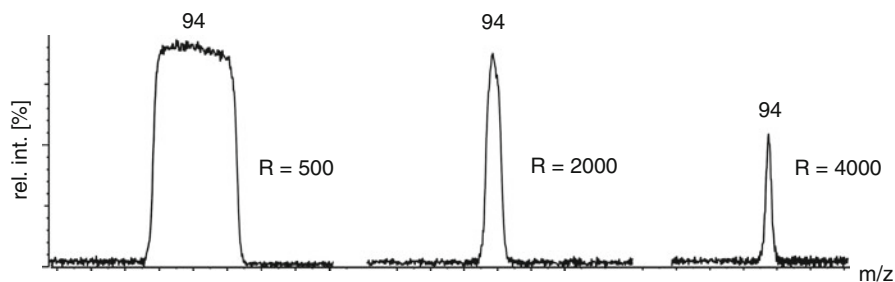


Fig. 4.26 The influence of relative slit width settings on peak shape and resolution on a magnetic sector instrument. The peak shape first changes from flat-topped (*left*) to Gaussian (*center*) and finally resolution improves at cost of peak height (*right*)

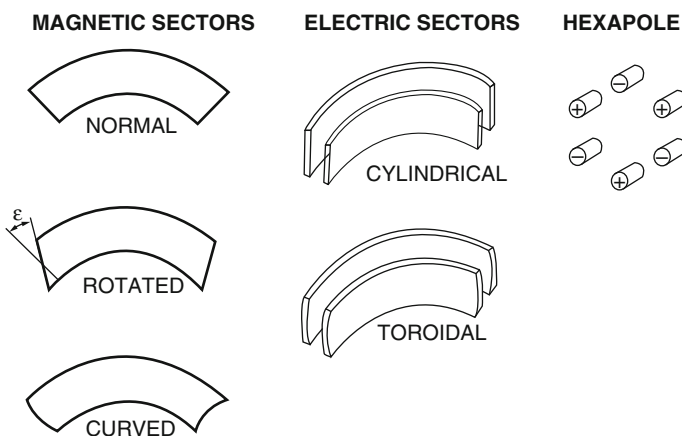


Fig. 4.27 Types and shapes of ion optical elements used in magnetic sector instrument design (By courtesy of Thermo Fisher Scientific, Bremen)

time, but lags behind due to the induction of eddy currents. On one side, this causes problems in creating a scan perfectly linear in time, on the other this prevents high scan rates as required for GC-MS. Lamination of the yoke substantially reduces these problems [98] and is employed in all modern sector instruments.

In order to extend the mass range one either has to increase the field strength or the radius of the magnet. However, there are limitations of the field strength with non-superconducting magnets at about 2.4 T. Instead of simply enlarging the radius, the pole faces of the magnet can be rotated to preserve a compact design by reduction of its focal length (Figs. 4.27, 4.28, and 4.29) [2].

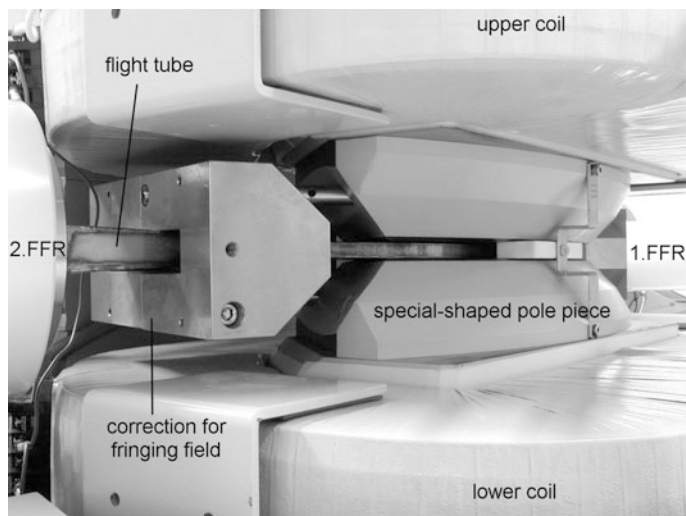


Fig. 4.28 Flight tube passing through the gap of the magnetic sector of a JEOL JMS-700 instrument seen from the ESA side. The shapes of the pole pieces of the yoke and the additional blocks around the tube are designed to minimize fringing fields. In addition the pole faces are rotated to increase the mass range

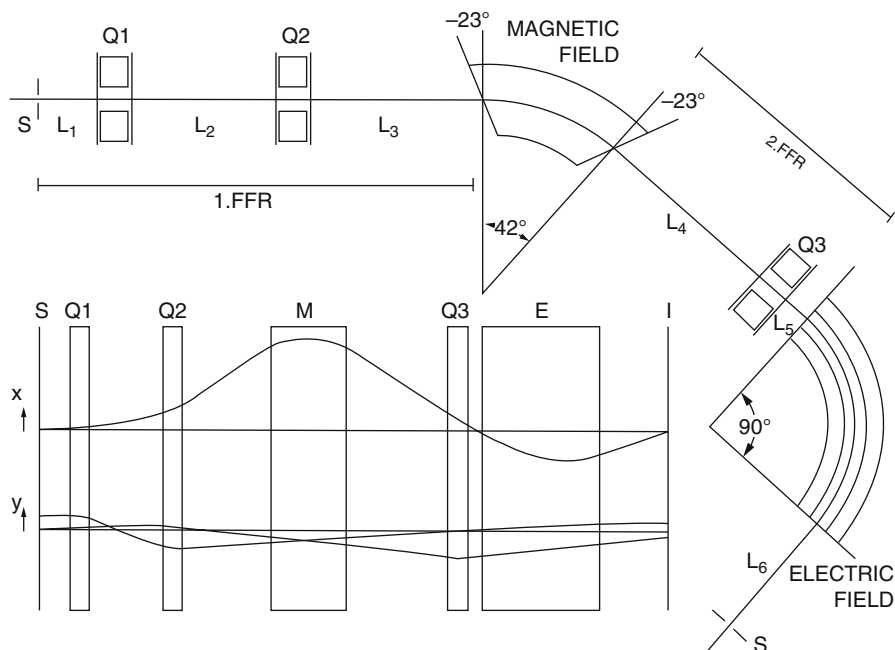


Fig. 4.29 Layout of the JEOL JMS-700. Three DC quadrupole lenses are used to improve the transmission of the magnetic sector. The inset shows horizontal (x) and vertical (y) trajectories where the height of the beam (y) is clearly reduced to pass through a narrow gap between the pole shoes of the magnet (Adapted from Ref. [99] with permission. © Elsevier Science, 1985)

Another problem is due to fringing fields. To reduce these defocusing effects at the entrance and exit of the field, the pole pieces of the yoke of the electromagnet generally have specially shaped edges.

Furthermore, pure EB and BE designs are somewhat limited concerning the transmittance through a narrow magnet gap as compared to instrument designs using some DC quadrupole (q) or DC hexapole (h) lenses to form the ion beam (Fig. 4.29) [99, 100]. However, quadrupole and hexapole lenses do not alter the effective instrument geometry, i.e., such an analyzer behaves like a pure BE analyzer in any mode of operation.

4.3.8 Summary of Magnetic Sector Instruments

Ion Separation

Ions moving perpendicular to a magnetic field are forced on a circular path by action of the Lorentz force. The radius of that motion is determined by a counterbalance of Lorentz force and centripetal force. Ions of equal kinetic energy but different in mass therefore travel on individual radii, and thus, a separation by momentum is effected. The radius of ion motion or the magnetic field strength to achieve a defined radius to hit the detector is then used to derive m/z values of the ions.

Configurations

Magnetic sector instruments can be built relying on magnetic (B) separation alone. Such single-focusing instruments are limited in resolving power. At least one order of magnitude higher resolving power is achieved when the kinetic energy spread of ions is compensated or filtered by means of an electrostatic sector (E). Designs employing B and E are termed double-focusing. E and B can be combined in numerous ways thereby giving rise to EB, BE, EBE, BEBE, and other designs.

Performance Characteristics

Double-focusing magnetic sector instruments, either in BE or EB configuration, typically can achieve resolving powers in excess of $R = 60,000$. However, this requires extremely slow scanning and comes at the expense of very low transmission, as the slits need to be closed down. High transmission at wide-open slits results in $R = 1000\text{--}2000$ and allows faster scanning. Accurate mass measurements are typically performed at moderate scan rates and $R = 5000\text{--}10,000$ and require internal mass calibration.

Magnetic Sector Instruments in the Laboratory

In organic and biomedical MS, magnetic sector instruments were most popular in the 1960s to early 2000s. More recently, most have been replaced by TOF, FT-ICR, or Orbitrap mass analyzers. In inorganic MS, in particular for isotope ratio determinations and spark-source MS, magnetic sector instruments are still of high

relevance as they can deal with large energy dispersion and allow for multi-collector setups in the image plane of the magnet.

4.4 Linear Quadrupole Instruments

4.4.1 Introduction

Since the Nobel Prize-awarded discovery of the mass-analyzing and ion-trapping properties of two- and three-dimensional electric quadrupole fields [101, 102] and the concomitant construction of a *quadrupole (Q) mass spectrometer* [103, 104], this type of instrument has steadily gained importance. Chiefly starting from GC-MS that demanded for rapid scanning analyzers, quadrupole instruments made their way into the MS laboratories [105–108], although those early systems offered poor resolving power and low mass range, e.g., m/z 1–200. Modern quadrupole instruments cover up to m/z 2000 or even higher with good resolving power and represent some kind of routine device in LC-MS. The advantages of linear quadrupoles are:

- Linear quadrupoles offer high transmission.
- Quadrupoles are light-weight, very compact, and comparatively low-priced.
- Quadrupoles require low ion acceleration voltages.
- Quadrupoles allow high scan speeds since scanning is realized by solely sweeping electric potentials.

Terminology

Linear quadrupoles were the first to be incorporated in commercial instruments. Thus, these instruments are simply referred to as quadrupole mass spectrometers and the attribute “linear” is often omitted. As we will see later (Sects. 4.5 and 4.6) other electrode shapes are also possible but are forming electric RF quadrupole fields of other geometries. These designs are also available in commercial mass spectrometers.

4.4.2 The Linear Quadrupole

A linear quadrupole mass analyzer consists of four hyperbolically or cylindrically shaped rod electrodes extending in the z -direction and mounted in a square configuration (xy -plane, Figs. 4.30 and 4.31). The pairs of opposite rods are each held at the same potential which is composed of a DC and an AC component.

As an ion enters the quadrupole assembly in the z -direction, an attractive force is exerted on it by one of the rods with its charge actually opposite to the ionic charge. If the voltage applied to the rods is periodic, attraction and repulsion in both the x -

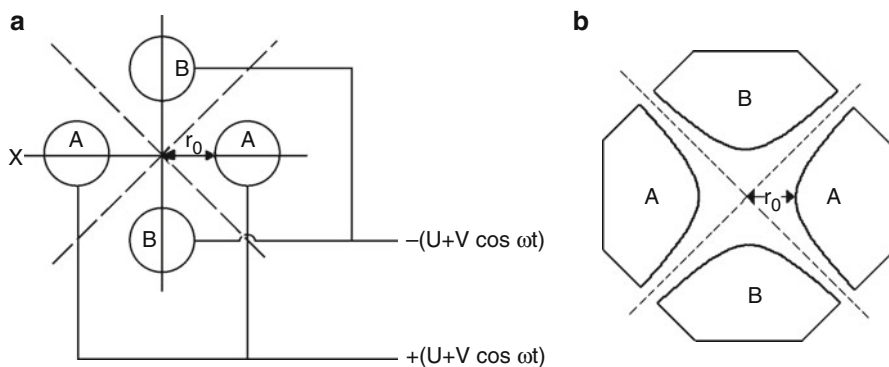


Fig. 4.30 Cross section of a quadrupole (a) for the cylindrical approximation and (b) for the hyperbolic profile of the rods. The electric field is zero along the *dotted lines*, i.e., along the asymptotes in (b) (a) Courtesy of Waters Corp., MS Technologies, Manchester, UK

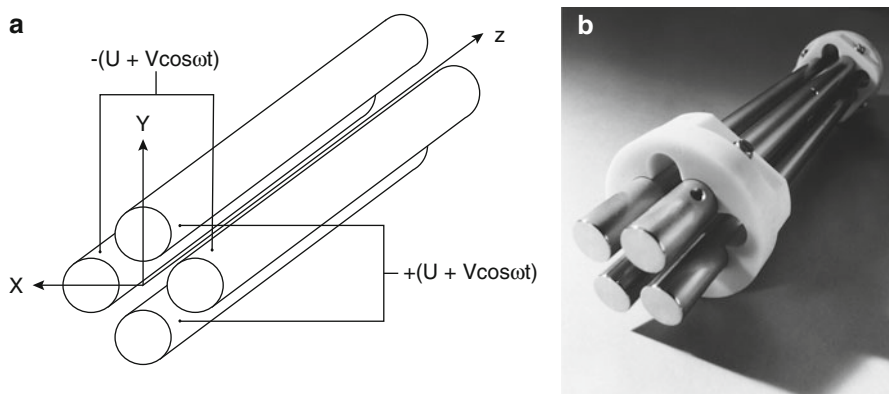


Fig. 4.31 Linear quadrupole mass analyzer: schematic (a) and photograph (b) (By courtesy of (a) JEOL, Tokyo and (b) Waters Corp., MS Technologies, Manchester, UK)

and y -directions will alternate in time, because the sign of the electric force also changes periodically in time. If the applied voltage is composed of a DC voltage U and a radiofrequency (RF) voltage V with the frequency ω the total potential Φ_0 is given by

$$\Phi_0 = U + V \cos \omega t \quad (4.18)$$

Thus, the equations of motion are

$$\begin{aligned}\frac{d^2x}{dt^2} + \frac{ez}{m_i r_0^2} (U + V \cos \omega t)x &= 0 \\ \frac{d^2y}{dt^2} - \frac{ez}{m_i r_0^2} (U + V \cos \omega t)y &= 0\end{aligned}\quad (4.19)$$

Remember that m_i denotes ion mass [kg] and charge is $q = ez$, where e is the electron charge [C] and z the charge number. In case of an inhomogeneous periodic field such as the above quadrupole field, there is a small average force which is always in the direction of the lower field. The electric field is zero along the dotted lines in Fig. 4.30, i.e., along the asymptotes in case of the hyperbolic electrodes. It is therefore possible that an ion may traverse the quadrupole without hitting the rods, provided its motion around the z -axis is stable with limited amplitudes in the xy -plane. Such conditions can be derived from the theory of the *Mathieu equations*.

Mathieu equations

The Mathieu functions were originally derived in 1868 by Émile Léonard Mathieu, a French mathematician, to describe the vibrations of elliptical drumheads. It turned out that they are also useful to treat quadrupole mass filters and several other physical phenomena.

Now, writing Eq. (4.19) in dimensionless form yields

$$\begin{aligned}\frac{d^2x}{d\tau^2} + (a_x + 2q_x \cos 2\tau)x &= 0 \\ \frac{d^2y}{d\tau^2} + (a_y + 2q_y \cos 2\tau)y &= 0\end{aligned}\quad (4.20)$$

The parameters a and q can now be obtained by comparing with Eq. (4.19)

$$a_x = -a_y = \frac{4qU}{m_i r_0^2 \omega^2}, \quad q_x = -q_y = \frac{2qV}{m_i r_0^2 \omega^2}, \quad \tau = \frac{\omega t}{2} \quad (4.21)$$

For a given set of U , V , and ω the overall ion motion can result in a stable trajectory causing ions of a certain m/z value or m/z range to pass the quadrupole. Ions oscillating within the distance $2r_0$ between the electrodes will have stable trajectories. These are transmitted through the quadrupole and detected thereafter. The path stability of a particular ion is defined by the magnitude of the RF voltage V and by the ratio U/V .

By plotting the parameter a (ordinate, time invariant field) vs. q (abscissa, time variant field) we obtain the stability diagram of the two-dimensional quadrupole field. This reveals the existence of regions where (i) both x - and y -trajectories are stable, (ii) either x - or y -trajectories are stable, and (iii) no stable ion motion occurs

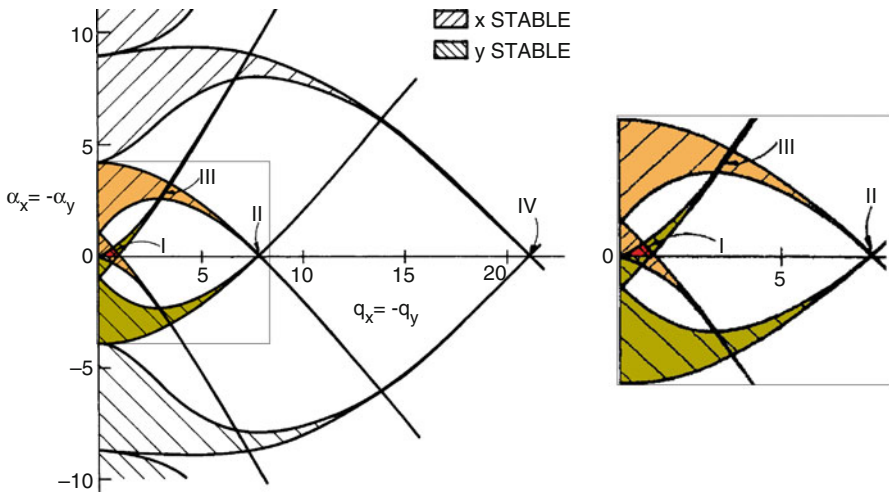


Fig. 4.32 Stability diagram for a linear quadrupole analyzer showing four stability regions (I–IV) for x - and y -motion. The portion within the *square frame* is zoomed to double size on the *right*. Stability region I only covers the small *red region* in the center (Adapted from Ref. [107] with permission. © John Wiley & Sons Inc., 1986)

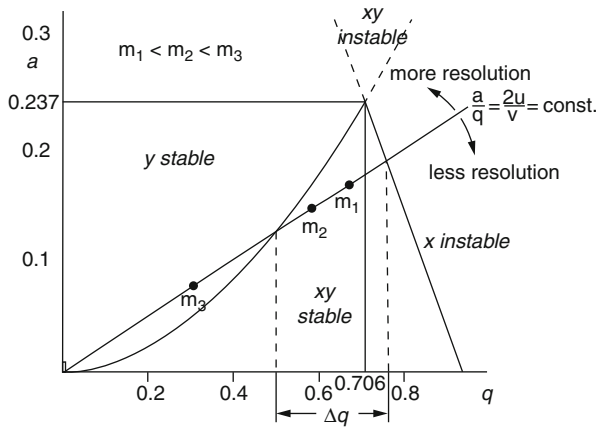
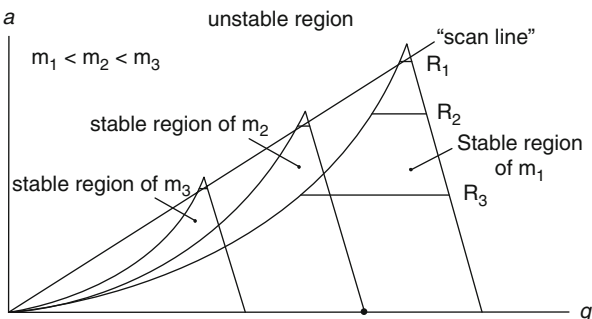


Fig. 4.33 Detail of the upper half of region I of the stability diagram for a linear quadrupole analyzer (Reproduced from Ref. [102] with permission. © World Scientific Publishing, 1993)

(Fig. 4.32) [107]. Among the four stability regions of the first category, the tiny central region I is of special interest for the normal mass-separating operation of the linear quadrupole. Zooming in to region I (x - and y -trajectories stable) yields what is commonly referred to as the *stability diagram of the linear quadrupole* (Fig. 4.33) [101, 102].

If the ratio a/q is chosen so that $2 U/V = 0.237/0.706 = 0.336$, the xy -stability region shrinks to one point, the apex, of the diagram (cf. Eq. 4.21, Fig. 4.33).

Fig. 4.34 Scanning of linear quadrupoles means performing a $U/V = \text{constant}$ linked scan. Resolution is adjusted by variation of the a/q ratio: higher a/q ratio means higher resolving power and is represented by a steeper “scan line”; $R_1 > R_2 > R_3$



By reducing a at constant q , i.e., reducing U relative to V , an increasingly wider m/z range can be transmitted simultaneously. Sufficient resolving power is achieved as long as only a small m/z range remains stable, e.g., one specific $m/z \pm 0.5$ for *unit resolution* (Sect. 4.4.3). Thus, the width (Δq) of the stable region determines the resolving power (Fig. 4.34). By varying the magnitude of U and V at constant U/V ratio an $U/V = \text{constant}$ linked scan is obtained allowing ions of increasingly higher m/z to pass the quadrupole.

Overall, the quadrupole analyzer rather acts as a mass filter than as a momentum (B sector) or energy (ESA) spectrometer; hence the widespread use of the term *quadrupole mass filter*.

Scanning a quadrupole

Scanning of any linear quadrupole means shifting the whole stability diagram along a “scan line”, because each m/z value has a stability diagram of its own (Figs. 4.33 and 4.34). The representation of a scan by a “scan line” would only be correct in case of infinite resolving power, i.e., if the apices were connected. Any real resolving power is represented by a horizontal line across the stability region, where only ions falling in the region above that line are transmitted.

Ion trajectory simulations allow for the visualization of the ion motions while traveling through a quadrupole mass analyzer (Fig. 4.35). Furthermore, the optimum number of oscillations to achieve a certain level of performance can be determined. It turns out that best performance is obtained when ions of about 10 eV kinetic energy undergo approximately a hundred oscillations (Fig. 4.36) [109].

Typical quadrupoles

Standard quadrupole analyzers have rods of 10–20 mm in diameter and 15–25 cm in length. The radiofrequency is in the order of 1–4 MHz, and the DC and RF voltages are in the range of some 10^2 – 10^3 V. Thus, ions of about 10 eV kinetic energy undergo about 100 oscillations during their passage.

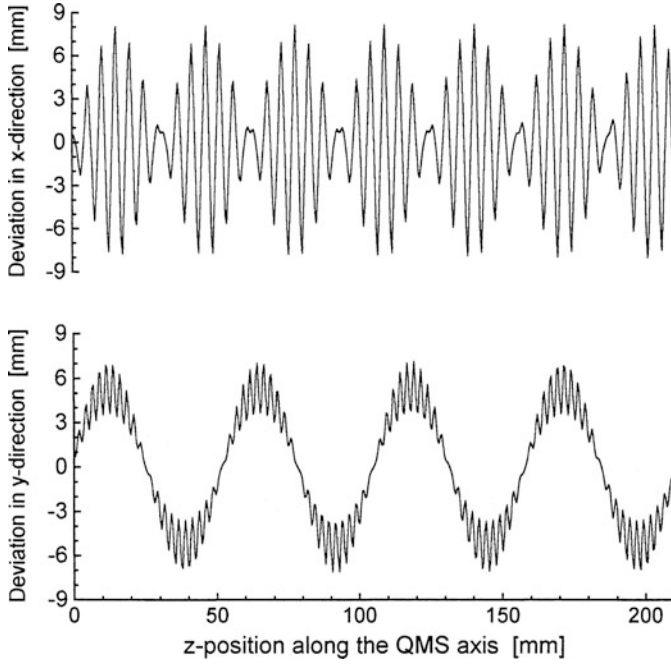


Fig. 4.35 Projection of a 3D trajectory simulation of a stable ion onto the x - and y -coordinates (Reproduced from Ref. [109] with permission. © Elsevier Science, 1998)

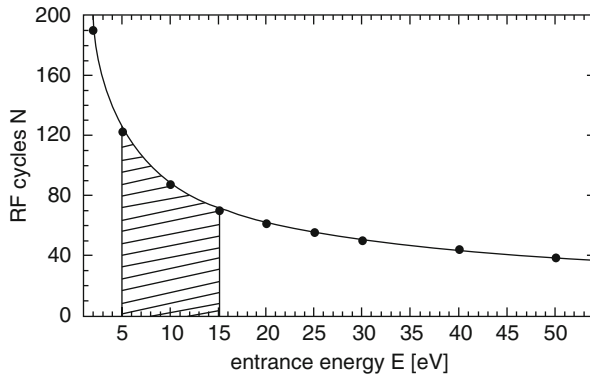


Fig. 4.36 Relation of RF cycles experienced by the ions as a function of entrance energy. The shaded area marks the region of optimized performance (Reproduced from Ref. [109] with permission. © Elsevier Science, 1998)

4.4.3 Resolving Power of Linear Quadrupoles

Quadrupole analyzers generally are operated at so-called *unit resolution*, normally restricting their use to typical low resolution (LR) applications [110, 111]. At unit resolution adjacent peaks are just separated from each other over the entire m/z range, i.e., $R = 20$ at m/z 20, $R = 200$ at m/z 200, and $R = 2000$ at m/z 2000. An example of unit resolution is presented in Sect. 4.5.3.

The resolution as adjusted by the U/V ratio cannot arbitrarily be increased, but is ultimately limited by the mechanical accuracy with which the rods are constructed and supported ($\pm 10 \mu\text{m}$) [110]. Above an m/z value characteristic of each quadrupole assembly, any further improvement of resolution can only be achieved at the cost of significantly reduced transmission. Nonetheless, high-performance quadrupoles allowing for about tenfold unit resolution can be built [111].

Theoretically, the electrodes of a quadrupole mass filter should have a hyperbolic cross section for optimized geometry of the resulting quadrupole field, and thus for optimized performance (Fig. 4.37) [101, 102]. However, for ease of manufacture, cylindrical rods are often employed instead. By adjusting the radius of the rods carefully ($r = 1.1468 \times r_0$), a hyperbolic field may be approximated [112]. However, even slight distortions of the ideal quadrupole field either from interference with external fields or due to low mechanical precision or inadequate shape of the device cause severe losses of transmission and resolution [113]. The expected advantages of hyperbolic rods [114] have been demonstrated by ion trajectory calculations [109, 115]: circular rods cause a reduction in macromotion frequency because of an increased residence time of the ions in close vicinity to the rods (Fig. 4.38); this in turn means reduced resolution.

Besides optimization of mechanical accuracy, the resolving power of quadrupoles can be improved by innovative modes of operation. The operation as a multiple pass system with ion reflection at either end extends the flight path and

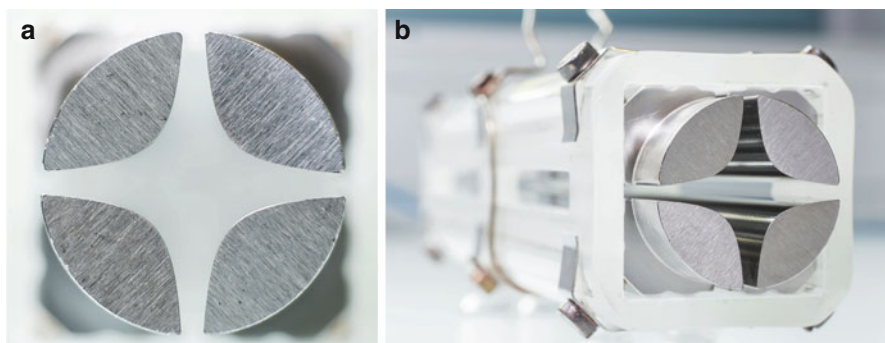
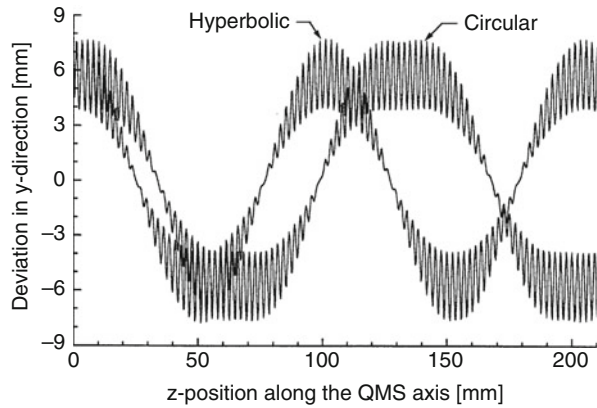


Fig. 4.37 Linear quadrupole with hyperbolic rods. (a) Head on view showing the cross section of the rods and (b) whole device partially revealing the polished inner surfaces. The rods are mounted in a precision-machined quartz frame. This particular quadrupole once belonged to a Finnigan TSQ 700 instrument

Fig. 4.38 Motion in the y -coordinate of ions traveling along a quadrupole with circular rods compared to ions in a quadrupole with ideal hyperbolic field. Circular rods cause a reduced macromotional frequency and longer residence time in the close vicinity to the (non-ideal) rod surfaces (Reproduced from Ref. [109] with permission. © Elsevier Science, 1998)



thus the number of RF cycles. The same effect can be obtained from increased radiofrequency and for ions traveling slower through the device [110]. Alternatively, the quadrupole may be operated in stability regions other than the first, e.g., in the second or fourth [110, 116]; doing so requires higher ion kinetic energies of about 750 eV.

4.4.4 RF-Only Quadrupoles, Hexapoles, and Octopoles

Setting the DC voltage U to zero transforms the quadrupole into a wide band pass for ions. In the stability diagram this mode of operation is represented by an operation line equivalent to the q -axis (Figs. 4.33 and 4.34). Such devices are commonly known as *RF-only quadrupoles* (q), *RF-only hexapoles* (h) and *RF-only octopoles* (o) are used analogously. Generally, higher-order RF $2N$ -multipoles differ from quadrupoles in that they do not exhibit a sharp m/z cutoff in transmission, because x and y motions are strongly coupled, which causes the boundaries of ion stability to become rather diffuse. For low trapping voltages, the ion trajectories in an RF $2N$ -multipole are approximated by an effective mechanical potential, $U_{\text{eff}(r)}$, given by [108, 117]:

$$U_{\text{eff}(r)} = \frac{N^2}{4} \frac{(ze)^2}{m_i \Omega^2} \frac{V^2}{r_0^2} \left(\frac{r}{r_0} \right)^{2N-2} \quad (4.22)$$

where N is the order of the multipole, e.g., $N = 3$ for a hexapole. According to Eq. (4.22), higher-order multipoles exhibit increasingly steeper potential wells, offer better ion-guiding capabilities and better wide-band pass characteristics, i.e., wider m/z range acceptance (Fig. 4.39). This property led to the widespread application of RF quadrupoles, RF hexapoles, and RF octopoles as *ion guides* and *collision cells* [118].

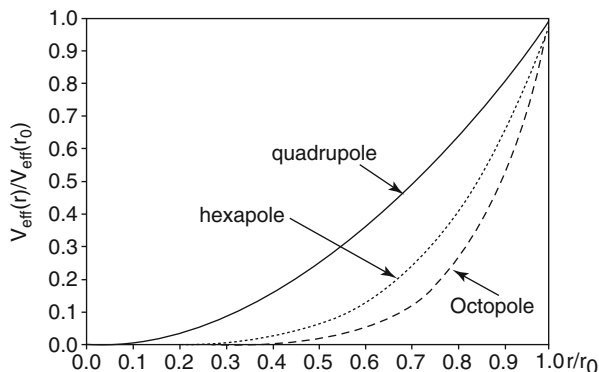


Fig. 4.39 Comparison of effective potentials for quadrupole (r^2), hexapole (r^4) and octopole fields (r^6) (Reproduced from Ref. [117] with permission. © Wiley Periodicals, Inc., 2005)

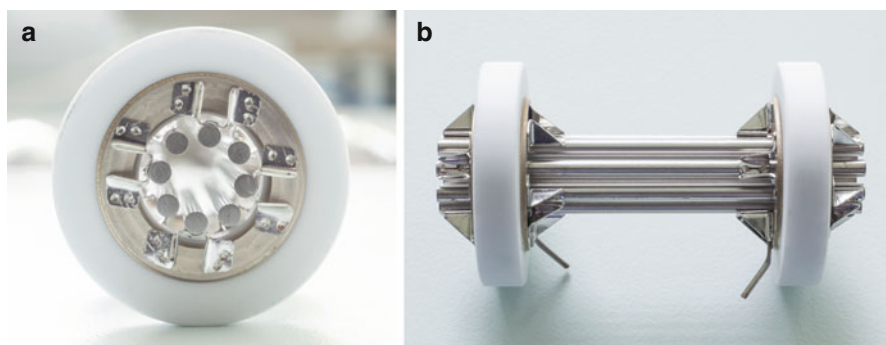
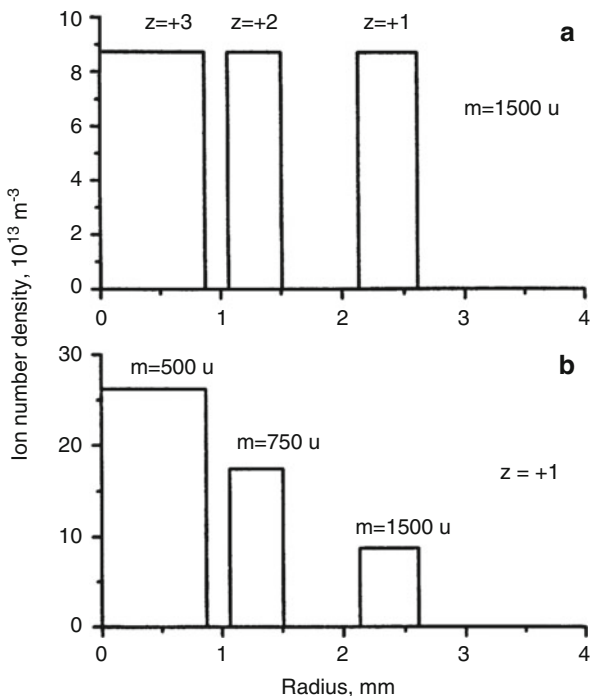


Fig. 4.40 RF octopole ion guide used to bridge a differential pumping stage of an ESI interface in a Finnigan LCQ instrument. (a) Head-on view to show the octopole alignment and (b) side view. Each of the two pins pointing down is connected to supply the RF voltage to four of the rods in alternation. The round rods are ca. 3 mm in diameter and the length of this device is about 7 cm

RF ion guides are employed in many ways to transfer ions of low kinetic energy, typically of 1–50 eV, from one functional unit to another without substantial losses [117, 119]. Ion guides are used to adapt atmospheric pressure ion sources to mass analyzers, e.g., for APCI, ESI, and ambient MS (Fig. 4.40; Chaps. 7, 8, 12, and 13). From the viewpoint of the ions, they act like a hose or pipe while being fully permeable for neutrals. Thus, the RF ion guide allows residual gas to effuse through the gaps between the rods into the vacuum pumps, whereas ions are escorted into the mass analyzer. Examples for RF ion guide usage will be given in the instrument schemes to follow later in this chapter.

In contrast to expectations based on scattering by collisions with residual gas, RF-only multipoles deliver even improved transmission at moderate vacuum conditions in the range of 10^{-3} – 10^{-2} mbar. This is due to a reduction in ion kinetic energy and concomitant collisional damping of ion motion toward the central axis of the device, so-called *collisional cooling* [108, 120–122]. It has been shown that

Fig. 4.41 Calculated number density distributions of ions stored in a collisional cooling RF-only quadrupole ion guide having an inner radius of 4 mm and being operated at 1 MHz. (a) Radial positions of ions of 1500 u bearing 1, 2, and 3 positive charges. (b) Radial position of ion clouds of singly charged ions of m/z 500, 1000, and 1500 (Reproduced from Ref. [121] with permission. © John Wiley & Sons, Ltd., 2000)



ions of 25 eV kinetic energy are slowed down to 0–2 eV upon passing through a 15-cm-long RF-only quadrupole ion guide at 8×10^{-3} mbar [120, 123]. Ions of higher mass (not higher m/z) are more prone to this effect, e.g., a sevenfold increase was found for ions of about 200 u, whereas ions of about 17,000 u showed 80-fold improvement in transmission [120]. Here, collisional cooling causes a confinement of the ion beam towards the central axis of the quadrupole which in turn increases the transmission efficiency through an exit aperture. This phenomenon is known as *collisional focusing* (cf. Fig. 4.43 in Sect. 4.5.1) [108, 122, 124].

It is even more interesting that the cooled ion cloud forms concentric cylindrical layers inside the RF-only multipole, each of those layers being composed of ions of the same m/z value with higher m/z ions gathering in more outward radial layers. This behavior is due to more effective RF focusing for ions of lower m/z that pushes these ions closer towards the center. Multiply charged ions form more distinct radial boundaries of the layers as compared to singly charged ion clouds of the same m/z and charge density (Fig. 4.41). The gaps of low ion population between the layers result from space charge repulsion [121]. Formation of such m/z -stratified structures requires sufficiently high charge density and effective collisional damping. Both RF-only collision multipoles and linear quadrupole ion traps as employed for external ion accumulation fulfill those criteria. When the linear ion density increases, the maximum ion cloud radius also increases. Overfilling of the multipole capacity results in a strong discrimination against high m/z ions, because the ion clouds expand to larger radii causing outer layers (high- m/z ions) to hit the multipole rods [121].

Conditions for thermalization

From the work by Douglas [120] a rule of thumb can be derived to judge whether thermalization occurs. This $p \times d$ rule demands the product of pressure (p in Torr) times path length (l in mm) to be larger than 0.2 mTorr. For example, at 2×10^{-3} Torr a RF-only device of 100 mm length is just sufficient for effective ion cooling as we have 2×10^{-3} Torr \times 100 mm = 0.2 mTorr.

RF-only *quadrupole*, *hexapole*, or *octopole collision cells* [117, 125, 126] are part of so-called *triple quadrupole mass spectrometers*, which essentially represent QqQ, QhQ, or QoQ instruments, respectively, depending on the type of RF-only collision cell actually in place. They are efficient tools for tandem mass spectrometry (Chap. 9).

Different from magnetic sector or TOF instruments having collimated beams of energetic ions, the ions are exiting from quadrupoles in almost any direction on the xy -plane. Thus, real field-free regions as employed in sector or TOF instruments have to be replaced by ion-guiding collision cells to allow CID of ions of 5–100 eV kinetic energy. RF-only collision cells need not to be straight: starting from the Finnigan TSQ700 bent geometries were introduced, and 90° cells or 180° cells are nowadays common. Besides a reduced footprint of the instrument, the bent geometries have other beneficial effects such as the elongation of the flight path through the collision region for improved fragmentation efficiency and the exclusion of neutrals or photons from hitting the detector, and thus, reduced noise levels.

Ions can even stop

The initial kinetic energy of slow ions can be lost upon several collisions. At 5×10^{-3} mbar (0.5 Pa) fragment ion kinetic energies are reduced to about 1 eV [123]. The ions may even stop their motion along the cell [121, 124]. Under such conditions, the continuous ion current into the cell is the only impetus to push the ions through as a result of space-charge effects. The resulting dwell time of about 10 ms allows up to about 5000 (reactive) collisions to take place at about 5×10^{-2} mbar (5 Pa) collision gas (or reagent gas) pressure in an octopole collision cell [127].

Within the last decade, RF quadrupole ion guides with square or at least rectangular rod cross sections have also been used. Most of this development has been done by instrument manufacturers and few has been published on this topic. However, it appears that these square-rod quadrupoles offer the same level of performance as round-rod higher-order RF ion guides at reduced cost of

manufacture. We will get back to square rods in the context of linear quadrupole ion traps in the next section.

Postponed summary A summary of RF quadrupole devices will be given in Sect. 4.6.12. As we will see during the next two sections dealing with linear quadrupole ion traps and ion traps with three-dimensional quadrupole fields these devices have much in common, suggesting to summarize and compare them together later.

4.5 Linear Quadrupole Ion Traps

4.5.1 Linear RF-Only Multipole Ion Traps

As we have just learned, collisional cooling may bring translational ion motion along the axis of an RF-only multipole almost to a halt, thereby transforming such an RF-only multipole ion guide into an ion storage device [121]. To prevent ions inside the multipole from escaping via either open end, one creates a trapping potential well by placing electrodes of slightly higher potential adjacent to the front and rear ends of the multipole [128]. Such devices are known as *linear (quadrupole) ion traps* (LIT).

Only quadrupoles are mass-selective

Quadrupoles are the only devices capable of mass-selective operation, whereas higher-order RF ion guides or higher-order LITs can only guide, accumulate, store, and finally release ions for subsequent m/z analysis.

While the entrance plate of the LIT is held at low potential, ions may enter the radially ion-confining RF field. The time span for ion accumulation is limited by

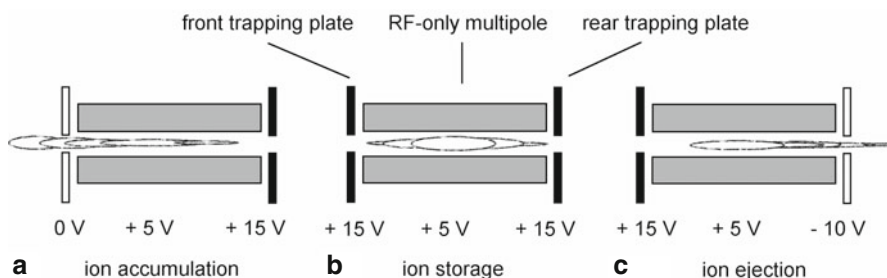
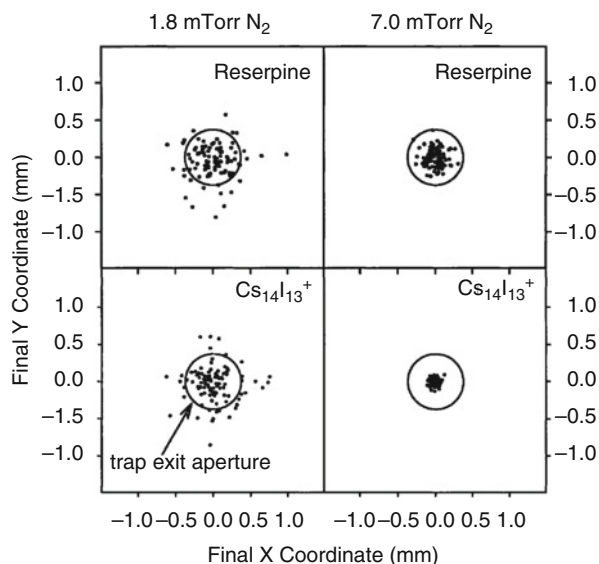


Fig. 4.42 Operation of a linear RF multipole ion trap illustrated using typical DC voltage offsets for positive ions. (a) Ion accumulation with backside potential wall up, (b) storage of ions with both trapping potentials up, and (c) axial ejection of ions from trap using an attractive exit plate potential. The trapping RF multipole section is held at constant DC offset of +5 V in this example

Fig. 4.43 Radial distribution of 100 ion trajectories at the LIT exit aperture (circle indicates 0.7 mm aperture hole) for ions of reserpine and $\text{Cs}_{14}\text{I}_{13}^+$ cluster ions. Collisional focusing is well improved when raising the LIT pressure from 1.8 mTorr (2.4×10^{-3} mbar) to 7.0 mTorr (9.3×10^{-3} mbar) (Adapted from Ref. [122] with permission. © John Wiley & Sons, Ltd., 2001)



reflection of the fast ions at the backside potential wall affording that the entrance gate has to be closed before the lightest ions to be stored can exit the trap via the entrance (Fig. 4.42). Storage of ions in the presence of some buffer gas, e.g., argon or nitrogen at 10^{-3} – 10^{-2} mbar, then allows for their thermalization and collisional focusing towards the LIT axis (Fig. 4.43). Both actual ion kinetic energy of the entering ion beam and the degree of thermalization directly influence the potential required to stop axial ion motion [122]. Vice versa, the trapping efficiency of an LIT for faster ions improves with rising pressure (Fig. 4.44) [129]. Finally, the ions can be axially ejected at any convenient point in time. Alternatively, the RF multipole may be segmented, typically into a longer middle and two shorter ends, which are operated at the same RF drive frequency and amplitude but at a DC offset voltage to create the switchable trapping potential well analogous to the trapping plates [130].

LITs present a rapidly expanding field of instrumentation; they have been established to collect ions externally before injecting them in bunches into an FT-ICR [131] or oaTOF analyzer [122, 128]. LITs capable of scanning by either axial or radial excitation of the ions and even capable of precursor ion selection for MS/MS experiments [129, 130, 132] and have been incorporated in commercial mass spectrometers [117, 133–135]. LITs can be built to store ions of very high m/z , e.g., singly charged ions of bovine serum albumine, m/z 66.000, or even charged particulate matter [136].

This tells us that LITs are highly versatile devices:

- LITs may thermalize ions during their passage to provide narrow kinetic energy distributions before the next step of ion manipulation.

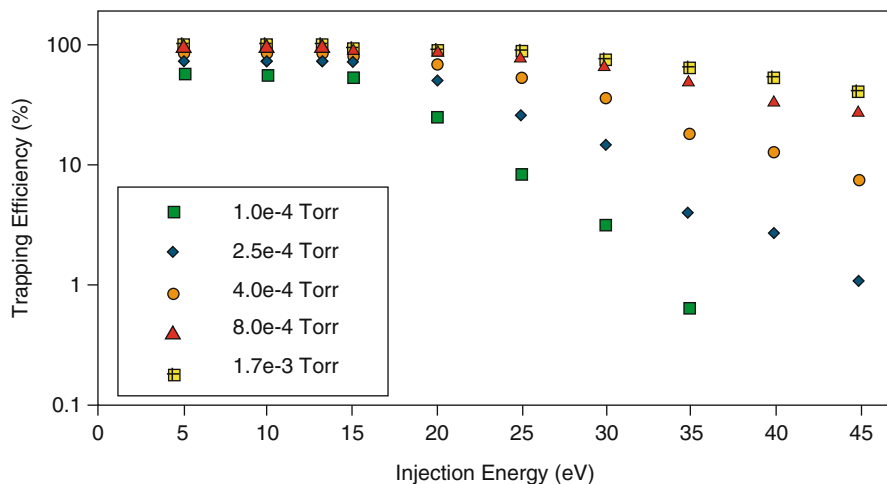


Fig. 4.44 Dependence of the trapping efficiency of an LIT on ion injection energy (reserpine $[M + H]^+$ ions, m/z 609) for varying LIT pressures (from the top 1.3×10^{-4} mbar, 3.3×10^{-4} mbar, 5.3×10^{-4} mbar, 1.1×10^{-3} mbar, 2.3×10^{-3} mbar) (Adapted from Ref. [129] with permission. © John Wiley & Sons, Ltd., 2002)

- LITs can accumulate ions until a population suitable for the respective next step of mass analysis is reached.
- LITs can deliver packages of ions for a mass analyzer operating in batch mode.
- LITs themselves are capable of mass-selective operation and scanning to serve as mass analyzers on their own (Sect. 4.5.2).
- LITs are even capable of precursor ion selection and subsequent ion fragmentation by collisions with buffer gas for MS/MS experiments.

A new time scale

With RF multipoles and even more so with LITs, we have definitely gone beyond the domain of the classical mass spectrometric time scale (Sect. 2.6.2). In ion trapping devices, ions are stored for milliseconds to seconds, i.e., 10^3 – 10^6 times longer than their lifetimes in beam instruments.

4.5.2 Mass-Analyzing Linear Quadrupole Ion Trap with Axial Ejection

Linear ion traps provide high capacities as far as the number of trapped ions is concerned, because the ion cloud can expand along the entire device. It is thus desirable to operate such an LIT not only for ion thermalization and ion accumulation but also as a mass analyzer. In principle, there are two modes possible: one employs excitation of the ions to achieve mass-selective ejection in radial direction

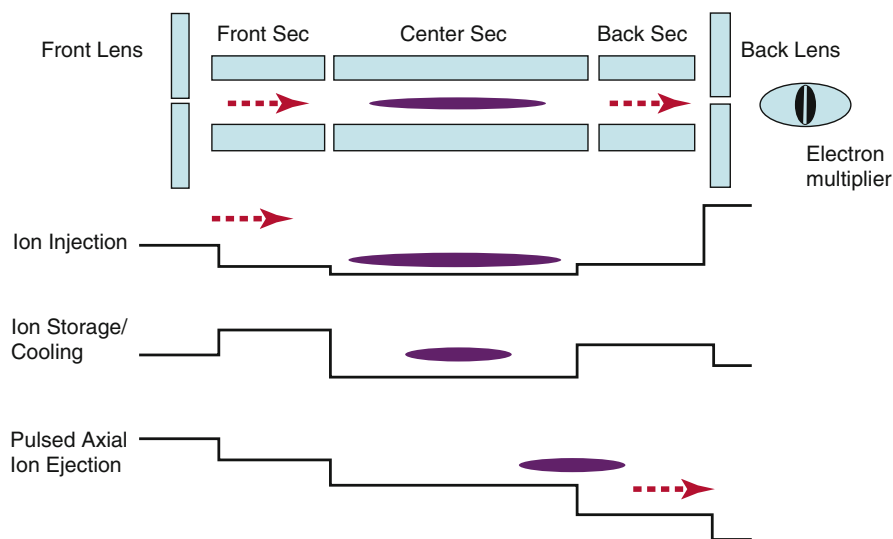


Fig. 4.45 Sequence of DC voltages applied of the lenses and sections of a segmented linear ion trap to achieve mass-selective isolation and axial pulse-out of trapped ions from the mass analyzer. The reasons for segmenting of the LIT are explained in Sect. 4.5.3 and Fig. 4.49 (Reproduced from Ref. [140] with permission. © American Chemical Society, 2004)

[137], the other uses mass-selective axial ejection by application of an auxiliary AC field to the rods of the LIT [129]. The latter mode makes use of the fact that near the exit of the LIT radial ion motion (RF-controlled) and axial ion motion (trapping potential-controlled) are coupled via the fringing fields. When the ion radial secular frequency (governed by the stability parameters and the drive RF) matches that of the auxiliary AC field, ion excitation is effected in a way that also enhances its axial kinetic energy, and thus, leads to ejection from the LIT (Fig. 4.45) [138] and Chap. 5 in [139]).

An instrument incorporating a LIT with mass-selective axial ejection has been developed by Hager by replacing either the RF-only collision quadrupole or the second mass-analyzing quadrupole of a QqQ instrument with a LIT. The attained configurations are Q-LIT-Q (Fig. 4.46) and QqLIT, respectively [129, 134, 135]. The QqLIT offers enhanced sensitivity as compared to its QqQ precursor model and offers new modes of operation [134] and Chap. 3 in [141]). The QqLIT has been commercialized by AB Sciex as their Q-Trap series.

As with the linear quadrupole before, the potential $\Phi_{(x,y,z,t)}$ in the two-dimensional quadrupole field of the LIT is expressed by a DC voltage U and an RF drive voltage V with the frequency Ω [129, 138] and Chap. 5 in [139])

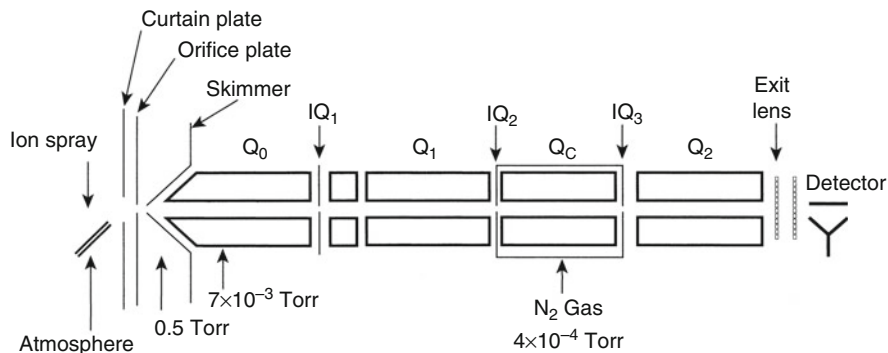


Fig. 4.46 A quadrupole-LIT hybrid instrument. In this scheme, the RF-only collision quadrupole has been replaced by the LIT. The other option, replacement of Q2 by a LIT, is finally in commercial use (Adapted from Ref. [129] with permission. © John Wiley & Sons, Ltd., 2002)

$$\Phi_{(x,y,z,t)} = (U - V \cos \Omega t) \frac{(x^2 - y^2)}{r_0^2} \quad (4.23)$$

from which the equations of motion can be derived. Assuming singly charged ions, i.e., $q = e$, we have

$$\begin{aligned} \frac{d^2x}{dt^2} + \frac{e}{m_i r_0^2} (U - V \cos \Omega t)x &= 0 \\ \frac{d^2y}{dt^2} - \frac{e}{m_i r_0^2} (U - V \cos \Omega t)y &= 0 \\ \frac{d^2z}{dt^2} &= 0 \end{aligned} \quad (4.24)$$

where m_i is the mass of the ion, r_0 is the distance between the central axis of the LIT and the surface of the rod. At least, these relationships hold valid as long as ions are sufficiently distant to the fringing fields at the end of the rods.

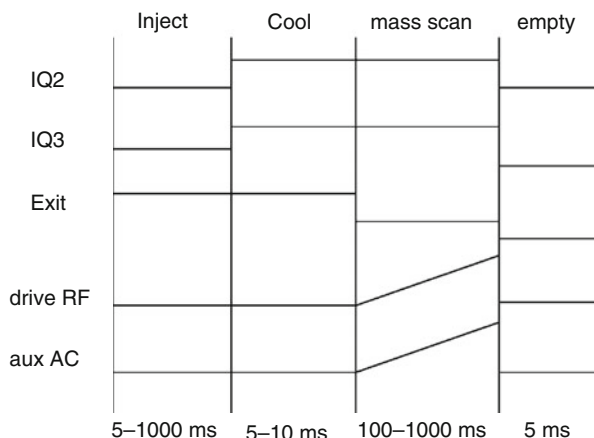
In practice, there is no DC component, and thus, only the Mathieu parameter q is required, which is obtained by solving the above equations

$$q_x = \frac{4eV}{m_i r_0^2 \Omega^2} \quad (4.25)$$

The voltage V is the zero-to-peak amplitude of the RF drive voltage. For an ion inside the quadrupole field the fundamental resonant frequency ω_n is obtained as

$$\omega_n = (2n + \beta) \left(\frac{\Omega}{2} \right) \quad (4.26)$$

Fig. 4.47 Scan function as used in the QqLIT instrument. IQ2, IQ3, and Exit belong to the trapping plates and the exit lens. Vertical displacements of lines indicate changes of the respective voltages. Note that the time slices are not to scale and that the duration of ion accumulation and mass scan may vary substantially (Adapted from Ref. [129] with permission. © John Wiley & Sons, Ltd., 2002)



For $n = 0$ Eq. (4.26) simplifies to become

$$\omega = \frac{\beta\Omega}{2} \quad (4.26a)$$

which for $q_x < 0.4$ can be approximated by the relationship

$$\omega \approx \frac{q_x}{\sqrt{8}}\Omega \quad (4.27)$$

The stability diagram for the LIT is analogous to that of the linear quadrupole (Figs. 4.32 and 4.33). While a description of the scanning of the LIT to achieve mass-selective axial ejection requires complex mathematics [138] far beyond the scope of this book, the practical application of LIT can easier be understood.

The scan function of such an instrument can be displayed in four time slices comprising:

1. ion injection until enough ions are accumulated,
2. trapping and thermalization,
3. mass scan by linear alteration of RF drive and auxiliary AC voltage,
4. a short blanking pulse to reset the LIT prior to the next scan cycle (Fig. 4.47).

Combination of two analyzer concepts

The QqLIT setup combines into one single instrument different types of mass analyzers, a scanning linear quadrupole, and a scanning linear quadrupole ion trap all connected via an RF-only ion guide. Instruments combining different types of mass analyzers are termed *hybrid instruments*. Most modern mass spectrometers are assembled from different elements to achieve optimum capabilities in the sense of creating instruments uniting the best of two worlds [133]. An overview of hybrids is presented at the end of the analyzer section.

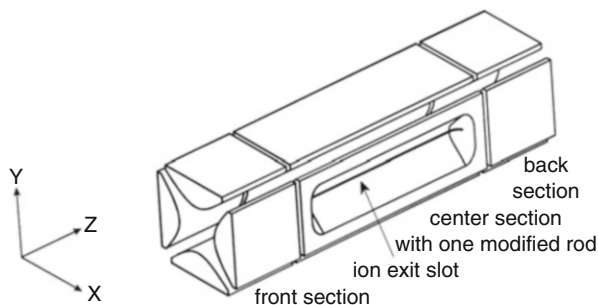


Fig. 4.48 A segmented linear quadrupole ion trap with mass-selective radial ejection capability. Applying higher potential to the front and back sections creates an axial trapping potential for ions in the center section. Radial trapping is again provided by the RF quadrupolar field. Ions are exiting through the slot in one of the four rods. The commercial design offers doubled sensitivity by using two detectors at opposite rods (Adapted from Ref. [130] by permission. © Elsevier Science, 2002)

4.5.3 Mass-Analyzing Linear Ion Trap with Radial Ejection

A scanning LIT [130] can alternatively be realized using a mass-selective radial ejection mode of operation. Such a LIT can either serve as a stand-alone mass analyzer (Thermo Scientific LTQ™ series) or can be combined into a hybrid LIT-FT-ICR instrument (Thermo Scientific LTQ-FT™ series). In the LTQ-FT instruments, the LIT shields the ultrahigh vacuum of the FT-ICR from collision gas and decomposition products in order to operate under optimum conditions. More importantly from the analytical point of view, the LIT can accumulate, mass-select and fragment selected ions prior to the next FT-ICR cycle while the ICR cell is still busy with the previous ion package (FT-ICR cf. Sect. 4.7). By using an Orbitrap analyzer (Sect. 4.8) in place of the FT-ICR cell, the same company offers the Thermo Scientific LTQ-Orbitrap™ series as an economical nonetheless powerful alternative to their LTQ-FT.

The LIT is composed of a quadrupole with hyperbolic rods that is cut into three segments of 12 mm in length for both trapping sections and 37 mm in length for the ion storage compartment (Fig. 4.48) [130]. The segmented design avoids fringing fields from the trapping plates as obvious from the electric field calculations using the SIMION software package (Fig. 4.49) [142, 143]. Although necessary for the axial ejection scan mode discussed in the preceding section, the radial excitation scanning requires the absence of fringing fields in the trapping zone. One pair of opposite storage compartment rods has cut a slit of 0.25 mm width and 30 mm length to allow for radial ejection of ions onto a conversion dynode. The conversion dynode is held at -15 kV (for positive-ion operation), and upon ion impact it delivers secondary electrons to an electron multiplier. In the commercial variant of the instrument, two detectors are in use to double the sensitivity of the device. The field inhomogeneity introduced by cutting slits into the rods is counterbalanced by

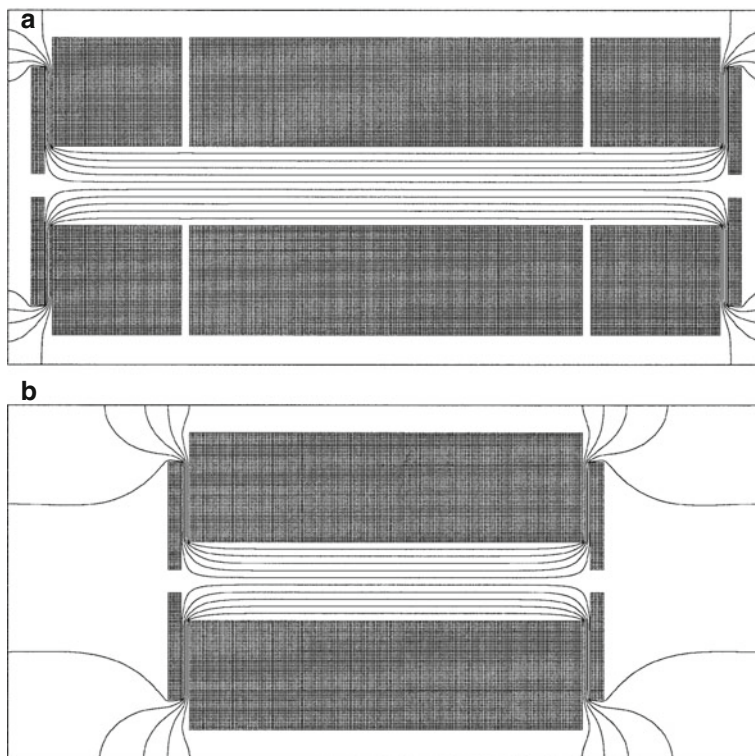


Fig. 4.49 SIMION simulation of the resonance excitation field comparing (a) a three-section ion trap and (b) a single-section device with end plates for trapping. In (a) the field inside the trapping compartment remains unperturbed from fringing fields (Adapted with permission from Ref. [130]. © Elsevier Science Publishers, 2002)

aligning them slightly outward from their theoretical x -position [130]. To operate as an m/z analyzer, the assembly of rods needs (i) a DC voltage supply to create the axial trapping field (z -coordinate), (ii) an RF voltage supply (1 MHz, ± 5 kV rod to ground) to deliver the radial quadrupolar trapping field (x,y -plane), and (iii) two phases of supplemental AC voltage (5–500 kHz, ± 80 V) that is applied across the x -rods for ion isolation, activation, and mass-selective ejection.

4.5.4 Constructing an Instrument Around the LIT

It takes more than just a nicely working m/z analyzer to put together an instrument suitable for real-world use and commercial success. Thus, the elaboration in this

short paragraph presents an example of what is relevant for any type of mass spectrometer.

To build a useful mass spectrometer, the above LIT is connected to an electrospray ionization (ESI, Chap. 12) source using RF-only ion guides to bridge the distance from the source orifice to the entrance of the LIT. As the ESI process starts at atmospheric pressure, the incipient ions need to be continuously transferred from outside the mass spectrometer into the high vacuum of the m/z analyzer. This can be achieved by so-called *differential pumping* (Sect. 4.13). Differential pumping makes use of the fact that macroscopic flow is only sustained as long as the mean free path of a molecule is shorter than the average dimension of the aperture it has to pass or of the vessel where it is contained. In practice, a powerful rotary pump ($30 \text{ m}^3 \text{ h}^{-1}$) maintains a pressure in the order of 1 mbar behind a 0.4–0.5 mm orifice. The next stages of the differentially pumped system are usually pumped by turbomolecular pumps. In modern instruments one split-flow turbomolecular pump often serves for both ports. In case of the LIT instrument the intermediate region is thus evacuated to about 2×10^{-3} mbar and the LIT itself to 2.6×10^{-5} mbar (Fig. 4.50).

The resulting mass spectrometer is able to deliver unit resolution over an m/z 150–2000 range at about 3 scans per second (Fig. 4.51) and even to provide higher resolution at lower scan rates ([130, 144] and Chap. 5 in [139]).

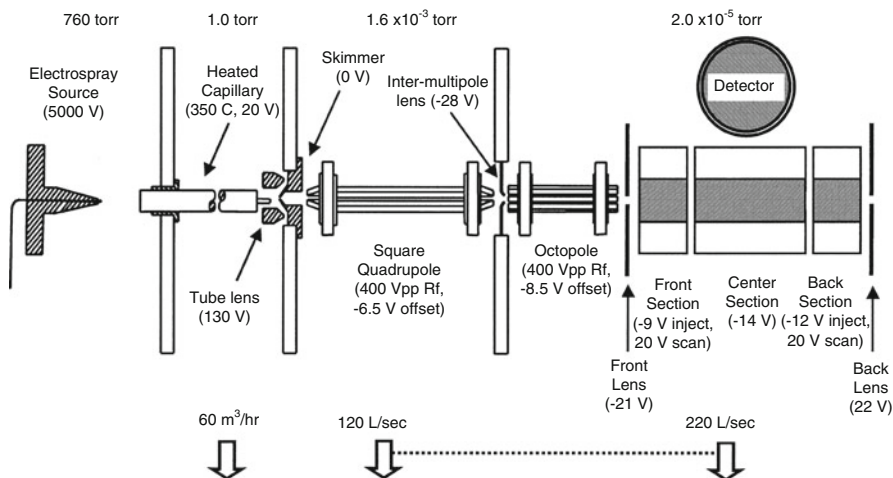


Fig. 4.50 Radial ejection LIT mass spectrometer with ESI source, more precisely the Thermo Fisher LTQ as of 2002. A square RF quadrupole is used to bridge the second pumping stage while an RF octopole like the one shown in Fig. 4.40 is used in the third pumping state. Typical operating voltages and pressures are given (Reprinted with permission from Ref. [130]. © Elsevier Science Publishers, 2002)

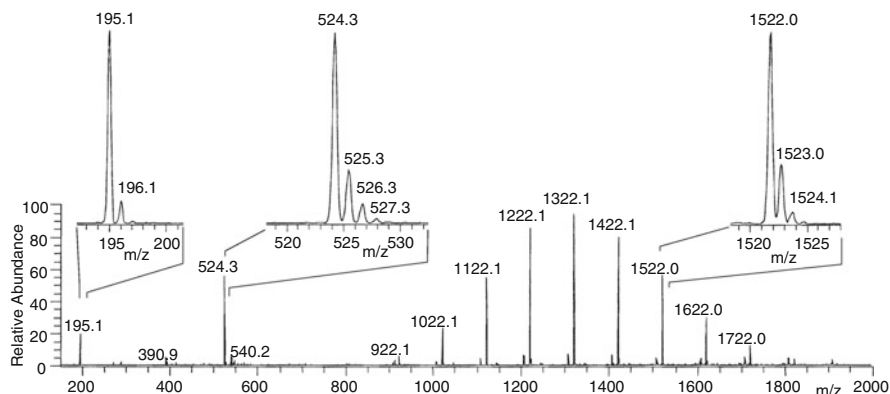


Fig. 4.51 Full scan mass spectrum of a calibration mixture containing caffeine, $[M + H]^+$ at m/z 195, the peptide MRFA, $[M + H]^+$ at m/z 524, and Ultramark 1621 yielding a series of ions from m/z 922 to 1722. The expanded views of selected signals show unit resolution, i.e., uniform resolution over the whole range (Adapted with permission from Ref. [130]. © Elsevier Science Publishers, 2002)

Just a reminder As already pointed out at the end of the linear quadrupole section, a summary of all RF quadrupole devices will be given in Sect. 4.6.12.

4.6 Ion Trap with Three-Dimensional Quadrupole Field

4.6.1 Introduction

In contrast to the linear two-dimensional quadrupole field of the LIT, the *quadrupole ion trap* (QIT) originally developed by Wolfgang Paul creates a three-dimensional RF quadrupole field of rotational symmetry to store ions within defined boundaries. The invention of the QIT goes back to 1953 [101–103]; however, it took until the mid-1980s to access the full analytical potential of quadrupole ion traps [139, 145–149].

Naming

Wolfgang Paul himself preferred to call the device “*Ionenkäfig*” (ion cage) because it does not actively act to catch ions from the outside. The acronym QUISTOR derived from *quadrupole ion store* was also in use for a while. To be precise, we would have to call it *ion trap with three-dimensional quadrupole field*, as used in the title of this section. Rather than insisting on this lengthy term we will be using the commonly accepted term *quadrupole ion trap* (QIT).

The first commercial quadrupole ion traps were incorporated in GC-MS benchtop instruments in the late 1980s (Finnigan MAT ITD and ITMS). Electron ionization was effected inside the trap by admitting the GC effluent and a beam of electrons directly into the storage volume of the trap. Later, external ion sources became available, and soon a large number of ionization methods could be fitted to the QIT analyzer [150–152]. Modern QITs cover ranges up to about m/z 3000 with fast scanning at unit resolution, and in addition, offer “zoom scans” over smaller m/z ranges at higher resolution; instruments delivering resolving power up to 5-fold unit resolution are commercially available. Accurate mass measurements with QITs were expected [148] but not realized so far. The tandem-in-time capabilities of QITs can be employed to conveniently perform MSⁿ experiments [146, 147], and their compact size is ideal for field applications [16].

Historical versus didactical

Historically, both the linear quadrupole analyzer and the quadrupole ion trap originate from the early 1950s (even from the same inventor), whereas the scanning linear ion trap is a design of the 1990s. A detailed timeline of the development of quadrupole ion traps can be found in the comprehensive monographs by March and Todd [139, 145]. However, from a teaching perspective, it appears advisable to align the explanations in the logical order as presented here. Once the concepts of trapping and mass-selective release from a quadrupole ion trap have been understood, the step from linear to rotational symmetry should be comparatively easy.

4.6.2 Principle of the Quadrupole Ion Trap

The *quadrupole ion trap* (QIT) consists of two hyperbolic electrodes serving as end caps along with a ring electrode that replaces two of the linear quadrupole rods, i.e., it could theoretically be obtained by rotating the axial cross section of a linear quadrupole with hyperbolic rods by 360° around an axis that traverses the apices of two opposed rods (Figs. 4.52 and 4.53). Thus, a section through the rz -plane of the QIT closely resembles that of the entrance of a linear quadrupole with hyperbolic rods (cf. Figs. 4.30 and 4.37) [105, 150]. However, the angle between the asymptotes enclosing the ring electrode is 70.5° ($2 \times \arctan(1/\sqrt{2})$) instead of 90°. The end caps are electrically connected and the DC and RF potentials are applied between them and the ring electrode. The working principle of the QIT is based on creating stable trajectories for ions of a certain m/z or m/z range while removing unwanted ions by letting them collide with the walls or by axial ejection from the trap due to their unstable trajectories [139, 145, 149].

For the QIT, the electric field has to be considered in three dimensions. Let the potential Φ_0 be applied to the ring electrode while the hyperbolic end caps are grounded. The axial coordinate of the trap is designated as the z -axis, the value z_0

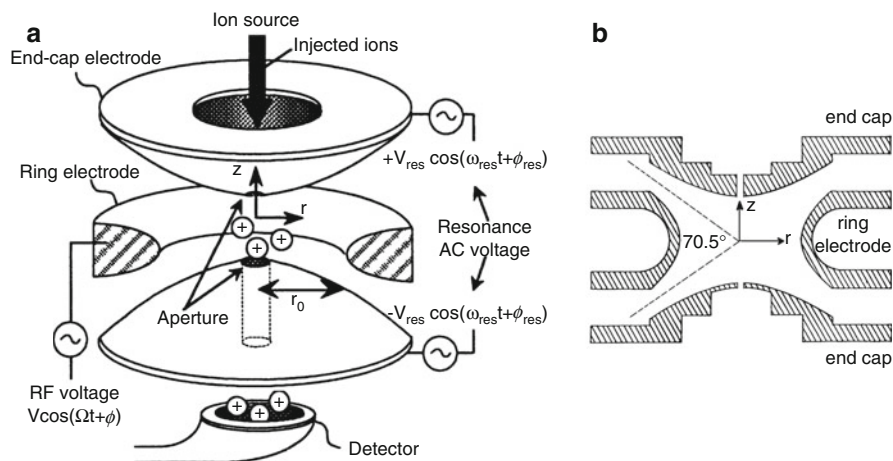


Fig. 4.52 A quadrupole ion trap. (a) QIT with external ion source (illustration stretched in z -direction) and (b) section in the rz -plane (in scale). (a) (Reproduced from Ref. [153] by permission. © John Wiley & Sons, 2000)

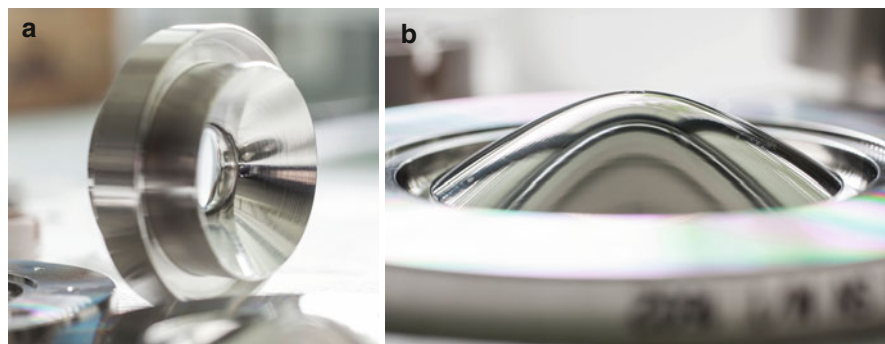


Fig. 4.53 Electrodes of the Finnigan LCQ quadrupole ion trap analyzer. (a) Ring electrode with symmetrical hyperbolic cross section of the inner walls of the ring. (b) One of the pair of hyperbolic end electrodes

defines the physical dimension of the trap (center to cap), and z presents the actual position of an ion with respect to the z -axis. The x,y -plane is resolved into the cell radius r_0 where r analogously defines the actual radial position of an ion. With the pair of end caps grounded the potential inside the trap is given as

$$\Phi_0 = U + V \cos \Omega t \quad (4.28)$$

Then, the field can be described in cylindrical coordinates (using the standard transformations $x = r \cos \theta$, $y = r \sin \theta$, and $z = z$) by the expression [145, 150]

$$\Phi_{x,y,z} = \frac{\Phi_0}{r_0^2} (r^2 \cos^2 \theta + r^2 \sin^2 \theta - 2z^2) \quad (4.29)$$

Because of $\cos^2 + \sin^2 = 1$ this reduces to

$$\Phi_{r,z} = \frac{\Phi_0}{r_0^2} (r^2 - 2z^2) \quad (4.30)$$

The equations of motion of a singly charged ion of $q = e$ in such a field are

$$\begin{aligned} \frac{d^2 z}{dt^2} - \frac{4e}{m_i(r_0^2 + 2z_0^2)} (U - V \cos \Omega t) z &= 0 \\ \frac{d^2 r}{dt^2} + \frac{2e}{m_i(r_0^2 + 2z_0^2)} (U - V \cos \Omega t) r &= 0 \end{aligned} \quad (4.31)$$

Solving these differential equations which are again of the Mathieu type, finally yields the parameters a_z and q_z

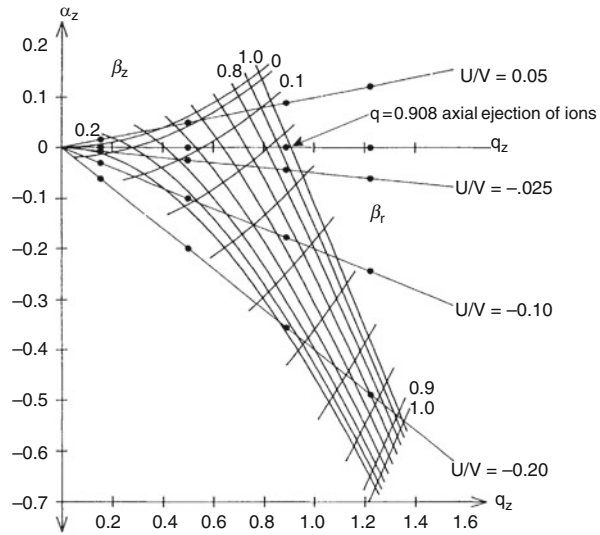
$$\begin{aligned} a_z &= -2a_r = -\frac{16eU}{m_i(r_0^2 + 2z_0^2) \Omega^2} \\ q_z &= -2q_r = \frac{8eV}{m_i(r_0^2 + 2z_0^2) \Omega^2} \end{aligned} \quad (4.32)$$

where $\Omega = 2\pi f$ and f is the fundamental RF frequency of the trap (≈ 1 MHz). To remain stored in the QIT, an ion has to be simultaneously stable in the r and z directions. The occurrence of stable ion trajectories is determined by the stability parameters β_r and β_z which depend on the parameters a and q . The borders of the first stability region are defined by $0 < \beta_r, \beta_z < 1$ [154].

A stability diagram can be drawn where the stability region closest to its origin is of greatest importance for the operation of the QIT (Fig. 4.54). At a given U/V ratio, ions of different m/z are located along a straight line crossing the stability region; ions of higher m/z are nearer to the origin than lighter ones. The regions of stability as plotted in the a/q plane are represented as envelopes of characteristic shape. Ions with their m/z value inside the boundaries are stored in the QIT. The low-mass limit of the trapped m/z range is strictly defined by $q_z = 0.908$.

Collisional cooling (Sect. 4.4.4) by several tens of soft collisions during the dwell time of the ions inside the QIT significantly enhances its resolving power and sensitivity [155, 156]. The light buffer gas, normally helium at 0.1 Pa, serves to dampen the ion motion towards the center of the trap, and thus, keeps them away from the electrode surfaces and from field inhomogeneities as induced by the entrance and exit holes of the QIT [157].

Fig. 4.54 Stability diagram for the quadrupole ion trap. The points collected on a common line mark the a/q values of a set of ions. Each line results from different settings of the U/V ratio (Reproduced from Ref. [145] by permission. © John Wiley and Sons, 1989)



4.6.3 Visualization of Ion Motion in the Ion Trap

The way the three-dimensional quadrupole field acts to keep ions within a certain volume, i.e., within a potential well some electron volts in depth, can be illustrated by a mechanical analog: A ball can be prevented from rolling from a saddle by rotating the saddle just right to bring the ball back to the middle before it can leave the surface via one of the steeply falling sides (Fig. 4.55a). Paul demonstrated the dynamic stabilization of up to three steel balls by such a device in his Nobel lecture [101, 102].

The trajectories of low-mass ions in a QIT were shown to be similar to those observed for charged aluminum dust particles [158–161]. Wuerker recorded Lissajous trajectories, superimposed by the RF drive frequency, as a photomicrograph (Fig. 4.55b) [158]. The complex motion of the ions is the result of the two super-imposed secular oscillations in r and z direction. Calculations of the trajectories yield the same results [162].

4.6.4 Mass-Selective Stability Mode

The whole range of ions is generated within or admitted to the QIT, but solely ions of one particular m/z are trapped at a time by setting appropriate parameters of the QIT. Then, the stored ions are pulsed out of the storage volume by applying a negative pulse to one of the end caps [163, 164]. Thus, they hit the detector located behind an opening in the center of one of the end caps. A full-scan mass spectrum is obtained by addition of several hundred single steps, one for each nominal m/z value. This is the so-called *mass-selective stability mode* of the QIT [165, 166]. The mass-selective stability mode is no longer in use, because it is too slow and provides poor sensitivity as most ions are wasted.

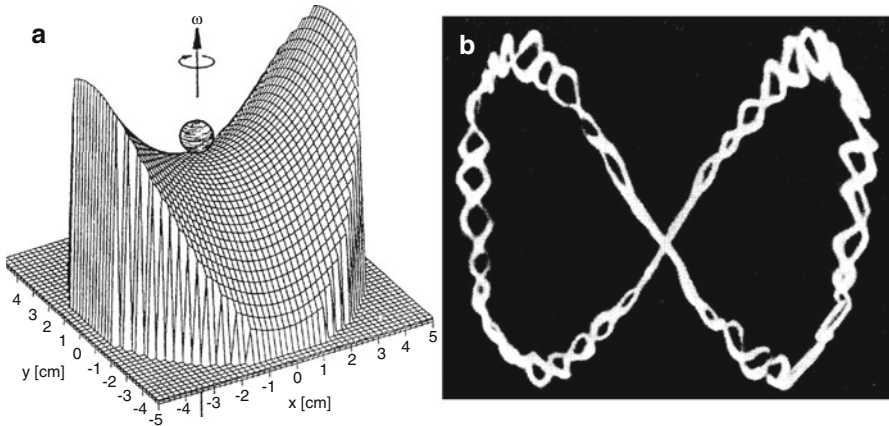


Fig. 4.55 Visualization of ion motion in the ion trap. (a) Mechanical analog of the QIT. (b) Photograph of ion trajectories of charged aluminum particles in a quadrupole ion trap ((a) Reproduced from Ref. [102] with permission. © World Scientific Publishing, 1993. (b) Reproduced from Ref. [158] with permission. © American Institute of Physics, 1959)

4.6.5 Mass-Selective Instability Mode

First, the full m/z range of interest is trapped within the QIT. The trapped ions may either be created inside the QIT or externally. Then, with the end caps grounded an RF-voltage scan (V) is applied to the ring electrode causing consecutive ejection of ions in the order of their m/z values. This is known as *mass-selective instability (ejection)* mode [155, 167]. It can be represented in the stability diagram by a horizontal line from the origin to the point of axial ejection at $q_z = 0.908$. The timing sequence is shown in Fig. 4.56 While easy to understand, this mode is also no longer relevant in QIT operation.

4.6.6 Resonant Ejection

Another technique to operate a QITs employs the effects of *resonant ejection* to remove ions of successively increasing m/z value from the storage volume, i.e., to achieve a scan. In an ideal QIT, the motions of the ions in radial and axial directions are mutually independent. Their oscillations can be described by a radial and an axial secular frequency, each of them being a function of the Mathieu trapping parameters a and q . If a supplementary RF voltage which matches the axial secular frequency is applied to the end caps, resonant ejection of ions occurs at $q < 0.908$ (Fig. 4.54) [168]. Excitation occurs when the frequency of a supplementary RF signal matches the secular frequency of a trapped ion in z direction. The secular frequency components in axial direction (ω_z) are given by $\omega_z = (n + \beta_z/2)\Omega$, where Ω represents the angular frequency, n is an integer, and β_z is determined by the working point of an ion within the stability diagram [169]. In the special case when

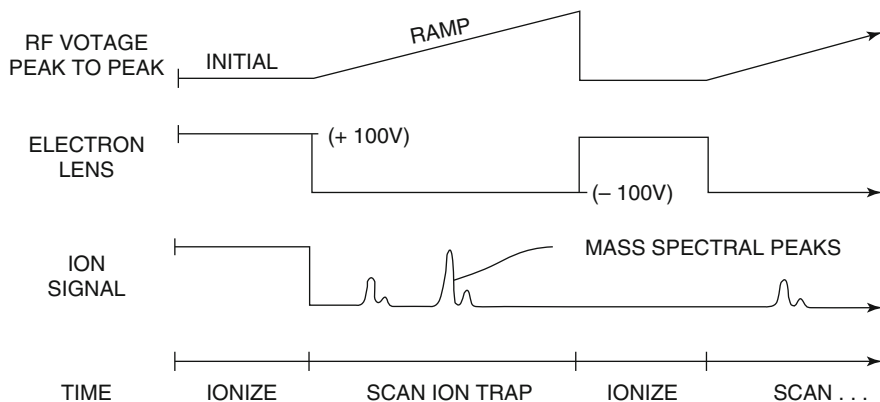


Fig. 4.56 Timing sequence used for mass-selective instability mode (about 1.5 cycles shown). With an external ion source the ionization time is replaced by the ion injection pulse (Reproduced from Ref. [155] by permission. © Elsevier Science, 1984)

$\beta_z = 1$ and $n = 0$, the fundamental secular frequency is exactly half of the RF drive frequency applied between ring electrode and end caps.

Scanning by Resonant Ejection To effect resonant ejection for the set of $\beta_z = 0.5$ and $n = 0$ we have $\omega_z = (0 + 0.5/2) = 0.25\Omega$, i.e., $1/4$ of the RF drive frequency has to be applied to eject ions at the $\beta_z = 0.5$ borderline. By scanning the voltage of the RF drive frequency upwards, ions of increasing m/z ratio are successively ejected.

Scans based on resonant ejection may either be carried out in a forward, i.e., from low to high mass, or a reverse direction. However, the scan direction has significant influence on the attainable resolving power, the reverse direction being clearly inferior in that respect. [170, 171] The combination of forward and reverse scanning allows for the selective storage of ions of a certain m/z value by elimination of ions below and above that m/z value from the trap. Thus, it can serve for precursor ion selection in tandem MS experiments [168, 170]. Axial excitation can also be used to cause collision-induced dissociation (CID) of the ions as a result of collisions with the helium buffer gas [155, 168]. A substantial increase of the mass range is realized by reduction of both the RF frequency of the modulation voltage and the physical size of the QIT [166, 172, 173].

4.6.7 Axial Modulation and Control of the Ion Population

Ion trapping devices are sensitive to overload because of the detrimental effects of Coulombic repulsion on the ion trajectories. The maximum number of ions that can be stored in a QIT is about 10^6 – 10^7 , but it reduces to about 10^3 – 10^4 if unit mass resolution in an RF scan is desired. *Axial modulation*, a subtype of resonant ejection, allows to increase the number of ions stored in the QIT by one order of

magnitude while maintaining unit mass resolution [173, 174]. During the RF scan, the modulation voltage with a fixed amplitude and frequency is applied between the end caps. Its frequency is chosen slightly below $1/2$ of the fundamental RF frequency, because for $\beta_z \leq 1$, e.g., $\beta_z = 0.98$, we have $\Omega_z = (0 + 0.98/2) \times \Omega = 0.49 \times \Omega$. At the stability boundary, ion motion is in resonance with this modulation voltage, and thus ion ejection is facilitated. Axial modulation basically improves the mass-selective instability mode of operation.

If resolving power is not a major concern, scanning of QITs can be very fast, a property that can be employed to make a *pre-scan*. The actual ion current into the trap is then determined from the pre-scan and the result is used to adjust the number of ions admitted to the QIT by a timed ion gate for the subsequent analytical scan. Thus, the number of ions, and hence, charge density inside the QIT are continuously held close to the optimum. This tool to control the ion population of the QIT has been introduced by Finnigan and referred to as *automatic gain control* (AGC) [146, 175]. AGC gives increased sensitivity at low sample flow and avoids overload of the QIT at high sample flow.

Importance of the ion population in traps

Careful control of the ion population, e.g., as implemented by AGC, is not only relevant for QITs but also for all other types of ion traps. The technique is implemented in LITs that are employed as stand-alone devices and also in LITs serving for ion selection and dosing into FT-ICR or Orbitrap analyzers (Sects. 4.7, 4.8, and 4.9).

Provided sufficiently high scan rates are also available whilst resolution is preserved, the pre-scan can be omitted. Instead, a trend analysis based on a set of two or three preceding analytical scans can be performed. This procedure avoids wasting of ions and results in further optimization of the filling level of the QIT. The exploitation of the phenomenon of nonlinear resonances turned out to be of key importance for the realization of this method.

Tandem MS in a QIT Tandem mass spectrometric experiments in quadrupole ion traps (more in Sect. 9.8) are performed by combining the techniques of resonant ejection, and forward and reverse scanning to achieve an optimum in precursor ion selection, ion activation, and fragment ion scanning (Fig. 4.57) [168].

4.6.8 Nonlinear Resonances

Higher multipole fields, in particular octopole fields, are induced in any real ion trap by deviations from the ideal electrode structure. The trapping potential may then be represented as a sum of an ideal quadrupole field and weak higher order field

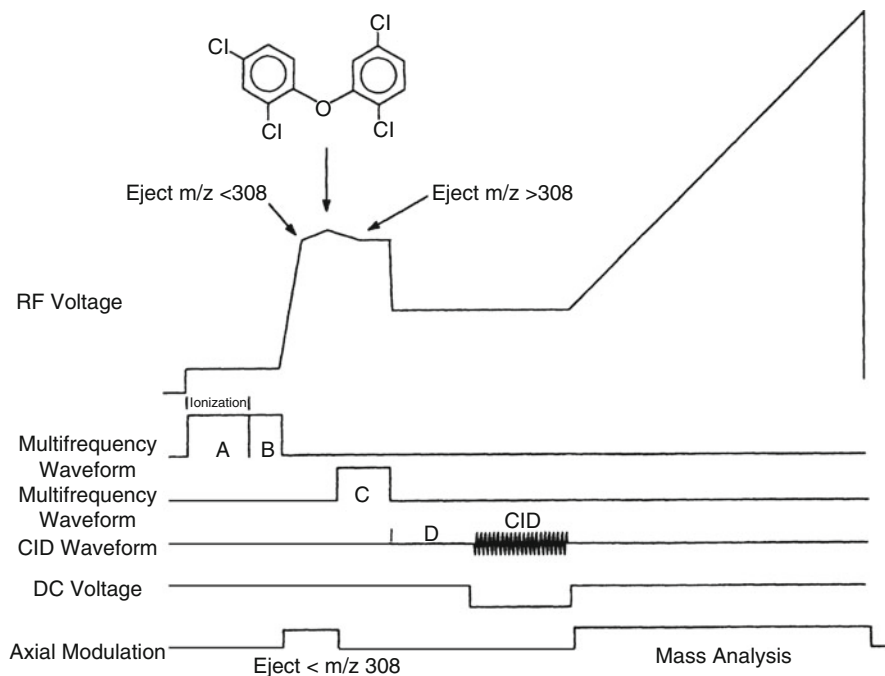


Fig. 4.57 Complex scan function used for a tandem mass spectrometric study of 2,4,3',6'-tetrachlorodiphenylether (Reproduced from Ref. [168] by permission. © John Wiley and Sons, 1997)

contributions [154, 176, 177]. Application of an excitation voltage across the end caps induces dipole and hexapole fields in addition. Those higher order fields in the QIT may have beneficial effects such as increase in mass resolution in the resonant ejection mode, but may also result in losses of ions due to nonlinear resonances [178]. Nonlinear resonances have been known for long [179, 180], but useful theoretical descriptions were only recently developed [154, 177, 181, 182]. The condition for the appearance of instabilities is related to certain frequencies through the stability parameters β_r and β_z and the integer multiples n_r and n_z . The locations of instability spread like a net over the stability diagram and have been experimentally verified with astonishing accuracy (Fig. 4.58) [154]. Excitation of ions with a suitable frequency can cause their fast ejection from the trap due to the sudden shift to nonlinear stability. Nonlinear resonances can thus be exploited to realize very fast scans of the QIT ($26,000 \text{ u s}^{-1}$) while maintaining good resolving power [182], e.g., irradiation of $0.33 \times \Omega$ amplifies hexapole resonances and causes sudden ejection at the $\beta_z = 0.66$ borderline.

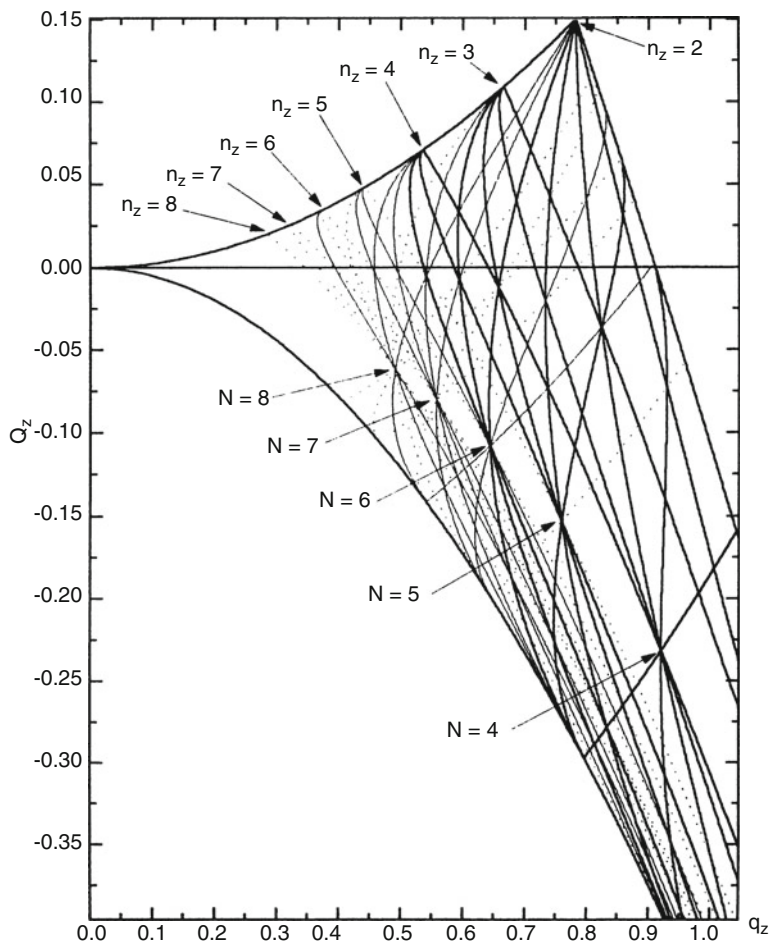


Fig. 4.58 Plot of theoretical lines of instability corresponding to the relation $n_r/2\beta_r + n_z/2\beta_z = 1$ for different orders $N = n_r + n_z$ (strong resonances represented by *solid lines*, weak ones by *dotted lines*) (Reproduced from Ref. [154] by permission. © Elsevier Science, 1996)

4.6.9 Miniaturization and Simplification of Ion Traps

The fabrication of quadrupole mass analyzers of any design necessitates high precision in machining and alignment of the electrodes; the production of hyperbolic electrode surfaces is especially challenging. While quadrupoles are compact, for mobile applications, even smaller and preferably less expensive analyzers are desirable [15, 183, 184]. Additionally, mobile instruments should have reduced vacuum requirements as the generation of high vacuum demands for comparatively heavy and energy-consuming pumps.

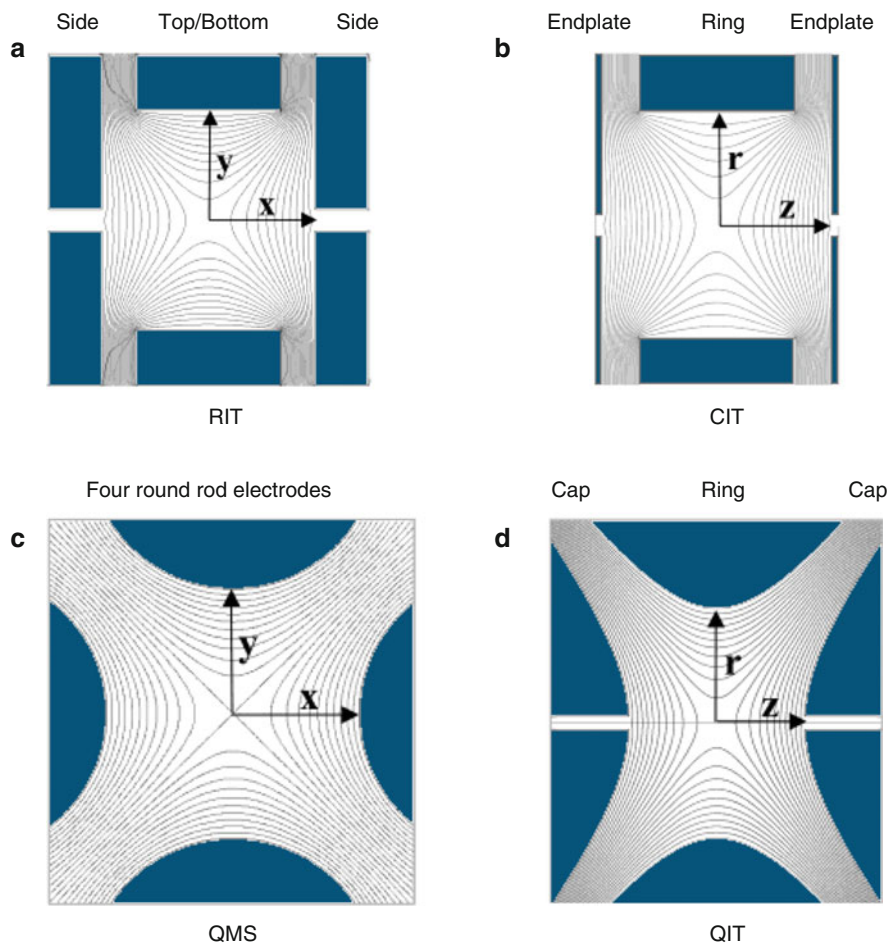


Fig. 4.59 Calculated trapping fields for (a) a rectilinear ion trap, (b) a cylindrical ion trap with planar endplates, (c) a quadrupole mass filter with round rods, and (d) a quadrupole ion trap with hyperbolic electrodes (Paul trap). Analyzer views (a) and (c) are end-on, (b) and (d) side-on (Adapted from Ref. [185] with permission. © American Chemical Society, 2004)

It turns out that the electrode geometries of LITs and QITs can largely be simplified without sacrificing too much of their performance. Thus, a *rectilinear ion trap* (RIT) can be constructed that has flat rectangular-shaped electrodes, one pair (top and bottom) being smaller than the other (side walls with slits for ion ejection, Fig. 4.59) [185, 186]. Also the geometry of the Paul trap can be transformed into a simple *cylindrical ion trap* (CIT) built of two planar endplates and a cylindrical ring electrode. Such simplified electrode shapes also allow for

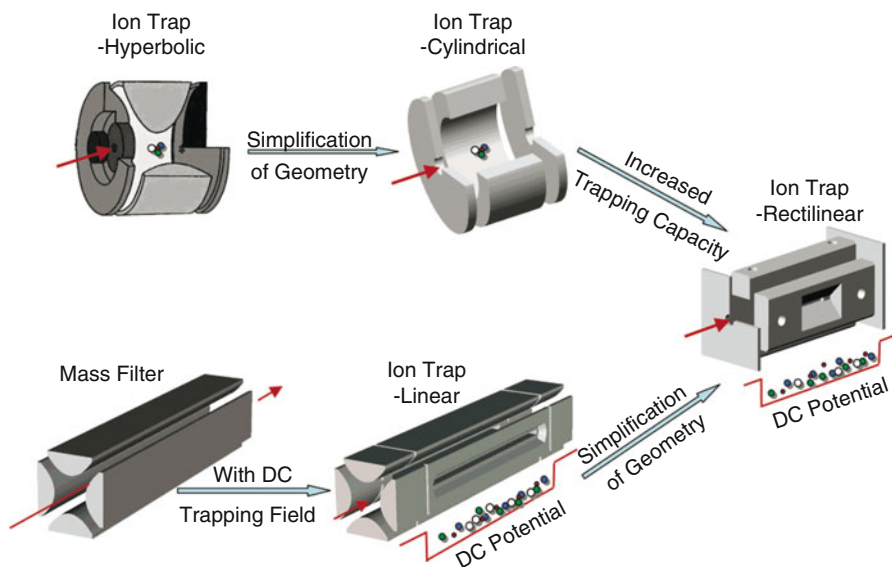


Fig. 4.60 Conceptual evolution of the rectilinear ion trap and interrelationship to other types of ion traps (Reproduced from Ref. [185] with permission. © American Chemical Society, 2004)

more compact traps to be built. The smaller dimensions then result in shorter ion paths, and thus, shorter mean free paths (poorer vacuum) can easily be tolerated. In turn, this allows vacuum generation to be performed by a single stage.

The evolution of ion traps and subsequent combination of characteristics of two “parent lines” that led to the construction of a RIT has instructively been illustrated in a paper by Ouyang et al. (Fig. 4.60) [185].

4.6.10 Digital Waveform Quadrupole Ion Trap

In almost all QITs, the m/z range is extended by lowering the RF drive frequency and/or by resonant ejection at a low q value, e.g., Thermo Fisher Scientific QITs eject the ions at $q = 0.78$ – 0.80 rather than the classical $q = 0.908$. Alternatively to a scan of the drive voltage at constant RF, a frequency scan at constant voltage can be applied to realize scans over an extended m/z range of up to about m/z 20,000. This demands a waveform generator coupled with a power amplifier, which is associated with excessive power consumption and difficulties in obtaining a high voltage output without waveform distortion [171].

The concept of the *digital ion trap* (DIT) makes use of a digital waveform to trap the ions. In this context, the terms *digital ion trap* and *digital waveform* describe a waveform composed of simple rectangular pulses applied to the ring electrode [171, 187]. In practice, a switching circuit is used to generate a pulsed waveform by rapid alternation between discrete DC high-voltage levels (± 250 to ± 1000 V).

The digital mode of pulse generation affords precise control of the timing. Furthermore, the AC excitation voltage connected across the end-cap electrodes can be delivered by the same digital circuitry. Interestingly, the ion motion under the influence of a digital waveform may still be expressed in terms of the conventional Mathieu parameters [171, 187, 188].

The development of the DIT has been pursued by Shimadzu and has reached a quite impressive level. Recently, an array of DITs, termed *ion trap array* (ITA), has been developed allowing multiple steps of isolation, activation, or scanning in parallel [189].

4.6.11 External Ion Sources for the Quadrupole Ion Trap

Chemical ionization (CI) mass spectra were first obtained by using the mass-selective instability mode of the QIT [166, 167, 190]. The reagent gas was admitted into the QIT, ionized and then allowed to react with the analyte.

With external ion sources it became feasible to interface any ionization method to the QIT mass analyzer [191]. However, commercial QITs are chiefly offered for two fields of applications: (i) GC-MS systems with EI and CI, because they are either inexpensive or capable of MS/MS to improve selectivity of the analysis (Chap. 14); and (ii) instruments equipped with atmospheric pressure ionization (API) methods (Chaps. 12 and 13) offering higher mass range, and some fivefold unit resolution to resolve isotopic patterns of multiply charged ions (Fig. 4.61) [161, 175, 192, 193].

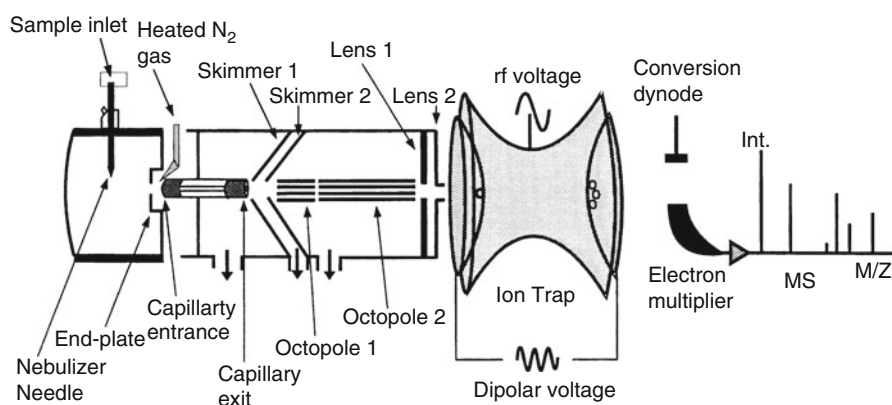


Fig. 4.61 Layout of a quadrupole ion trap instrument equipped with an external ESI ion source. The analogy to the ESI-LIT configuration shown in Fig. 4.50 is striking (Reproduced from Ref. [193] by permission. © John Wiley & Sons, 2000)

4.6.12 Ion Trap Maintenance

The confined volume of quadrupole ion traps and their mode of operation causes a large fraction of the ions to hit the electrodes thereby leading to contamination of their surfaces. Quadrupoles and quadrupole ion traps thus require occasional cleaning, which means that the entire analyzer needs to be disassembled and reassembled afterwards. The photograph in Fig. 4.62a shows the analyzer of a



Fig. 4.62 Analyzer maintenance of a QIT; here of the Finnigan LCQ. (a) Complete QIT analyzer mounted onto the top cover plate of the vacuum manifold, (b) after taking it apart for cleaning

Finnigan LCQ instrument after dismantling the entire unit from the instrument frame. Ions would enter from an ESI source on the right (not shown) and be passed across two stages of differential pumping by means of RF-only octopoles. Here, the second octopole also serves as a linear ion trap to dose ion packages into the QIT under AGC control. The polished electrode on the left below the exit endcap of the QIT is the entrance into the detector.

Figure 4.62b shows the analyzer components spread on a clean sheet of lint-free paper. After gentle cleaning with fine metal polish (only if there are permanent dark spots), water with detergent, distilled water, and finally solvent like methanol or isopropanol the parts are allowed to dry. Finally, the analyzer is reassembled, mounted into the vacuum manifold, and evacuated. About 1 h later, the QIT should be ready for performing the full tuning procedure to achieve restored performance.

Stay grounded

“Ion traps are also the only type of mass spectrometer that most users can disassemble and reassemble without sacrificing instrument performance.” [185].

4.6.13 Summary of RF Quadrupole Devices

Principle of Operation

In an electric radiofrequency (RF) quadrupole field, ions are forced to oscillate in the open space between the four electrodes creating this field. Suitable frequency and amplitude provided, this motion can be stable in that the ions never hit one of the electrodes and never escape through the gaps in between. RF quadrupoles can be mass-selective as these conditions are only met for ions of a selected m/z value or range of m/z values. The m/z range is adjusted by superimposition of an RF and a DC voltage. Mass-selective operation also requires that ions to be analyzed experience a sufficient number of oscillations or have sufficient dwell time within this field to eject ions outside the boundaries of stability due to their unstable trajectories.

Types of RF Quadrupole Devices

Linear quadrupoles (Q) are operated as mass filters, while linear RF-only multipoles (q, h, o) are used as ion guides and collision cells. In both cases, a beam of ions is passed through the device so that the duration of interaction is determined by the velocity of the ions and the length of the RF device (Q, q, o, h).

Linear quadrupole ion traps (LIT) as well as quadrupole ion traps with three-dimensional quadrupole fields (QIT) are marked by storing ions inside. They are more flexible as they can either serve to accumulate ions to provide ion packages for other analyzer stages or be run to mass analyze a package of ions. During the

period of ion storage, ions can also be activated by collisions with residual gas inside the LIT or QIT. Fragment ions arising thereof can be stored and mass-analyzed as well (Chap. 9).

General Characteristics

As Q, LIT, and QIT are purely driven by RF and DC voltages, operational parameters can be changed at very high rates, typically $>10,000 \text{ u s}^{-1}$. These analyzers are also very compact (neither requires a long flight tube nor for a heavy magnet), and thus, ideal for use in benchtop instruments. Q, LIT, and QIT are easy to handle and user-friendly. They are typically run at unit resolution but zoom scans to increase the resolving power across a narrow m/z window are sometimes enabled. None of these analyzers is adequate for accurate mass measurements.

Use in MS Instrumentation

Most manufacturers offer a variety of Q, LIT, and QIT instruments for use with the different kinds of ionization methods. The majority of stand-alone Q, LIT, and QIT instruments is used in routine gas chromatography (GC)- and liquid chromatography (LC)-mass spectrometry applications. Additionally, Q, LIT, and QIT devices are frequently incorporated into hybrid instruments to serve as the first of the two mass analyzers.

4.7 Fourier Transform Ion Cyclotron Resonance

4.7.1 From Ion Cyclotron Resonance to Mass Spectrometry

The development that led to modern *Fourier transform ion cyclotron resonance* (FT-ICR) mass spectrometers began in 1932 when E. O. Lawrence applied a transverse alternating electric field orthogonally to a magnetic field to build a particle accelerator [194, 195]. It was demonstrated that in *ion cyclotron resonance* (ICR) the angular frequency of the circular motion of ions is independent of the radius they are traveling on.

Later, this principle was applied to construct an ICR mass spectrometer [196, 197]. ICR mass spectrometers measuring the power absorption from the exciting oscillator were commercialized in the mid-1960s by Varian. Starting from their application to gas-phase ion chemistry [198], ICR instruments made their way into analytical mass spectrometry [199]. However, it was the introduction of FT-ICR in 1974 that initiated the major breakthrough [200, 201]. Ever since, the performance of FT-ICR instruments has steadily improved [202, 203] to reach unprecedented levels of resolving power and mass accuracy when superconducting magnets are employed [204–209]. The introduction of a dynamically harmonized ICR cell gave new thrust to the technique [210, 211]. Now, more than 40 years after FT-ICR-MS has been introduced [212], the technique can achieve resolving powers of up to 1.2×10^7 (12 million), and even a 21-Tesla superconducting magnet has

been constructed for FT-ICR-MS to obtain ultrahigh resolving power at high spectral acquisition rates and outstanding sensitivity [213].

FT-ICR analyzers are operated in a way that notably differs from what we have dealt with so far. FT-ICR-MS relies on nondestructive ion detection by registering image currents of circulating ions in the time domain. FT is applied to deliver frequency domain data that can then be converted into the intensity versus m/z data format. This may appear to be quite complex – and in fact, it is. So let's approach this issue step by step – FT-ICR-MS is well worth the extra effort.

Top-of-the line MS

Today's FT-ICR mass spectrometers offer ultrahigh resolving power ($R = 10^5$ to $>10^6$) [214–217] and highest mass accuracy ($\Delta m = 10^{-4}$ – 10^{-3} u, cf. Sects. 3.5 and 3.6) [208, 209], attomol detection limits (with nanoESI or MALDI sources), high mass range and MS^n capabilities [218]. Modern FT-ICR instruments actually represent some sort of hybrids with linear quadrupole or LIT front ends.

4.7.2 Ion Cyclotron Motion – Basics

As we know from the discussion of magnetic sectors, an ion of velocity v entering a uniform magnetic field B perpendicular to its direction will, by action of the Lorentz force (Sect. 4.3.2), immediately move on a circular path. Contemplating the path in the direction of the magnetic field reveals that negative ions circulate clockwise while positive ions move counterclockwise (Figs. 4.19 and 4.63).

The radius r_m of the ions' circular motion is determined by Eq. (4.13):

$$r_m = \frac{m_i v}{qB} \quad (4.13)$$

Upon substitution with $v = r_m \omega$ and rearrangement of the resulting term, *the cyclotron angular frequency* ω_c is obtained as:

$$\omega_c = \frac{qB}{m_i} \quad (4.33)$$

and by substituting with the cyclotron frequency ($f_c = \omega_c/2\pi$) Eq. (4.33) becomes

$$f_c = \frac{qB}{2\pi m_i} \quad (4.34)$$

One realizes that the cyclotron frequency is independent of the ions' initial velocity, but proportional to its charge and the magnetic field, and inversely proportional to its mass. Of any physical quantity, frequencies can be measured at

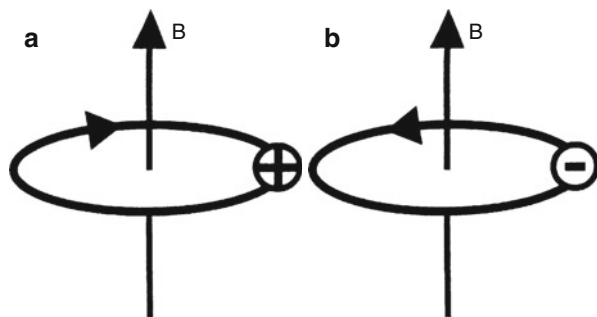


Fig. 4.63 Circular motion of ions in a magnetic field. Viewing along the direction of the magnetic field one observes (a) a counterclockwise motion for positive ions and (b) a clockwise motion for negative ions (Adapted from Ref. [219] with permission. © Elsevier Science Publishers, 2002)

the highest accuracy, and thus, cyclotron frequency measurements appear as ideal premises for building powerful m/z analyzers.

4.7.3 Cyclotron Motion: Excitation and Detection

Gaseous ions are not at rest but at least move arbitrarily at their thermal velocities. When such a package of thermal ions is generated within a magnetic field or is injected into it, the resulting small ion cloud contains ions that are all spinning at their respective cyclotron frequencies (circular micromotion) while the cloud as a whole remains stationary provided it has been brought to a halt within the field boundaries. Therefore, the magnetic field not only acts in an m/z -sensitive way by imposing the cyclotron motion on the ions, but also provides ion trapping in a plane perpendicular to its field lines (xy -plane, cf. action of the quadrupolar field in a LIT).

Upon excitation, the circular micromotion is superimposed by the macroscopic cyclotron motion of the whole ion cloud, i.e., the RF excitation field preserves the coherence of ion packages composed of ions of the same m/z value. As the initial kinetic energy of the ions is small as compared to the energy uptake from the RF field, it is of minor importance for the experiment [220]. Nonetheless, the complexity of the overall motion affects frequency-to-mass calibration if accurate results are required [221].

In practice, mass-selective excitation, so-called *resonant excitation*, is achieved by applying a transverse electric field alternating at the cyclotron frequency f_c ($\omega_c = 2\pi f_c$) to accelerate the ions. Such a field can be applied by a pair of RF electrodes placed on opposite sides of the orbit. As the ions accelerate, the radius of their orbit increases, and the resulting overall motion is a spiral (Fig. 4.64a) [195, 203]. For lighter ions, the spiral reaches the same radius with fewer cycles

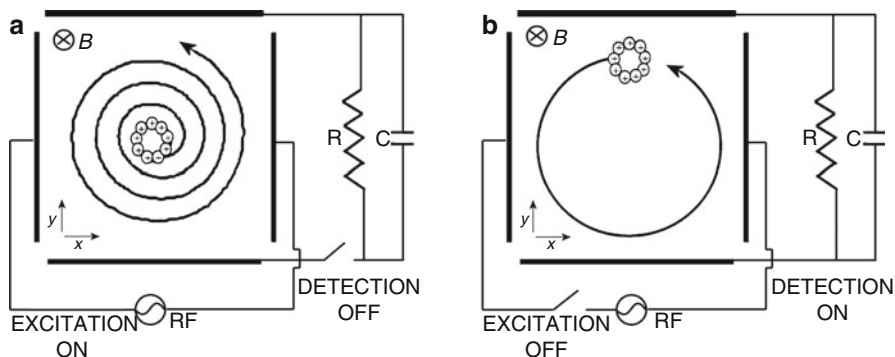


Fig. 4.64 The sequence of (a) excitation (b) and image current detection in ICR-MS. The ionic micromotion is indicated by the small circle of ions. The cell is shown along the direction of the magnetic field. (a) Illustrates the spiral trajectory of the ion cloud as induced by excitation of the ions by an RF electric field oscillating at the cyclotron resonance frequency. Note that the radius is a function of ion velocity, but the frequency f_c of circulation is not and that the radius remains constant during detection

than in case of heavier ones, i.e., the spiral is steeper, because low-mass ions need less energy than high-mass ions to accelerate to a certain velocity.

Ion kinetic energy in ICR Consider a singly charged ion of a mass of 100 u at thermal energy. Assuming a temperature of 300 K, its average velocity (Boltzmann distribution) is about 230 m s^{-1} . In a 3-T magnetic field it will circulate at $r_m \approx 0.08 \text{ mm}$. To increase the radius to 1 cm, Eq. (4.13) demands the velocity to rise by a factor of 125, i.e., to $28,750 \text{ m s}^{-1}$. Rearranging Eq. (4.3) delivers $eU = v^2 m_i/2$, and thus, we calculate a kinetic energy of about 430 eV. Definitely, the translational energy of ions in an ICR cell is high enough to effect activating collisions (Fig. 4.65 and Chap. 9) [220].

Omegatron The so-called *omegatron* was an early ICR motion-based mass spectrometer. The ions in an omegatron are generated by electron ionization of a gaseous sample inside the cell (Fig. 4.66). The electric RF field causes ions fulfilling the resonance condition, i.e., those of $f_c = f_{\text{RF}}$, to accelerate and consequently to increase the radius of their orbit. The m/z value is derived from the number of half cycles (proportional to ion kinetic energy) until the ions strike the electrometer plate at $r = r_{\text{cell}}$ [196, 197]. Thus, the omegatron essentially measures ion kinetic energy. To analyze a m/z range either the RF frequency (adaptation of f_{RF} to f_c) or the magnetic field (shifting of f_c to f_{RF}) are varied. Omegatrons were small ($r_{\text{cell}} \approx 1 \text{ cm}$) and mainly used as compact residual gas analyzers.

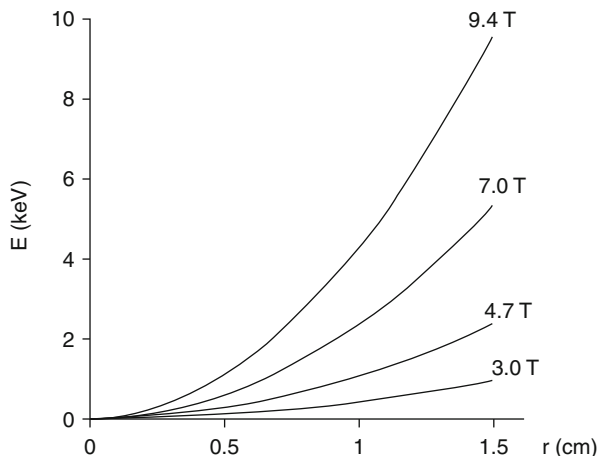


Fig. 4.65 Kinetic energy of m/z 100 ions in an ICR cell vs. orbital radius at magnetic field strengths from 3.0 to 9.4 T (Adapted from Ref. [220] with permission. © John Wiley and Sons, Inc., 1998)

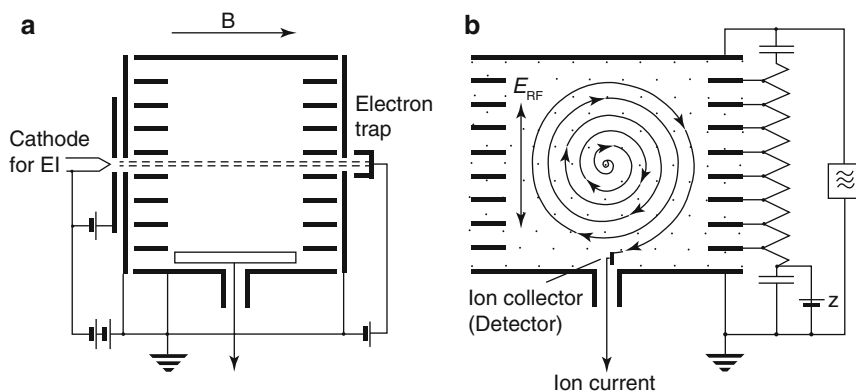


Fig. 4.66 Omegatron. (a) View parallel to B (*horizontal*) and parallel to the electron beam (*horizontal*) used to generate ions by EI inside the cell. The accelerating electric RF field acts vertical to B . (b) View on-axis to B shows the spiral motion of accelerating ions until the radius of their orbit approaches that of the cell where the ions hit an ion collector for detection (Adapted from Ref. [91] with kind permission of Curt Brunnée)

Mission half-accomplished

The disadvantages of the omegatron for use as a mass analyzer are clear: (i) mass accuracy and resolving power are limited to $1/N_c$ (N_c = number of half cycles); (ii) the electric signal for ion detection is solely due to neutralization

(continued)

of the ions, and there is no amplification as obtained with multiplier-type detectors used with all other analyzers; and (iii) the ions are removed from the cell upon detection precluding the use for MS/MS.

Moving from destructive detection by discharging the ions on the detection plates to nondestructive *image current detection* allows to switch from energy scanning to – indirect – cyclotron frequency measurement (Fig. 4.64b) [222, 223]. Image current detection relies on the fact that an ion cloud repeatedly attracts (positive ions) or repels (negative ions) the electrons of the detection electrodes upon its passage. The resulting minuscule image current can be amplified, transformed into a voltage signal and recorded as long as the ion motion exhibits sufficient coherence. In other words, a transient periodic signal is recorded in the time domain.

Observing swarms in flight

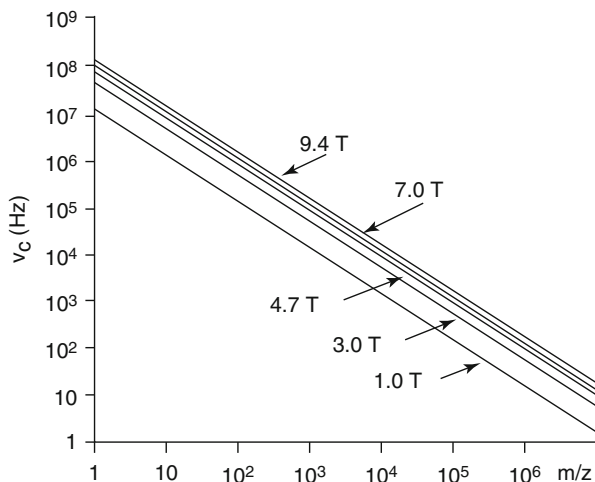
In ICR cells, the ions circulate like separate swarms of birds rather than like matter in the rings of Saturn. If ions of the same m/z non-coherently circulated at the same frequency and radius, but occupied the total orbit rather than a small sector of it, there would be no image current induced upon their passage at the detector plates, i.e., coherence of the circulating ion motion is crucial.

4.7.4 Cyclotron Frequency Bandwidth and Energy-Time Uncertainty

The *frequency bandwidth* to be covered by an ICR instrument is governed by the m/z range to be analyzed. Assuming a 9.4-T superconducting magnet, which currently represents the “upper-middle class”, we may now use Eq. (4.34) to calculate f_c for singly charged ions of m/z 50 ($m_i = 8.30 \times 10^{-26}$ kg) as $f_c = (1.66 \times 10^{-19} \text{ C} \times 9.4 \text{ T}) / (2\pi \times 8.30 \times 10^{-26} \text{ kg}) = 3.00 \text{ MHz}$. For an ion of m/z 500 (8.30×10^{-25} kg) we get a 10 times lower value, $f_c = 300 \text{ kHz}$, and for an ion of m/z 5000 (8.30×10^{-24} kg) we arrive at 30 kHz. To handle ions in the range m/z 50–5000, the ICR frequency band has to span from 30 kHz to 3.0 MHz. In other words, an ICR instrument needs to cover a frequency range from several tens of kilohertz to a few megahertz (Fig. 4.67). The tremendous bandwidth has severe implications on both the mode of operation to achieve homogeneous excitation and detection and on the electronics to deliver the required level of performance over the entire range.

Following the above calculation, it takes a frequency resolution of 3 Hz (300 kHz/100,000) to achieve a resolving power of $R = 100,000$ at m/z 500. The *energy-time uncertainty principle* states that $\Delta E \times \Delta t \approx h$. With $\Delta E = h\Delta\nu$ we

Fig. 4.67 Plot of ICR frequencies vs. m/z for different magnetic field strengths from 1.0 to 9.4 T (Reproduced from Ref. [220] with permission. © John Wiley and Sons, Inc., 1998)



derive $h\Delta\nu \times \Delta t \approx h$ or $\Delta\nu \times \Delta t \approx 1$. Accordingly, the above frequency resolution of 3 Hz in 0.3 MHz corresponds to a measurement time of 0.33 s per data point of the scan range. Operation of an ICR instrument in *continuous wave mode*, i.e., scanning in the frequency domain, is obviously unrealistic as soon as high resolving power is to be achieved. Therefore, the only practical way to acquire high-resolution ICR spectra would be to realize a broad band detection of all frequencies in parallel.

Although discouraging for ion detection, the energy-time uncertainty principle opens up new perspectives for ion excitation. According to $\Delta\nu \times \Delta t \approx 1$, a rectangular pulse of 1 ms duration covers a frequency bandwidth of 1000 Hz; a pulse of even 1 μ s should correspond to a bandwidth (frequency uncertainty) of 1 MHz, i.e., shorter pulses cover increasingly broader ranges. This has been employed in so-called *pulse excitation*.

The “bell model”

To understand pulse excitation, it is helpful to consider a mechanical comparison – a bell, for example, does not require excitation at its resonance frequency. Instead, a short strike with a hammer (pulse excitation) is fully sufficient. The bell takes up the energy with no specified frequency (all potential frequencies are contained) and automatically “finds” its own frequency plus its overtones to resonate and, thus, to sound.

According to the above considerations, the resolving power R that can theoretically be achieved depends on the smallest $\Delta\nu$ that can be resolved, and thus, increases the longer Δt used for acquiring the transient, t_{acq} . Further, it depends

on m/z of the ion and the magnetic field B . A simple numerical-value equation may be used to calculate the theoretical maximum R [220, 224]:

$$R = \frac{v}{\Delta v} = \frac{m}{\Delta m} = 1.274 \times 10^7 \frac{zB t_{\text{acq}}}{m} \quad (4.35)$$

For example, for an ion of m/z 400, $B = 7$ T, and $t_{\text{acq}} = 1$ s, we obtain $R = 222,950 \approx 230,000$. A transient of 0.2 s would therefore reduce it to one fifth, $R = 46,000$, while recording the transient for 10 s could deliver $R = 2,300,000$.

Resolving power's interdependence

Obviously, the resolving power of any FT-ICR instrument can only be stated along with m/z of the ion of interest, the magnetic field, and the acquisition interval of the transient. A high rate of spectral acquisition sacrifices resolving power, while a long transient can yield ultrahigh resolving power at the expense of speed and duty cycle.

4.7.5 Fourier Transform – Basic Properties

Some knowledge of the basic properties of the *Fourier transform* (FT) will be helpful prior to discussing FT-ICR instrumentation [225]. The Fourier transform is a mathematical operation that transforms one complex-valued function of a real variable into another. The domain of the original function is typically time (as is here) and accordingly is termed the *time domain*. The domain of the function generated upon FT is frequency. The product of FT then is the *frequency domain* representation of the original function. The frequency domain function describes which frequencies are contained in the original function. For example, FT applied to a chord of music comprising several fundamental frequencies (and overtones) as represented by the notes would deliver all contributing frequencies and their amplitudes. The Fourier transform makes the move from a wave and its amplitude to its frequency and its amplitude (Fig. 4.68a, b).

FT of a transient signal, i.e., a signal vanishing to zero amplitude at the end of the observation time span, delivers a Lorentzian curve in the frequency domain (Fig. 4.68c, d). In accordance with the energy-time uncertainty principle, the frequency domain output becomes increasingly sharper the longer the observation time span, because the frequency is more accurately determined the more cycles are recorded in the transient.

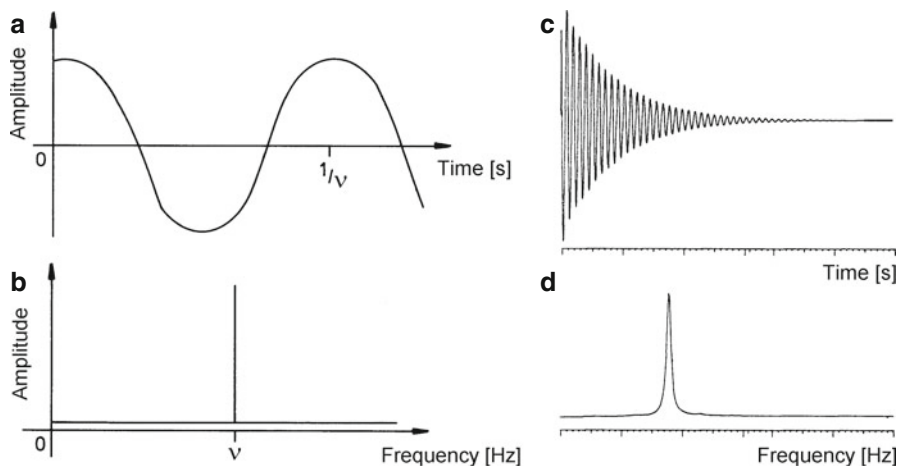


Fig. 4.68 Illustration of the principle of FT. (a) A time domain wave, infinite in time, is transformed by FT to (b) reveal its frequency. The amplitude is conserved. (c) FT of a transient time domain signal into (d) a frequency domain signal of Lorentzian shape. FT works equally well if an extremely large number of frequencies and amplitudes is contained in the time domain signal

Jean-Baptiste Joseph Fourier

Fourier was a French mathematician (1768–1830). Besides Fourier transformation, his influential work concerns the mathematical description of the conduction of heat in solids and the development of infinite series (Fourier series). He witnessed the French revolution and accompanied Napoleon on his expedition to Egypt.

In FT-ICR experiments, the observation time span is normally shorter than the time required to damp down the transient to zero. Instead, the detection is abruptly ended when the preset transient length is reached. The duration of the transient is generally determined by the product of the number of data points that is to be recorded and the rate at which those data points are being sampled. The minimum *sampling rate* is in turn determined by the highest cyclotron frequency to be observed. Typical values in FT-ICR-MS are 0.5–2 s transients of 512 k to 2 M (2×10^6) data points at 250 kHz to 1 MHz sampling frequency. Thus, the arbitrary truncation of the transient causes the transient to represent a combination of a step function and a perfectly dampened signal (Fig. 4.69). As FT yields $\text{sinc}(x)$ from a step function, the FT output from a truncated signal is a Lorentzian main peak accompanied by side bands, so-called *wiggles*.

To reduce the side band-creating effect of truncation, the transient is normally subjected to *apodization* prior to FT. Apodization means the multiplication of the signal by a mathematical function that causes the values to smooth out to zero.

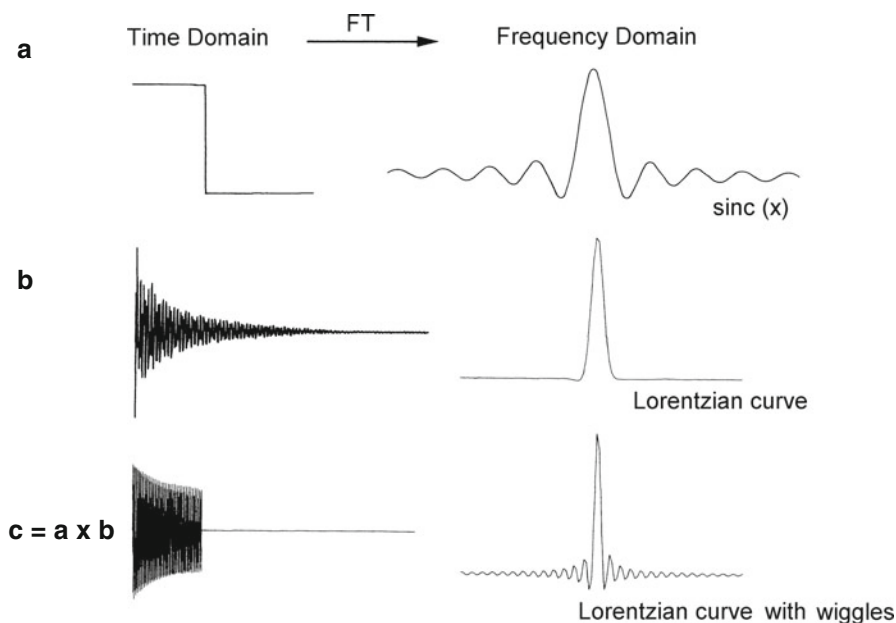


Fig. 4.69 The effects of Fourier transforms on different input signals. (a) A step function is converted to $\text{sinc}(x)$, (b) a fully damped transient signal containing only one frequency yields a single Lorentzian curve, and (c) the truncated transient can be regarded as a combination of (a) and (b) and yields a Lorentzian curve accompanied by “wiggles”

Some sophisticated apodization methods are in use to deliver the ultimate resolution, nonetheless, simple $\sin(x)$ or $\sin^2(x)$ functions work well.

Another feature of FT is to yield better resolved frequency spectra from larger data sets, which not necessarily need to contain real data. Simply adding a row of zeros to the end of the experimental transient is beneficial in that it smooths the peak shape by increasing the number of data points per m/z interval. This “trick” is known as *zero-filling*. The number of attached zeros normally equals the number of data points, sometimes even twice as many are filled in (*double zero-filling*).

4.7.6 Nyquist Criterion

The actual shape of a peak not only depends on the capabilities of the mass analyzer in use but is also determined by the sampling rate applied to collect the signal (Sects. 4.12 and 11.5). The sampling rate is even more relevant for periodic signals such as from the cyclotron motion in FT-ICR. The minimum sampling rate needed to correctly detect any periodic signal is governed by the *Nyquist criterion*, according to which the sampling rate, ν_{samp} , must have at least twice the frequency of the process, ν_{proc} , that is to be recorded

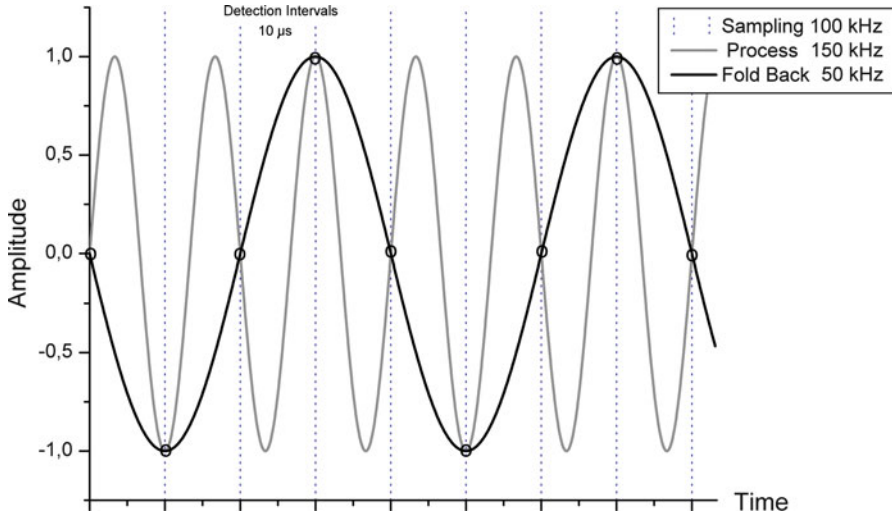


Fig. 4.70 The aliasing phenomenon. Detection points are where the *dotted* verticals cross the *light gray* signal curve (○). The process (150 kHz) occurs at $v_{\text{proc}} = 1.5 \times v_{\text{samp}}$ (100 kHz or 10 μs per point) instead of $\leq 0.5 v_{\text{samp}}$. This causes the output of an aliased signal at $v_{\text{fold}} = 50$ kHz as determined by Eq. (4.37) (*dark curve*). In this special case setting $n = 1$ just delivers $v_{\text{fold}} = v_{\text{nyq}}$

$$v_{\text{samp}} \geq 2 \times v_{\text{proc}} \quad (4.36)$$

Vice versa, the Nyquist limit frequency, v_{nyq} , up to which a process can just be correctly detected is given as

$$v_{\text{nyq}} = v_{\text{samp}}/2 \quad (4.37)$$

aliasing (or *folding back*) occurs beyond the Nyquist limit. Then, the detected signal pretends the process to proceed at a foldback frequency, v_{fold} , described by

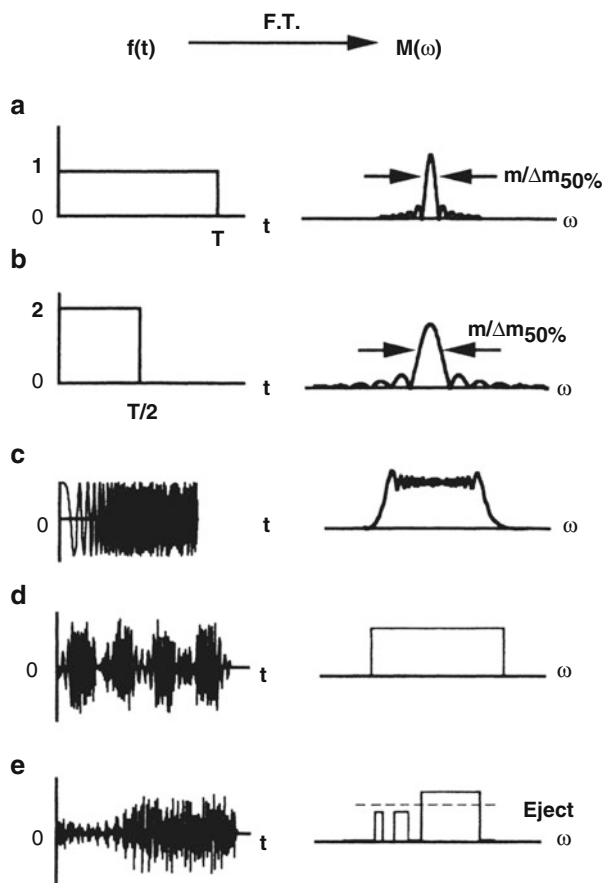
$$v_{\text{fold}} = |n \times v_{\text{samp}} - v_{\text{proc}}| \quad (4.38)$$

where the factor n is an integer selected as to fulfill the condition $0 < v_{\text{fold}} \leq v_{\text{nyq}}$. An illustration of the folding back phenomenon is given in Fig. 4.70.

4.7.7 Excitation Modes in FT-ICR-MS

In the ICR cell, there is a stringent correlation of cyclotron frequency f_c and m/z value. For simplicity, the very first FT-ICR experiment was therefore performed with an excitation pulse of a fixed f_c tailored to fit the model analyte, methane molecular ion [200]. However, useful measurements require the simultaneous excitation of all ions in the cell, and this in turn demands for a large RF bandwidth.

Fig. 4.71 Time-domain (*left*) and frequency-domain (*right*) excitation waveforms: (a, b) rectangular pulses yield inhomogeneous and rather narrow excitation windows; (c) “chirp” excitation; (d, e) SWIFT excitations, with (e) designed to eject a certain mass range from the cell (Reproduced from Ref. [220] by permission. © John Wiley & Sons, 1998)



Several excitation methods have been developed to cope with this technically nontrivial task. The differences between these methods can easily be judged from the shape of the frequency-domain excitation waveforms (Fig. 4.71) [203, 220]. The simplest approach is to irradiate a single frequency (resonant excitation) for some time, i.e., as a *rectangular pulse*, but this selectively excites ions of a single mass [200]. Applying such a narrow band excitation as a short pulse yields some expansion of the range. The effect of a *frequency sweep* or “*chirp*” excitation is much better [201]. Chirp excitation sequentially affects ions across the m/z range although it never delivers a defined frequency. Instead, the chirp exploits the wide band character of rushing across the frequencies. Chirp excitation is not perfectly homogeneous as it gives some distortions close to the borders of the range, nonetheless is it successfully employed in commercial FT-ICR instruments.

The best results are to be expected from *stored waveform inverse Fourier transform* (SWIFT) excitation [226]. First, the ideal excitation waveform is tailored to the needs of the intended experiment and then produced by an RF generator. SWIFT excitation also allows to remove ions of predefined m/z ranges from the ICR

cell. This results in storage of a small m/z range, or after repeated SWIFT pulsing of a single nominal mass out of a broad band spectrum. Those ions are then accessible for ultrahigh resolution measurements or as precursors for tandem MS.

4.7.8 Axial Trapping

Our basic considerations of ICR (Sect. 4.7.3 and Fig. 4.64) were so far restricted to the xy -plane of a cell. Two of the four side walls (x -axis) of the ICR cell are connected to the RF power supply during the period of excitation. Then, the image current induced in the detector plates (y -axis) is recorded as transient signal for some period of time (0.5–30 s). The excitation of the ions within the ICR cell has to stop at a level low enough to avoid wall collisions of the lightest ions to be measured [206, 219, 220].

At a first glance, the z -dimension of the cell seems to be of no importance for the function of an FT-ICR mass spectrometer. However, the z -component of thermal energy and the kinetic energy of ion injection into the ICR cell in case of an external ion source both would lead to rapid loss of the xy -trapped ions along that axis, because they would pass through the cell along the z -axis on a helical trajectory. It is therefore important to establish a trapping potential in z -direction. The simplest way is to place DC trapping electrodes at the open ends [197]. Furthermore, our initial treatment of the ICR cell was also done with the implicit understanding that this would be a cubic cell.

4.7.9 Magnetron Motion and Reduced Cyclotron Frequency

Trapping of ions in a potential well implies reflection of ions between the trapping plates that induces an oscillatory motion along the z -axis the frequency ω_z of which is given by

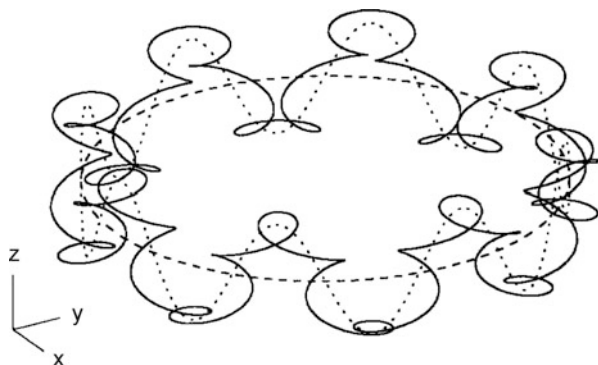
$$\omega_z = \sqrt{\frac{2qV_{\text{trap}}\alpha}{ma^2}} \quad (4.39)$$

where a is the physical z -dimension of the trap and α represents a shape parameter that depends on the trap design [220]. The curved electric field close to the borders also produces an outward-bound radial force $F_r = qE_{(r)}$ opposed to the action of the Lorentz force F_L that is given by

$$F_r = qE_{(r)} = \frac{qV_{\text{trap}}\alpha}{a^2}r \quad (4.40)$$

The magnetic field now acts by transforming the radial force component into another circular motion of the trapped ions. The total force on an ion then is

Fig. 4.72 Ion motion for $\omega_+ = 4\omega_z$ and $\omega_z = 8\omega_-$ in an ICR cell. Pure magnetron motion (*dashed*), magnetron plus trapping motion (*dotted*), and the resulting overall motion (*solid*) (Reproduced from Ref. [227] by permission. © Elsevier Science Publishers, 1995)



$$F_{\text{tot}} = F_L - F_r = m_i \omega^2 r = qB\omega r - \frac{qV_{\text{trap}}\alpha}{a^2} r \quad (4.41)$$

which can be rewritten to reveal its character of a quadratic equation in ω

$$\omega^2 - \frac{qB\omega}{m_i} + \frac{qV_{\text{trap}}\alpha}{a^2} = 0 \quad (4.42)$$

This quadratic equation has two solutions, the first of them representing the *reduced cyclotron frequency* ω_+

$$\omega_+ = \frac{\omega_c}{2} + \sqrt{\left(\frac{\omega_c}{2}\right)^2 - \frac{\omega_z^2}{2}} \quad (4.43)$$

and the second the *magnetron frequency* ω_-

$$\omega_- = \frac{\omega_c}{2} - \sqrt{\left(\frac{\omega_c}{2}\right)^2 - \frac{\omega_z^2}{2}} \quad (4.44)$$

where ω_z is obtained from Eq. (4.39) and ω_c from Eq. (4.33). The obvious consequence for the ionic motion in an ICR cell is that the simple description of ω_c by Eq. (4.33) only yields the so-called *unperturbed cyclotron frequency*, whereas the real motion is by far more complex. Figure 4.72 shows the overall motion of ions in an ICR cell taking ω_z , ω_+ and ω_- into account [227]. It should be noted that the radius of the magnetron motion is generally larger than that of the cyclotron motion. In many cases the magnetron motion also causes a small side peak in the vicinity of the main peak.

4.7.10 Detection and Accuracy in FT-ICR-MS

An FT-ICR experiment requires full temporal separation of excitation and subsequent detection of the trapped ions. Detection is based on the measurement

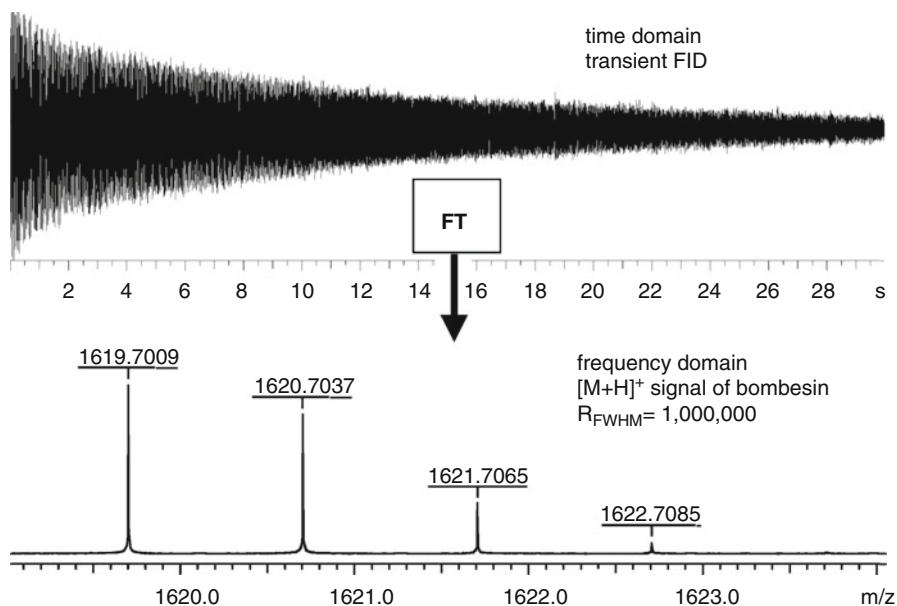


Fig. 4.73 The principle of FT-ICR-MS. In detail, the procedure includes recording the transient, apodization of the transient, zero-filling, FT, and finally the calculation of m/z values from the cyclotron frequencies. The longer the detection interval the higher the attainable resolving power. This example shows the $[M + H]^+$ ion of the peptide bombesin, m/z 1619.7009, where a 30 s transient resulted in a spectrum at $R = 10^6$ (By courtesy of Bruker Daltonik, Bremen)

of image currents in the detector plates. An image current is induced by each ion package when repeatedly passing the detector plates at its individual cyclotron frequency, i.e., detection in FT-ICR means “listening to the circulating ions”. The transient signal or *free induction decay* (FID) is recorded, and afterwards, the FID is converted from the *time domain* to the *frequency domain* by means of Fourier transformation. This means that the complex FID caused by superimposition of many single frequencies is deconvoluted to reveal the single contributing frequencies and their respective amplitudes. Using Eq. (4.34), the frequencies are converted to m/z values; their amplitudes now representing the abundances of the corresponding ions (Fig. 4.73) [195, 200, 203, 228, 229].

There is a correlation between the transient signal and the pressure in the ICR cell [220, 228]. In perfect vacuum, the orbiting motion would solely be damped by induction, whereas in the presence of residual gas collisions will finally slow down the ions to thermal energy. As the resolving power in FT-ICR-MS is also proportional to the acquisition time of the transient signal, ultrahigh vacuum in the range of $\approx 10^{-10}$ mbar is a prerequisite in the ICR cell. Based on a 7-T magnet and Eq. (4.35), the theoretical resolution for the example in Fig. 4.73 is $R \approx 1.6 \times 10^6$, which shows the influence of residual gas and other factors causing loss of coherence on actual resolving power.

Ultrahigh vacuum required

The need for extremely long mean free paths in FT-ICR mass spectrometers arises from the combination of high ion velocities of several 10^3 m s^{-1} and observation intervals in the order of seconds. Coherent swarms of ions thus need to travel hundreds of meters during the detection interval. Collisions would be detrimental for peak shape. The typical ICR cell pressure therefore is 10^{-10} to 10^{-9} mbar.

The detection efficiency is greatly improved for cylindrical cells as compared to cubic cells, because the ions pass the detection electrodes at almost constant distance to their surface. This results in stronger image currents due to on the average closer passages and sharper detection wave forms as their entering and exiting from the detection zone causes more sudden changes.

The ICR voltage signal strength at the detector plates is inversely proportional to ion mass if the monitoring circuit is predominantly resistive, and is independent of ion mass if the circuit is predominantly capacitive [229]. Image current detection at room temperature is typically less sensitive than ion counting techniques in beam instruments. Nonetheless, for modern FT-ICR instruments the detection limit to yield a signal-to-noise ratio of 3:1 corresponds to roughly 200 ions, provided these are excited to travel at half of the maximum cyclotron radius [211, 219].

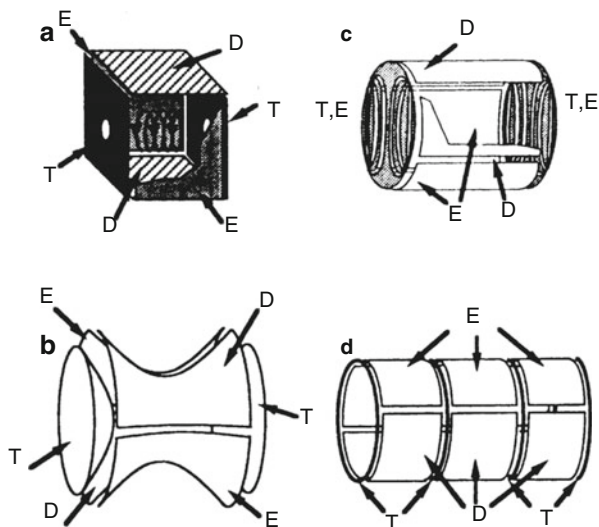
The advantages of FT-ICR detection over ICR are obvious:

- The $1/N_c$ limit vanishes because every ion undergoes some 10^4 – 10^8 cycles during the detection interval.
- Sensitivity improves because the ions give rise to a detectable image charge during each passage of a detector plate.
- Ion detection is nondestructive, i.e., ions are not lost upon detection (this enabling MS/MS experiments).
- Elongated recording of the FID provides for extremely precise determination of all cyclotron frequencies, thereby yielding the highest values of resolution and mass accuracy available [214, 215, 230].

External calibration is most effective when the level of excitation and the number of trapped ions of calibrant ions closely approaches that of the analyte ions [219]. The latest FT-ICR instruments can routinely attain mass accuracies of better than 1 ppm. Internal calibration can yield further improvement.

Although resolution and mass accuracy are already high in broadband spectra ($R = 3 \times 10^4$ – 10^5 , $\Delta m < 10^{-3}$ u), the performance of FT-ICR instruments further improves by storing only narrow m/z ranges, because fewer ions in the cell mean less distortion by coulombic interactions.

Fig. 4.74 Important ICR cell types; electrodes are labeled with *E* excitation, *D* detection, *T* trapping; (a) classic cubic cell, (b) Penning cell with hyperbolic electrodes, (c) infinity Cell™ with segmented trapping plates, and (d) triple cell. The latter two aim at virtually expanding the potentials in the trapping zone along the *z*-axis (Adapted from Ref. [232] with permission. © Elsevier Science Publishers, 1995)



4.7.11 Design of ICR Cells

We have seen that ion motion and detection in FT-ICR are affected by various parameters. Axial trapping oscillation, resulting magnetron motion, and disturbances leading to loss of coherence – or dephasing – strongly depend on the geometry of the ICR cell and on the homogeneity of the magnetic field. The simple cubic cell (the ICR cell of the pioneers) severely suffers from field imperfections. Therefore, numerous other designs have been developed offering remarkable improvements over the cubic cell (Fig. 4.74) [219, 220].

A nearly ideal hyperbolic field is created inside a hyperbolic trap, also known as *Penning trap* or *Penning cell* (Fig. 4.74b). However, this shape requires a small inner volume for the ions to circulate and the performance soon suffers from space charge effects as the number of ions increases. While capable of extremely high performance with 10–1000 ions, Penning cells are not suited for analytical work where a cell has to accommodate large ion populations to offer a high dynamic range and to deal with complex mixtures.

As in the case of segmented LITs with radial ejection (Sect. 4.5.3 and Figs. 4.48 and 4.49), the distortion of the electric field can be avoided when the trapping sections are properly designed and operated; then the ICR cell displays itself to the ions as being of virtually infinite length. Thus, triple-segmented cylindrical cells [231] and many others have been developed [232]. Another approach, the *infinity cell* makes use of segmented end caps on a cylindrical cell (Fig. 4.74c) [233].

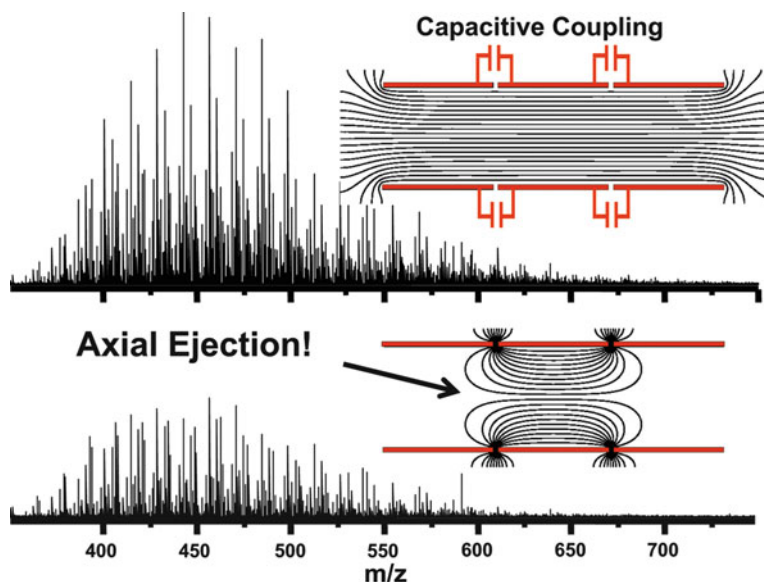
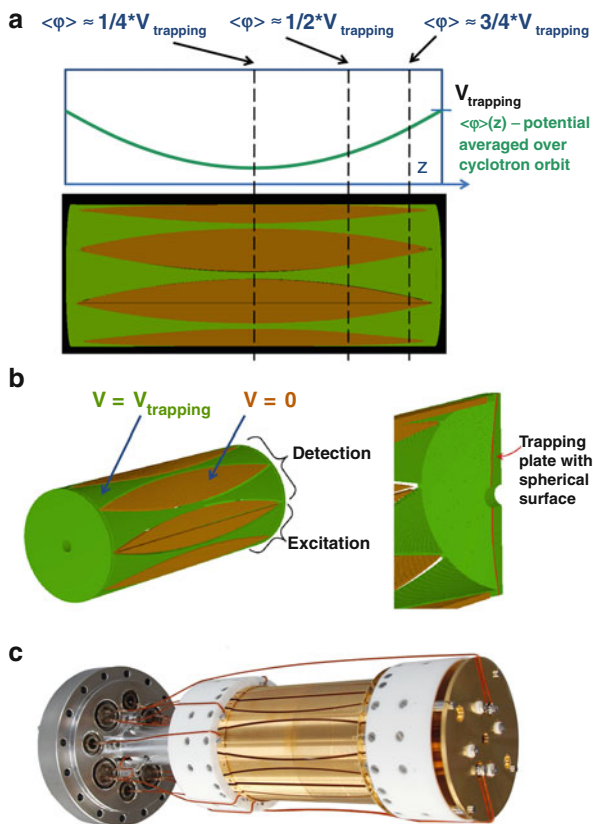


Fig. 4.75 Comparison of a cylindrical cell having both capacitively-coupled (*top*) and noncoupled trapping electrodes (*bottom*) to the resulting spectra of a complex sample. The curvature of the RF excitation isopotentials for the single electrode pair (*bottom*) produces axial RF excitation leading to m/z -dependent axial ejection. Capacitive coupling of the RF excitation to the end cap electrodes effectively eliminates axial ejection and yields an improved spectrum. (Reproduced with permission from Ref. [212]. © Elsevier Science Publishers, 2015)

The advantageous effect of capacitive coupling of trapping segments in a triple-segmented cylindrical cell are shown in Fig. 4.75. The figure not only depicts the field flattening effect of the capacitive coupling but also shows its correlation to the enhancement of FT-ICR spectra due to this design [212]. ICR cells of this type are used in the Thermo Scientific LTQ-FT Ultra series.

A recently designed cell by E. Nikoleav extends the region of harmonic potential to almost its full volume. This is achieved by subdivision of the walls of a long cylindrical cell (150×56 mm) into alternating convexly and concavely shaped segments [210, 224, 234]. The convex segments stay grounded while the trapping potential is applied to the concave parts. The trapping plates are slightly spherical in shape. Overall, this causes ions to experience an on-average harmonic potential per full cycle of cyclotron motion (Fig. 4.76). This fact gives rise to its description as a *dynamically harmonized ICR cell*. For excitation and detection the cylinder is classically divided into four sections of 90° with the dividing cuts slicing every second convex electrode into halves. This design provides a major boost in

Fig. 4.76 Dynamically harmonized ICR cell. (a) Axial cross section showing the segmented cell walls and the hyperbolic trapping potential experienced by ions on average per full cycle. (b) Division into four 90° sections to accomplish excitation and detection plus detail of a trapping plate. (c) Photograph of the Paracell; gold plating is used to minimize electrode oxidation. (Figure compiled from material by courtesy of Bruker Daltonik, Bremen)



resolving power whilst maintaining high ion capacity and dynamic range [216, 217, 235]. It is commercialized as Paracell by Bruker Daltonik.

4.7.12 FT-ICR Instruments

Ion traps, ICR cells as well as QITs, are best operated with the number of trapped ions close to their respective optimum, because otherwise ion trajectories are distorted by coulombic repulsion. Hence, external ion sources in combination with ion transfer optics capable of controlling the number of injected ions are ideally attached to ion traps. Currently, MALDI [236] and even more so ESI [207, 214, 215, 230, 237] and other atmospheric pressure ionization sources predominate in FT-ICR.

The ion current is not solely regulated by the source but by some device to collect and store the desired amount of ions until the package is ready for injection

into the ICR cell. Linear RF-multipole ion traps are normally employed for that purpose (Sect. 4.5.1) [119, 238, 239], but other systems are also in use [218]. RF-only multipoles are commonly used to transfer the ions through the boundaries of the magnetic field into the ICR cell (Sect. 4.4.4) [238]. For their injection, it is important to adjust the conditions so that the ions have low kinetic energy in z -direction in order not to overcome the shallow trapping potential. While some buffer gas is beneficial in case of LITs and QITs, ICR cells are operated at the lowest achievable pressure. The typical path from an external ion source into the ICR cell is therefore characterized by multistep differential pumping to achieve some 10^{-8} – 10^{-7} Pa inside the ICR cell.

FT-ICR instruments are always equipped with superconducting magnets usually having 7 T and 9.4 T field strength; while 12 T and 15 T is also occasionally available. The advantages of increased field strengths are numerous: resolving power and scan speed, for example, increase linearly with B . Moreover, upper mass limit, ion trapping time, ion energy, and number of trapped ions even increase with B^2 .

At the time of writing, FT-ICR instruments as considered here are provided by just two manufacturers: (i) the Qh-FT-ICR type as by the Bruker Solarix series (Fig. 4.77) and LIT-FT-ICR hybrid instruments as by the Thermo Scientific LTQ FT Ultra series (Sect. 4.8 and Fig. 4.86).

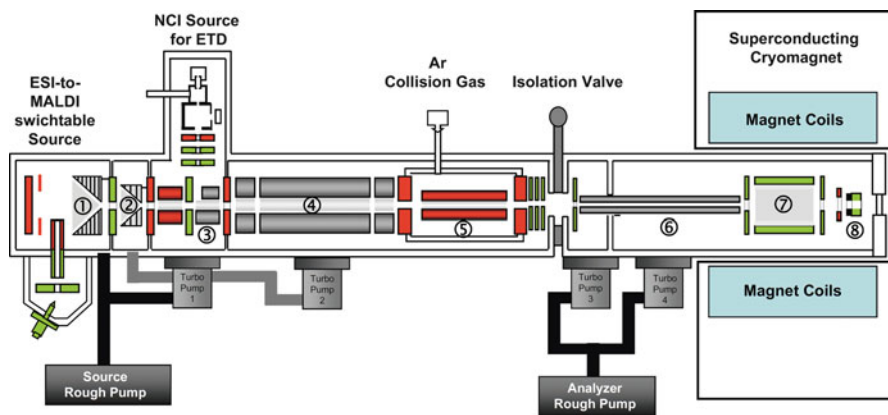


Fig. 4.77 A hQh-ICR hybrid instrument. This instrument is equipped with an ESI-to-MALDI switchable ion source that makes use of a two-stage ion funnel (①, ②) to focus ions into a RF hexapole ion guide (h, ③). The ions then pass a quadrupole (④) that may either be run as band pass (q) or as mass-selective device (Q) and then reach a multifunctional RF hexapole ion trap (h, ⑤) where they can be (i) accumulated, (ii) collisionally activated, or (iii) reacted with radical anions from the NCI source to effect ETD as required. For mass analysis the ions are then guided via an RF-only hexapole (⑥) into the ICR cell (⑦) where a hollow cathode (⑧) is attached for ECD. RF-only hexapole (⑥) and magnet are not to scale but shown relatively much smaller (Schematic of Bruker Solarix instrument series by courtesy of Bruker Daltonik, Bremen)

4.7.13 Summary of FT-ICR Instrumentation

Principle of Operation

Ions moving on a plane orthogonal to the direction of a magnetic field are forced on circular orbits by action of the Lorentz force. The radius of their orbit depends on ion kinetic energy, while the frequency of oscillation – the so-called cyclotron frequency – depends on the mass of the ions. To induce this mass-dependent ion motion, ions that are transferred into a magnetic field need to be excited by an RF electric field of a frequency equaling that of their cyclotron frequency. Once excited, ions of equal m/z coherently circulate inside the ICR cell. Upon their passage, the ion swarms induce image currents in the detection plates making up about half of the inner wall surface of the ICR cell. The image currents are recorded in the time domain (for 0.2–20 s), transformed into frequency domain by means of Fourier transformation (FT), and finally used to calculate the corresponding m/z values.

Performance Characteristics

FT-ICR instruments are the best-performing mass spectrometers in terms of resolving power (10^5 to $>10^6$) and mass accuracy (typically 0.1–2 ppm). The level that is achieved depends on the actual instrument, the duration of the transient, and numerous other parameters. Due to the long detection interval and the use of image current detection, FT-ICR-MS offers comparatively low sensitivity. This is counterbalanced by the fact that modern instruments can accommodate different ionization techniques, offer a variety of tandem-MS capabilities, and may even serve for sophisticated experiments in gas-phase ion chemistry. The extraordinary resolving power and mass accuracy enable the analysis of complex mixtures like crude oil or dissolved organic matter. Tandem-MS may serve to solve complex problems in protein analysis.

General Considerations

Mostly due to the prerequisite of using high-field superconducting magnets and the need for ultrahigh vacuum, FT-ICR instruments are large, heavy, and expensive in terms of both investment and cost of operation. While it may be challenging to exploit an instrument's full potential, modern FT-ICR instruments are nonetheless suitable for routine use. In fact, there are problems that can only be solved by FT-ICR-MS.

FT-MS

Occasionally, FT-ICR-MS is referred to as FT-MS or even FTMS. Apparently, FT-MS is most frequently used by mass spectrometrists who have dealt with FT-ICR-MS since the early days of the technique. Of course, ICR-MS without Fourier transformation would never have become as successful, but Fourier transformation alone cannot separate ions according to m/z . With the advent of the Orbitrap analyzer (Sect. 4.8), there is a second system making use of Fourier transformation of a time domain signal, although the prefix FT finds no mention in that name.

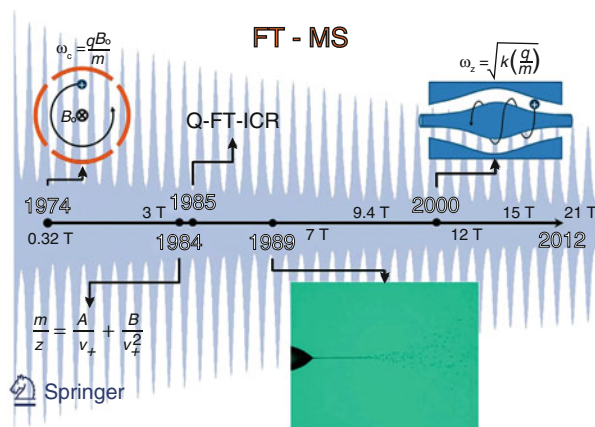


Fig. 4.78 FT-MS timeline as displayed on the journal cover of an issue dedicated to HR-MS. The journey starts with the introduction of FT-ICR and proceeds via m/z calibration, introduction of RF quadrupole transfer optics, external ESI source, and the first papers dealing with Orbitrap development. The magnetic fields available for FT-ICR-MS are also included (Adapted from *Analytical and Bioanalytical Chemistry* **403**(5) 2012 with permission. © Springer-Verlag, Heidelberg, 2012)

The acronym FT-MS is hence proposed as a collective term summarizing all FT-based MS techniques, i.e., FT-ICR-MS and Orbitrap-MS. Figure 4.78 taken from a journal cover of a special issue dedicated to HR-MS presents a welcome transition from FT-ICR to Orbitraps and also presents a compact timeline of developments.

4.8 Orbitrap Analyzer

The Orbitrap analyzer incorporates a concept of m/z analysis of its own [20, 240]. Commercialized by Thermo Fisher Scientific in 2005, the Orbitrap™ delivers high resolving power and accurate mass measurement at a level rivaling FT-ICR to a certain extent [20, 241–245]. It is the special charm of the Orbitrap to operate without a magnetic field, and therefore, to be available at a lower price and having fewer installation room requirements than FT-ICR instruments. Nonetheless, it has one important feature in common with FT-ICR: the Orbitrap also employs image current detection of ion oscillations and Fourier transformation for the conversion of the transient into the frequency domain. As we already have dealt with the very basics of FT in the context of FT-ICR-MS we may now concentrate on design and operation of the Orbitrap analyzer itself.

Orbiting in an electrostatic field

The Orbitrap is also an ion trap, but there is neither a magnet to hold ions inside nor is there any sort of RF excitation to initiate their motion. Instead, moving ions are trapped in a constant radial electrostatic field. The electrostatic attraction towards the central electrode is compensated by a centrifugal force that arises from the initial tangential velocity of ions: very much like a satellite in orbit [241].

4.8.1 Orbitrap – Principle of Operation

In 1923, Kingdon constructed an ion trapping device based on a straight wire along the axis of a surrounding cylindrical electrode having flanges that enclosed the trapping volume. Ions tangentially approaching the wire that is set to attractive electric potential would not hit the wire but become captured in a rotational motion around it. Their trajectory is then defined by an equilibrium of the centrifugal force and the electrostatic force generated by applying a voltage between wire and enclosing cylinder. Axial motion along the wire is confined by the field curvature introduced by the flanges of the cylinder. This became known as the *Kingdon trap* [246]. Later, Knight refined the outer electrode shapes to a design with large radius in the center that continuously decreased toward both ends. The outer electrode was symmetrically split into halves in a fashion similar to the end caps of the QIT. This trap design is often called *ideal Kingdon trap* [247]. Knight's trap could store ions and eject them onto a detector, but did not perform any m/z analysis [245]. The first proposal to build a Kingdon trap-based mass analyzer with image current detection addressed the ion rotational frequencies, but it suffered from the poor definition of those frequencies due to the influence of initial ion velocity upon entering the trap [248]. Finally, the concept of Makarov exploited the periodic back and forth motion of ions along the central electrode [240]. This setup requires a precisely defined field composed of a quadrupole field of the ion trap and the logarithmic field of a cylindrical capacitor that is split into two halves. This mass analyzer was termed *Orbitrap* [240] and can be considered as a refined Knight-style Kingdon trap. It has a spindle-like central electrode and a barrel-like outer electrode (Fig. 4.79) [245].

The electric field resulting from the complex shape of the Orbitrap electrodes may be termed quadrologarithmic field and has the potential distribution $U(r, z)$

$$U(r, z) = \frac{k}{2} \left(z^2 - \frac{r^2}{2} \right) + \frac{k}{2} (R_m)^2 \ln \left[\frac{r}{R_m} \right] + C \quad (4.45)$$

where r and z are cylindrical coordinates ($z = 0$ being the plane of symmetry of the field), k is the field curvature, R_m the characteristic radius, and C is a constant [240, 249]. Equation (4.44) determines the electrostatic field experienced by ions inside the Orbitrap that forces them to move in complex spiral patterns. Stable ion trajectories combine rotation around the central axis with axial oscillations, the

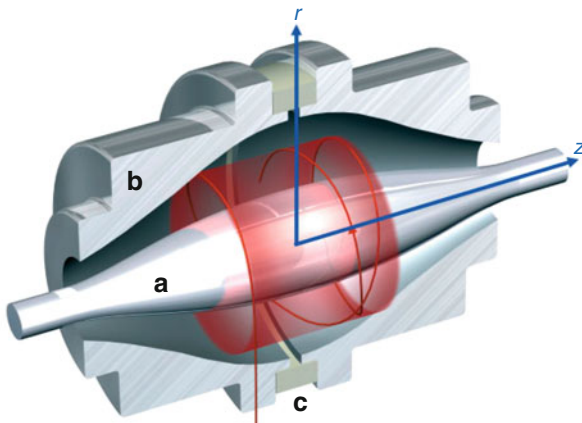


Fig. 4.79 A cut-away view of the Thermo Fisher Orbitrap™ mass analyzer. Ions are moving in spirals around a spindle-like-shaped central electrode (a) that creates an axial field gradient. An outer electrode (b) is split in half by an insulating ceramic ring (c). An image current induced by moving ions is detected via a differential amplifier between the two halves of the outer Orbitrap electrode. The m/z of different ions in the Orbitrap can be determined from respective frequencies of oscillation after a Fourier transform (Reproduced from Ref. [241] with permission. © Wiley-VCH, Weinheim, 2006)

frequency ω_z of which solely depends on the ratio of ionic charge q to ionic mass m_i and the field curvature, but is independent of the tangential velocity and spatial spread of the ions [241].

A detailed mathematical treatment of the Orbitrap can be found in Refs. [20, 240]. It delivers this important frequency of axial oscillations ω_z (in rad s^{-1}) as given by

$$\omega_z = \sqrt{k \left(\frac{q}{m_i} \right)} \quad (4.46)$$

The frequency of the harmonic axial oscillation ω_z is inversely proportional to the square root of the mass-to-charge ratio of the ions.

Another two characteristic frequencies can be derived for ions inside the Orbitrap. First the frequency of rotation ω_ϕ around the central electrode

$$\omega_\phi = \frac{\omega_z}{\sqrt{2}} \sqrt{\left(\frac{R_m}{R} \right)^2 - 1} \quad (4.47)$$

and second, the frequency of radial oscillation ω_r , i.e., the “pumping motion” of the orbit as the ions move along the variable radius of the central electrode:

$$\omega_r = \omega_z \sqrt{\left(\frac{R_m}{R}\right)^2 - 2} \quad (4.48)$$

4.8.2 Ion Detection and Resolving Power of the Orbitrap

The frequency of the harmonic axial oscillation ω_z can be determined by image current detection from a differential amplifier connected to the halves of the outer electrode; for each m/z value a sine wave is produced. Analogous to FT-ICR, the image current signal is monitored, stored, and translated into a frequency domain signal by fast Fourier transform resulting in an accurate reading of their m/z (Fig. 4.80) [241, 250]. Different from FT-ICR, there is no excitation prior to the detection period. Instead, the electric field gradient induces the axial oscillation when ions are injected tangentially but off-center with respect to plane of symmetry. All ions have exactly the same amplitude whereas the frequency of axial motion is dictated by their m/z value. Again, there is an analogy to FT-ICR in that packets of ions of common m/z exhibit discrete motions with some interference by interpenetration of ion clouds of different m/z that are simultaneously occupying the trapping volume [20].

In an Orbitrap, the mass resolving power R is half the frequency resolving power due to the square root in Eq. (4.46) [245, 249]. It can be calculated as

$$R = \frac{m}{\Delta m} = \frac{1}{2\Delta\omega_z} \sqrt{\frac{kq}{m}} \quad (4.49)$$

Orbitrap versus FT-ICR While the frequency of the axial oscillation ω_z in an Orbitrap is proportional to $(q/m)^{1/2}$, the cyclotron frequency ω_c in FT-ICR is proportional to q/m . Accordingly, FT-ICR offers higher resolving power for lower m/z ions whereas the Orbitrap may outperform it at high m/z values. For example, in case of an FT-ICR instrument with a 7-T magnet, the Orbitrap has an edge over FT-ICR above m/z 800 (Fig. 4.81) [241, 245].

4.8.3 Ion Injection into the Orbitrap

The Orbitrap alone does not present a very practical instrument. While it serves as a high performance m/z analyzer, its operation demands for proper ion injection and it requires ultra-high vacuum in order to realize sufficiently long transients. Ion injection has to comply with several conditions and restrictions:

- Geometric prerequisites have to be met, such as injection angle, angular spread, and position with respect to the electrodes.

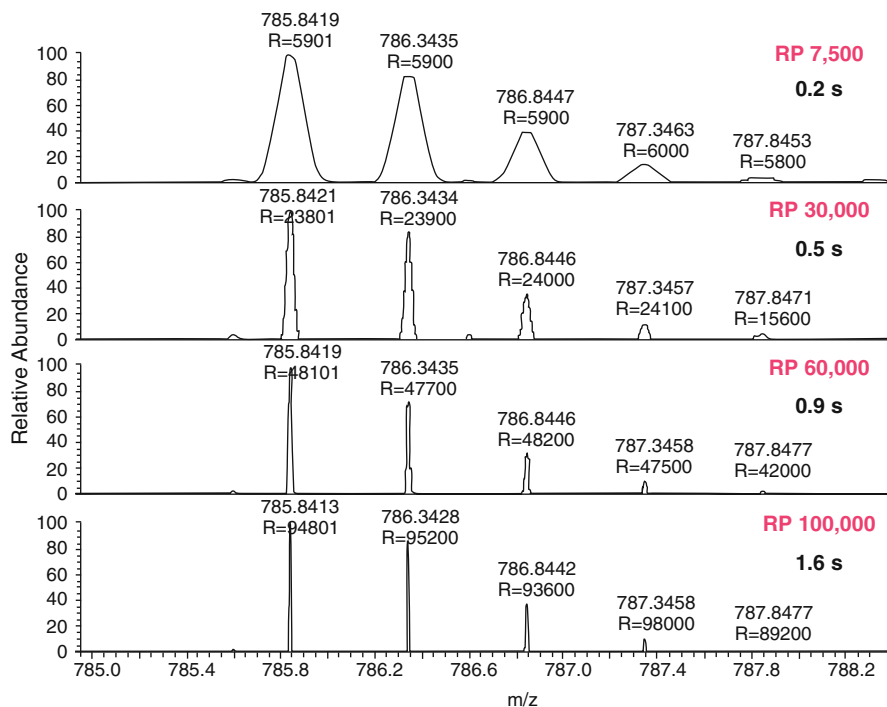


Fig. 4.80 Resolving power of a commercial Orbitrap instrument as achieved for doubly charged peptide ions at detection intervals ranging from 95 to 1267 ms resulting in cycle times from 0.2 to 1.6 s. The cycle times are longer than pure detection intervals due to preparation of ion packets, data processing etc. The values specified are calculated with reference to the manufacturer's standard value of m/z 400 (Reproduced from Ref. [241] with permission. © Wiley-VCH, Weinheim, 2006)

- Initial ion velocity and velocity distribution are important.
- Timing of the injection and its duration need to be carefully adjusted.
- Dosage of ions to achieve optimum ion population in the Orbitrap is required.
- Ultrahigh vacuum may not be interrupted to warrant the mean free path for tens to hundreds of thousands of undisturbed revolutions around the central electrode.

Thus, a bent RF-only quadrupole is employed to accumulate, store, and thermalize the ions by a low pressure of nitrogen prior to injection. Derived from the shape of the RF section in the form of the letter “C” this part has been termed the *C-trap*. The C-trap can be filled with about a million elementary charges. Collisional damping is important, because this way the ions are brought to rest in the middle of the C-trap. Nitrogen is used for that purpose as it is already used in the source region of the instrument and it is efficient at capturing and cooling the ions. In other words, the C-trap decouples the Orbitrap from all preceding steps of ion generation, desolvation, and eventually precursor ion selection [250].

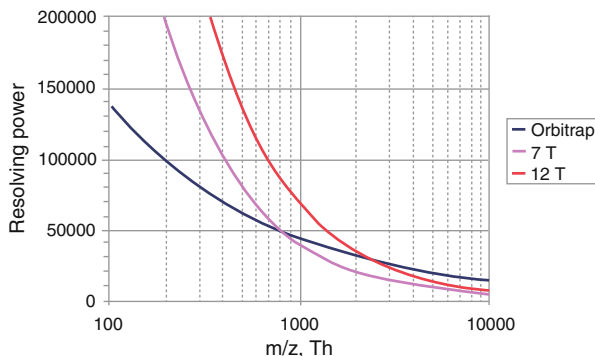


Fig. 4.81 For an Orbitrap analyzer the drop in resolving power with increasing m/z is less pronounced than for FT-ICR instruments. While FT-ICR clearly outperforms Orbitraps up to m/z 8000 (7 T, pink line) or even m/z 2500 (12 T, red line) the Orbitrap can deliver somewhat better resolving power in the high mass range (blue line) (Reproduced from Ref. [241] with permission. © Wiley-VCH, Weinheim, 2006)

High-voltage electric pulses with short rise times in the order of few hundreds of nanoseconds serve to eject the ions from the C-trap through the gap between the inner pair of quadrupole rods along lines converging on the entrance of the Orbitrap. By lowering the electric potential of the central electrode simultaneously with the entry of the ion packets, ions are captured and start circling. Typically, the ions are injected at kinetic energies of about 1.3 keV while the central electrode is set to -3.4 kV (for positive-ion mode) [245]. The initial bunches become reshaped into rings that oscillate axially along the central electrode. The amplitude of these oscillations is determined by the initial offset of ion injection from the Orbitrap center, whereas coherency of axial oscillations, i.e., maintenance of thin rings, is ensured by the short temporal duration of ion packet injection (Fig. 4.82).

One Orbitrap cycle

Ions are collected and thermalized in the C-trap and are injected as a focused beam off-center into the Orbitrap. The electric field of the Orbitrap is increased during the period of injection to compress the ion cloud towards the center. The ions thus are rotating around the central spindle electrode, and in addition, perform radial as well as axial oscillations. After stabilization of the high voltage, the axial oscillation proportional to $(q/m)^{1/2}$ is recorded via image current detection using the pair of outer electrodes.

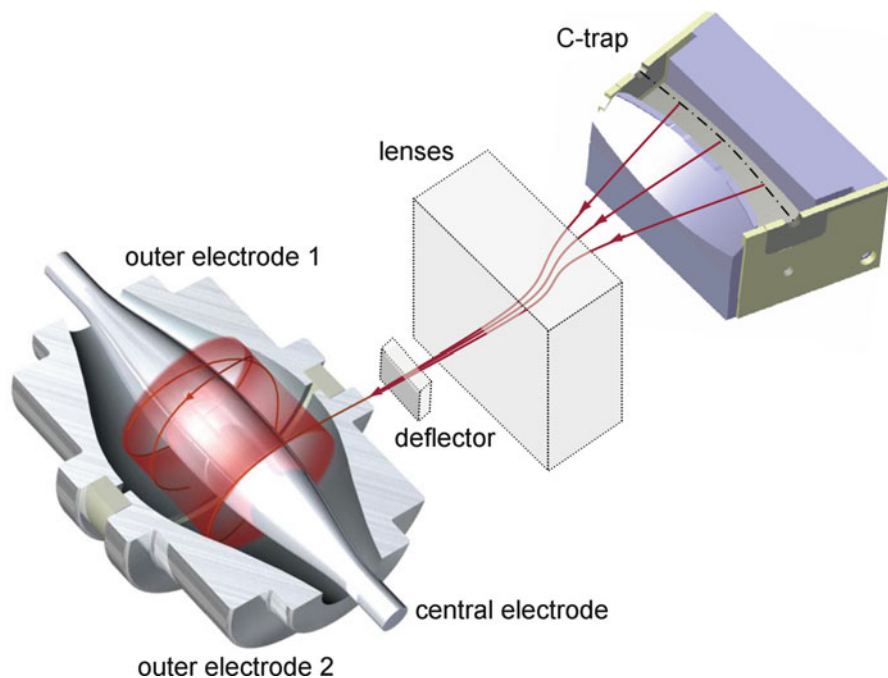


Fig. 4.82 The Orbitrap mass analyzer with ions being injected from the C-trap through lenses and a deflector. During injection, the C-trap acts as a convex lens with the outer rods pushing and the inner short rods pulling the ions by a DC pulse. Trapping voltage is applied to the central electrode (Courtesy of A. Makarov, Thermo Fisher Scientific)

4.8.4 Hybridization with a Linear Quadrupole Ion Trap

To become an analytically useful mass spectrometer, the above combination still needs to be interfaced to an ion source. The prototype implementation of the Orbitrap made use of laser desorption/ionization in the immediate vicinity of the Orbitrap [240], but soon, an external electrospray ion source followed [249]. For highest versatility, the Orbitrap has been attached to the rear of a fully functional Thermo Fisher LTQ instrument (cf. Sect. 4.5.4 and Fig. 4.50). The LIT may either be operated on its own as it still is equipped with SEM detectors or it may be axially emptied into the C-trap via an RF-only transfer octopole. The entire setup, dubbed LTQ-Orbitrap, is shown in Fig. 4.83. This instrument offers both low-resolution MS and MSⁿ operation in the LTQ section and final high-resolving m/z analysis at ppm-accuracy of whatever ions decided to be sent into the Orbitrap [241–244, 250]. A differential pumping system reduces the pressure along the instrument to achieve about 2×10^{-10} mbar in the Orbitrap. While Orbitrap technology has strongly advanced, there is still ongoing research for further improvements [251–255].

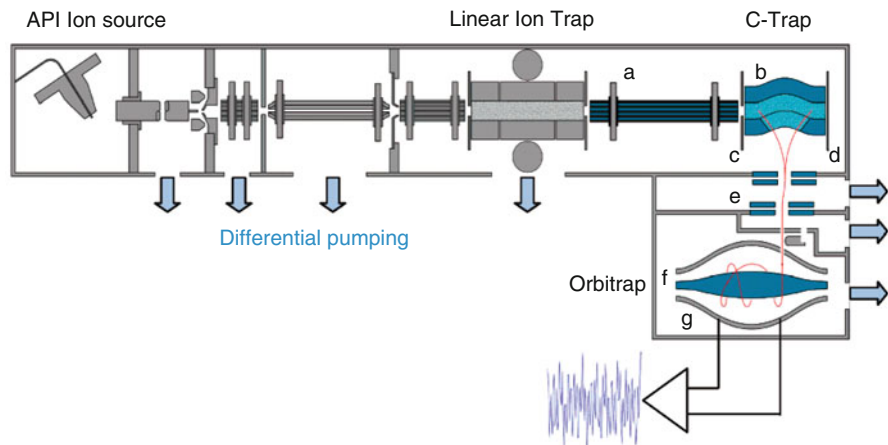


Fig. 4.83 The Thermo Scientific LTQ Orbitrap mass spectrometer. The front end up to the LIT is identical to the LTQ instrument introduced in Sect. 4.5.3 and Fig. 4.41. Ions axially ejected from the LIT are entering (a) a transfer octopole to (b) a curved RF-only quadrupole known as C-trap, from where they are injected via (c) gate electrode, (d) trap electrode, and (e) ion optics into the Orbitrap comprising (f) the inner electrode and (g) outer electrodes for detection. Note that there are four ports for differential pumping along the LTQ section and another three sideways to reduce the pressure from the C-trap to the Orbitrap (Adapted from Ref. [243] with permission. © American Chemical Society, 2006)

4.8.5 Orbitrap at a Glance

Mass Analysis in the Orbitrap

In an Orbitrap ions are captured by electrostatic attraction of a spindle-shaped central electrode provided they are entering the trapping field in a tangential direction. Proper ion injection in terms of kinetic energy, spatial focusing, and timing is achieved by radial ejection of ion bunches from a C-shaped quadrupole ion trap. The resulting ionic motion inside the Orbitrap is a superimposition of circulation around the central electrode and oscillation along the axis of the same. The longitudinal oscillation is caused by the electric field gradient along the spindle axis. The oscillation is recorded in the time domain via image current detection by two outer electrodes. The frequency is then obtained by FT of the recorded transient and used to calculate m/z and abundance of the ions in the Orbitrap.

Performance Characteristics

The main features of the Orbitrap are high resolving power and accurate mass. The level of both depends on the actual Orbitrap model and the exact mode of operation. Typically, spectra are acquired at a resolving power of $R = 20,000\text{--}200,000$ and mass accuracy is in the order of 0.5–3 ppm.

Growing Orbitrap Family

Since the introduction of the first instrument featuring an Orbitrap mass analyzer, the array of instruments has continuously been growing. In between, the range includes benchtop systems purely offering HR-MS for routine LC-MS and lately also GC-MS plus benchtop systems with tandem MS capabilities due to a Q-Orbitrap design. Instruments of increasing sophistication with LIT and even dual-LIT frontends and other features complement the Orbitrap family of instruments. Some of them will be discussed in the context of tandem MS (Sect. 9.10). The Orbitrap is set apart from all other types of mass analyzers not only by its unique working principle but also by the fact of being exclusively commercialized by a single company, Thermo Fisher.

4.9 Hybrid Instruments

As anticipated in the sections on linear ion traps (Sect. 4.5.4), modern Fourier transform-ion cyclotron resonance (Sect. 4.7.12), and LIT-Orbitrap mass spectrometers (Sect. 4.8.4), instruments can efficiently be designed by combining different types of mass analyzers and ion-guiding devices in a single so-called *hybrid instrument* [256, 257]. By these means one can obtain mass spectrometers that unite the advantageous properties of each mass analyzer they are composed of.

Hybrid mass spectrometers combine the expertise of the various highly developed dedicated devices and mass-analyzing, ion-guiding, ion-accumulating, and ion-focusing elements in a way that ensures the most versatile and yet economic solution. The design of a hybrid instrument may aim at:

- achieving highest resolving power and accuracy,
- boosting speed and sensitivity,
- realizing a compact and versatile yet affordable multi-purpose instrument.

Budgetary aspects are an important issue in favor of hybridization because each stage is selected as to deliver optimum performance at lowest cost. Hybrids are ideally employed for tandem mass spectrometry, for instance. In tandem mass spectrometers the first stage of m/z analysis (MS1) is used to select ions for further fragmentation and subsequent analysis of the product ions in a second m/z analyzer (MS2, Chap. 9). It is generally sufficient to combine a low-resolution MS1 unit with a high-resolution MS2.

Table 4.2 Hybrid mass analyzers.

MS1	Properties of MS1	MS2	Properties of MS2
BE or EB	LR and HR	qQ	LR, low energy CID
BE or EB	LR and HR	QIT	LR, low energy CID, MS ⁿ
EB or EBE	LR and HR	oaTOF	LR, low energy CID, high sensitivity
Qq	LR, low-energy CID	oaTOF	high resolution and mass accuracy, high sensitivity
Qq	LR, low-energy CID	LIT	LR, higher sensitivity than QqQ, MS/MS in LIT
Qq	LR, low-energy CID	Orbitrap	High resolution and mass accuracy
QIT	LR, low-energy CID, MS ⁿ	TOF	HR, high sensitivity
LIT	LR, low-energy CID, MS ⁿ	Orbitrap	High to ultrahigh resolution and mass accuracy
Qq	LR, low-energy CID, MS ²	ICR	Ultrahigh resolution and mass accuracy, MS/MS in ICR
LIT	LR, low-energy CID, MS ⁿ	ICR	Ultrahigh resolution and mass accuracy, MS/MS in ICR

4.9.1 Evolution of Hybrid Mass Spectrometers

The development of hybrid instruments started from magnetic sector-quadrupole hybrids, either BqQ [258, 259], EBqQ, [260] or BEqQ [261–263]. Numerous other systems such as magnetic sector-QIT [264], magnetic sector-*oa*TOF [265, 266], QITTOF [159, 267, 268], QqTOF [55, 269–271], QqLIT [129], LIT-ICR, and QqICR followed. LIT-Orbitraps present the most recent addition [241, 242, 252, 253] (Table 4.2).

The adaptation of conceptually different mass analyzers to each other may demand for sophisticated interfaces, because of the largely differing requirements concerning ion kinetic energies. The magnetic sector-quadrupole or magnetic sector-QIT hybrids, for example, require keV ions exiting the sector to be decelerated to some 10 eV before entering the qQ section, or to be slowed down and pulsed into the QIT, respectively. Due to the bulky and demanding magnetic sector analyzer, hybrids of that type do not anymore play a role.

Geometries composed of an *oa*TOF as second analyzer bear the advantage that advanced TOFs offer accurate mass measurements equaling the accuracy of magnetic sector instruments. While their linear quadrupole front end serves as MS1 in tandem MS experiments, it is operated in RF-only mode when tandem MS is not intended, because this allows to acquire full-range spectra at high resolution using the TOF analyzer (MS2, Fig. 4.84). It should be noted that the first quadrupole of hybrids with Qq as MS1, i.e., Qq-TOF hybrids, typically offers mass-selective operation covering an *m/z* range different from the range in RF-only operation, e.g., *m/z* 50–4000 in mass-selective and *m/z* 50–10,000 in RF-only transmission mode.

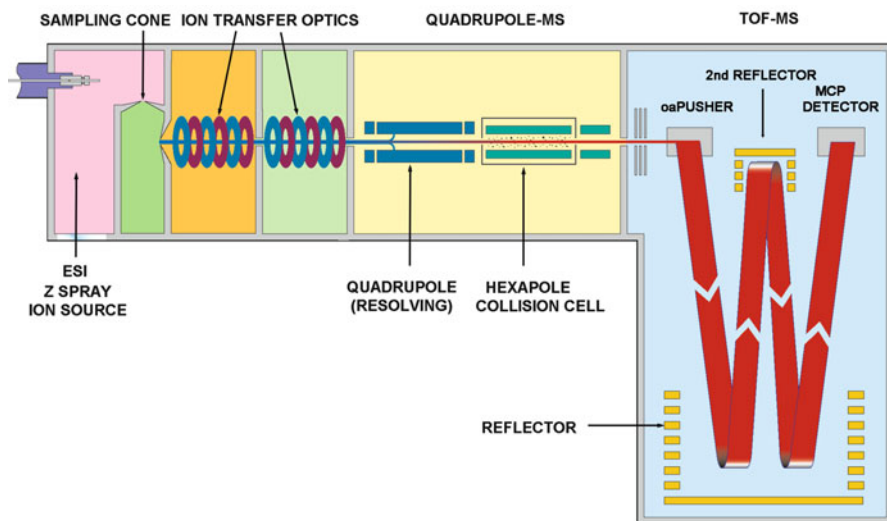


Fig. 4.84 The Q-TOF Ultima, Qh-oaTOF design, with ESI ion source in MS/MS mode. The TOF analyzer has a reflector that can either be operated using the large reflector alone (V-mode) or adding a second stage of ion reflection (W-mode) for higher resolving power (Courtesy of Waters Corporation, MS Technologies, Manchester, UK)

Widespread in use

Besides accommodating to their versatility, there is nothing new to understand with hybrid instruments. Exotic at a first glance, hybrids are governing today's market of mass spectrometers [133–135].

There is very strong competition between high-end QqTOF instruments, on the one side, and Qq-Orbitrap and LIT-Orbitrap hybrid instruments like the aforementioned LTQ-Orbitrap (Fig. 4.83), on the other. The Orbitrap instrument family shows remarkable flexibility in terms of how the Orbitrap analyzer is implemented as part of a complex hybrid system. The range not only includes Qq-Orbitrap and LIT-Orbitrap hybrids but recently even a Q-Orbitrap-tandemLIT configuration. The latter instrument, the Orbitrap Fusion is marketed as a *tribrid* because it incorporates three different types of mass analyzers (Fig. 4.85) [254, 255]. The purpose of the tandem LIT is to provide a higher-pressure LIT for precursor ion selection and ion fragmentation plus a lower-pressure LIT for effective mass analysis. The Orbitrap Fusion architecture permits a multitude of operational modes that allow tandem MS experiments to be run in parallel while a full range survey scan delivers accurate mass data of the next package of precursors to be interrogated or accurate mass of fragments.

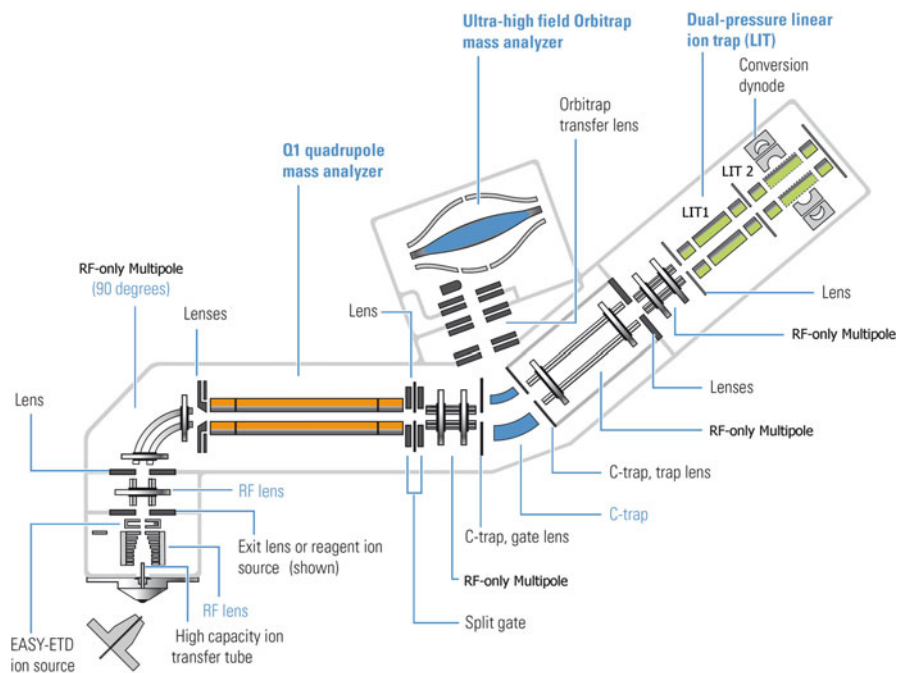


Fig. 4.85 The Orbitrap Fusion Lumos tribrid mass spectrometer. The first RF-only multipole is bent by 90° to get rid of neutrals before ions are entering the analyzer section comprising quadrupole (orange), Orbitrap (blue), and LIT/LIT (green) (Adapted from Thermo Fisher technical documentation with kind permission. © Thermo Fisher Scientific, Bremen, 2015)

The highest level of resolving power and mass accuracy can be achieved by replacing the oaTOF section with a FT-ICR analyzer. Those high-end hybrid instruments are either available as Qh-ICR by employing a quadrupole as first mass analyzer (Bruker Daltonik APEX-Q and Solarix instruments, Fig. 4.78) or as LIT-ICR, i.e., with a linear ion trap in front of the ICR cell (Thermo Scientific LTQ-FT series, Fig. 4.86).

4.10 Ion Mobility-Mass Spectrometry Systems

There is an increasing interest in *ion mobility spectrometry* (IMS) as it presents an effective means of separating gaseous ions [272, 273]. In IMS an electric field forces the ions to drift along a path through a countercurrent inert gas atmosphere whereby they are separated due to their collision cross sections. IMS does for gaseous ions what gas chromatography does for gaseous neutrals, and in fact, IMS was initially referred to as *plasma chromatography* (PC). IMS can separate isobaric ions of different charge state (size-to-charge ratio) resulting from their distinct speed of propagation along the electric field of the ion mobility tube or

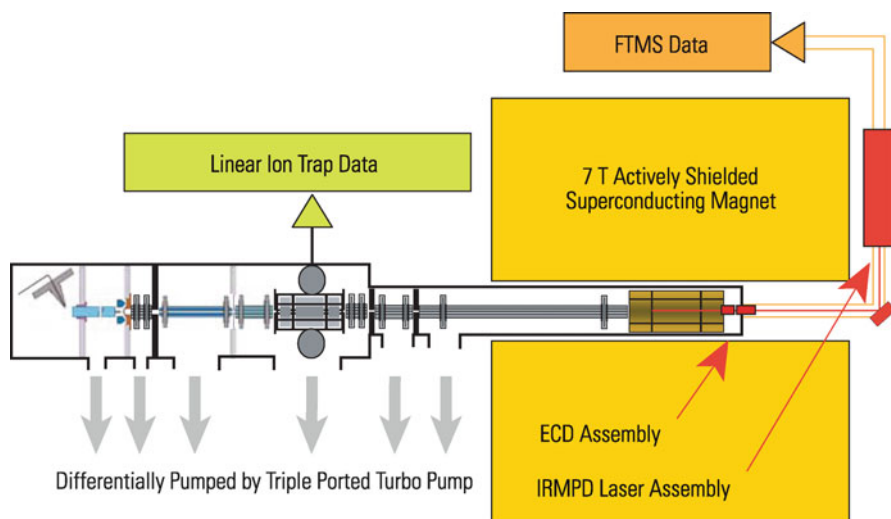


Fig. 4.86 Schematic of a LIT-FT-ICR hybrid instrument, the Thermo Scientific LTQ FT Ultra, incorporating a fully functional LTQ front end (as in LTQ Orbitrap) for highest versatility (Courtesy Thermo Fisher Scientific, Bremen)

distinguish isobars of the same charge state by their steric properties, i.e., it separates isomers and conformers alike by their shape. Thus, IMS is a valuable aid in biomolecular analysis [274–276].

Clearly, mass spectrometry is perfectly suited for the detection for gaseous ions eluting from an ion mobility device. Therefore, *ion mobility-mass spectrometry* (IM-MS) coupling has received considerable attention since the 1970s [277–279]. The IM-MS instrument provides the following functional features [272]:

- transfer of gaseous sample into the ion source,
- ion formation from neutral sample molecules at atmospheric pressure,
- accumulation of an ion package and injection into the drift region,
- measurement of drift velocities of the swarms of ions while passing the electric field of the drift region in a drift gas atmosphere, and
- detection of ions by a mass analyzer coupled to the IMS stage.

Hybrid, hyphenation, or something in between?

While a detailed treatment of ion mobility spectrometry is beyond the scope of this book, it is certainly useful to provide a brief description of the technique [272, 273]. In principle, IM-MS systems can be regarded as hyphenated instrumentation (for applications cf. Sect. 14.6) because the peculiarities of ion mobility demand an integrated instrumental approach.

(continued)

This distinguishes IM-MS from gas or liquid chromatography couplings to MS that may be coupled to and decoupled from a mass spectrometer as required [274, 280]. Therefore, IM-MS is dealt with here as a special case of hybridization.

4.10.1 Ion Mobility Separation

Ion mobility effects separation of ions based on their different velocities when accelerated by a constant electric field along a drift tube with a countercurrent inert gas, typically helium or nitrogen. The average velocity, v_D , of a drifting ion is then governed by the number of soft collisions it experiences within the drift tube. This number of collisions with the neutrals is directly proportional to the electric field strength, E , and the ion mobility constant K (in $\text{cm}^2 \text{V}^{-1} \text{s}^{-1}$).

$$v_D = K E \quad (4.50)$$

The value of K depends on the ion and the drift gas. Equation (4.50) is only valid up to field strengths of about 1000 V cm^{-1} , whereas above that electric field strength the proportionality between K and E is canceled [274].

The electric field needs to be weak enough so that collisions at given gas density dampen the ions to achieve an internal ion energy in equilibrium with the temperature of the bath gas [276]. Furthermore, gas discharges have strictly to be avoided. In the high-pressure regime (133–1013 mbar or 100–760 Torr) drift tubes are operated at $100\text{--}300 \text{ V cm}^{-1}$ to deliver what in IMS is considered as high resolving power of 100–300. In the low-pressure regime, field strengths are limited to $10\text{--}30 \text{ V cm}^{-1}$. Unfortunately, lower pressure goes along with reduced resolving power of the device while coupling to mass analyzers is simplified due to reduced load on the vacuum system [276].

In the low-field regime, the value of K can be calculated from

$$K = \frac{3q}{16N} \sqrt{\frac{2\pi}{kT}} \sqrt{\left(\frac{m_g + m_i}{m_g m_i}\right)} \left(\frac{1}{\Omega}\right) \quad (4.51)$$

where q is the ionic charge, N the number density of the buffer gas, k is Boltzmann's constant, T is the absolute temperature, m_g is the mass of the buffer gas molecules, and m_i is the mass of the ions that have the collision cross section Ω [275, 280].

In the IM-MS experiment, q and Ω are a priori unknown, but m_i is derived from m/z as soon as the charge state z has been identified, which in turn delivers q from

$q = ze$. As hundreds of TOF mass spectra can be acquired during the tens of milliseconds required for one ion mobility run, the setup easily delivers high-quality MS data to identify the drift time-separated ions.

The reduced mobility, K_0 , is calculated for comparing IMS data between runs obtained at different buffer gas temperature and pressure and also across different instruments. The reduced mobility, K_0 , is obtained from:

$$K_0 = \frac{l_D^2}{t_D U_D} \frac{T_0}{T} \frac{p}{p_0} \quad (4.52)$$

where l_D is the length of the drift tube and U_D the voltage applied along it; the temperature is given in units of Kelvin ($T_0 = 273.2$ K) and the pressure in units of millibar ($p_0 = 1013$ mbar). K_0 has the physical dimension of $\text{cm}^2 \text{V}^{-1} \text{s}^{-1}$. Depending on the source, the equation for the reduced mobility may also be stated in the literature using the electric field strength instead of the voltage and the pressure in Torr:

$$K_0 = \frac{l_D}{t_D E_D} \frac{273.2 \text{ K}}{T} \frac{p}{760 \text{ Torr}} \quad (4.52a)$$

where l_D is the length of the drift tube and E_D the voltage applied divided by l_D [276].

For this classical approach to IMS, the theory of ion propagation is very well developed and allows to calculate the orientationally averaged collision cross sections with high confidence [275].

IM-TOF-MS The mass analyzer of an IM-MS instrument must be able to deliver a spectral acquisition rate that allows to collect mass spectra faster than the time span for elution of an IMS peak. As ion mobility separation proceeds in the order of tens of milliseconds, a typical IMS resolving power in the order of 100 implies that at least 100 mass spectra have to be acquired per IMS run. Only TOF analyzers are capable of delivering spectra at 100–1000 Hz, and thus, the IM-TOF-MS hybrid presents the natural combination for IM-MS (Fig. 4.87).

4.10.2 Stacked Ring Ion Guide

As an alternative to RF-only multipole ion guides, the *stacked ring ion guide* (SRIG) has been newly recognized since 2004. Ring electrodes (2–3 mm i.d.) are aligned with 1–2 mm insulating ceramics spacers in between them and supplied with an RF drive voltage ($U_{\text{RF}} \approx 100$ V at 1 MHz) that is reversed in phase between adjacent rings (Fig. 4.88) [118, 281]. Ions entering the SRIG experience a deep radial potential well with comparatively steep walls towards the inner ring surfaces when traveling through the apertures. The SRIG offers high transmission if operated with a thermalizing buffer gas at around 3 mbar. Interestingly, the SRIG not merely

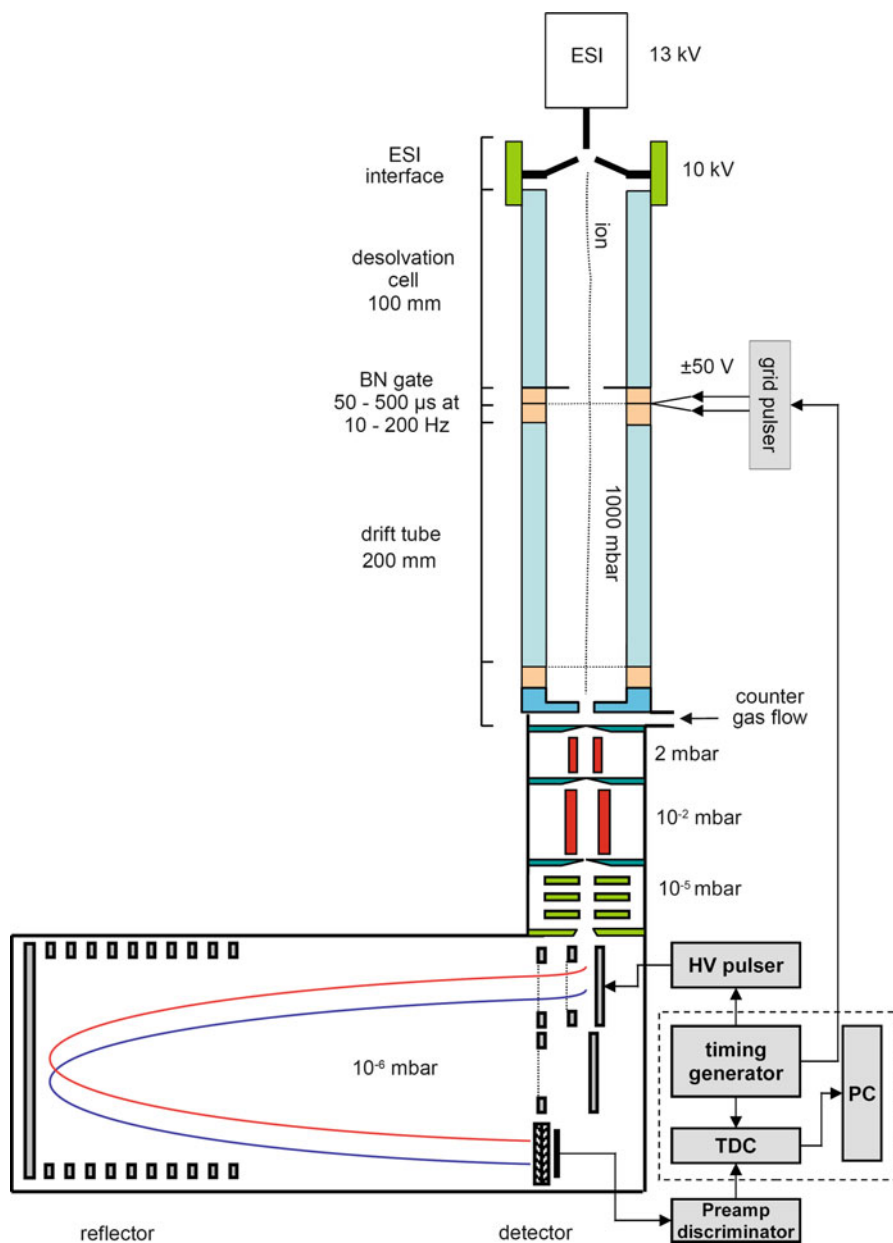


Fig. 4.87 Basic design of an ambient-pressure IMS-TOF mass spectrometer. Ions from an electrospray source are entering a desolvation chamber from where packets are pulsed into the ion mobility tube by means of a Bradbury-Nielsen (BN) ion gate. The ion path is shown uneven to indicate diffusion of ions. After ion mobility separation the ions are transferred into the reflector via a differentially pumped interface (Courtesy of ToFwerk AG, Thun, Switzerland)

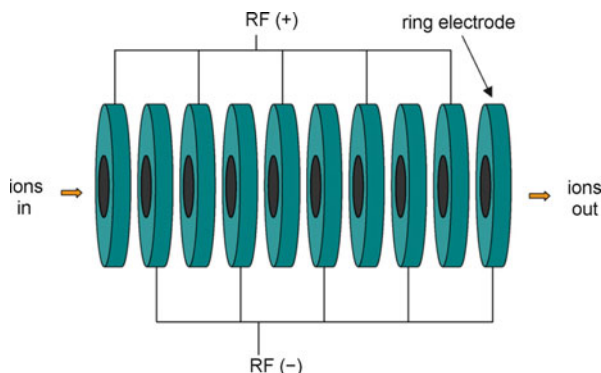


Fig. 4.88 A stacked ring ion guide. Rings are connected to an RF drive voltage in alteration of the phase. Normally tens of pairs are used to build one ion guide. Ions entering from the left experience a deep radial potential well with comparatively steep walls toward the inner ring surfaces when traveling through the apertures (Reproduced from Ref. [281] with permission. © Elsevier Science Publishers, 2007)

forms a kind of pipe for the ions, its effective potential more resembles a corrugated hose where the grooves act as low potential wells in axial direction, which are deep enough to restrain axial drift of thermalized ions by soft trapping.

To avoid stopping of the ions, a DC pulse can be delivered to a pair of rings causing the ions to move forth to the next potential groove. If the DC pulse makes a progression from pair to pair it creates a traveling wave (T-wave) that makes the ions “surf” along the SRIG (Fig. 4.89).

Such *traveling wave ion guides* (TWIGs) are incorporated in many Waters instruments to replace the more traditional RF-only multipoles as ion guides and collision cells, e.g., in the “triplequadrupoles” of the Xevo™ and Quattro Premier™ series that essentially are of Q-TWIG-Q design. The wave created by a potential of about 2 V is generally propagating at around 300 m s^{-1} . This provides an effective means of minimizing dwell times in the corresponding compartment.

4.10.3 Traveling Wave Ion Guides for IMS

When ions differing either in charge state or collision cross sections, or both, are entering the TWIG, the less mobile ones may occasionally transverse a wave in backward direction. Those ions lagging behind the traveling wave will exit later than those surfing on the wave. This makes the TWIG become an ion mobility separator.

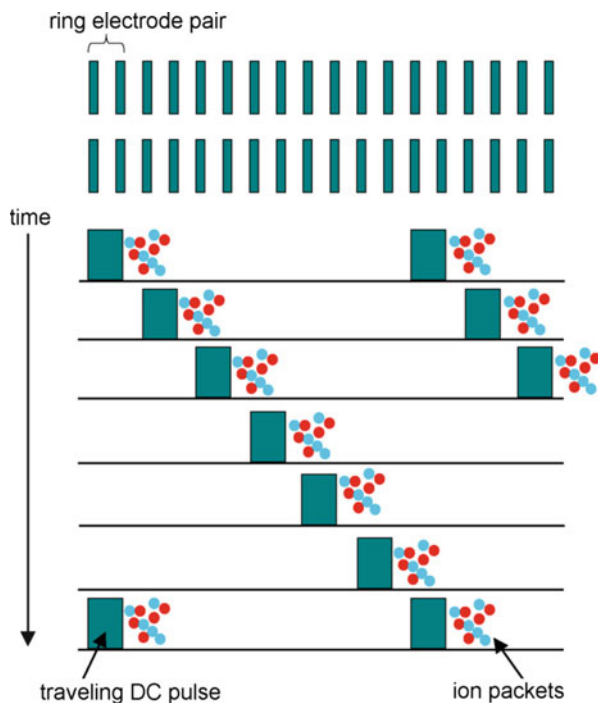


Fig. 4.89 Effect of a traveling wave DC pulse along a stacked ring ion guide. Ions in front of the DC pulse are moving along from stack to stack and are thus propelled through the device (T-wave ion guide). A buffer gas is required to narrow down the thermal energy distribution (Reproduced from Ref. [281] with permission. © Elsevier Science Publishers, 2007)

Traveling wave

A specific type of IM-MS instrumentation using a *traveling-wave* (T-wave™) approach is available from Waters. In a T-wave ion mobility device ions are pushed by low-voltage waves established along a large stack of paired ring electrodes. However, the theory of ion mobility separation in the T-wave is not as fully understood as in traditional IMS devices [275, 280].

Obviously, multi-RF-ring electrode devices can be designed, optimized, and operated in numerous ways to

- guide ions on their transit from one instrument stage to another or across a pumping stage,
- keep ions on track while they are subjected to collisions with gas for excitation and fragmentation,



Fig. 4.90 Waters TriWave as incorporated in Synapt G2 instruments for ion mobility separation. Ions entering from the *left* are accumulated in the first section acting as the ion trap, then batch wise admitted into the ion mobility separation zone, and finally collected for transfer into the oaTOF analyzer (Adapted with permission. Courtesy of Waters MS Technologies)

- admit, stop, and collect ions to accumulate packets for subsequent IMS or mass analysis,
- provide ion mobility separation.

Compartments serving either purpose can be combined to form a linear operational unit as part of a more complex hybrid mass spectrometer (Fig. 4.90). With the exception of IMS, which is performed at 100–200 mbar of buffer gas countercurrent to the ion motion, multi-RF-ring electrode devices are typically operated in the 0.1–10 mbar pressure range. Thus, they are compatible with all sorts of applications of RF multipole ion guides.

4.10.4 Hybrid Instruments with IMS

A hybrid instrument comprising a mass-selecting quadrupole, a traveling wave ion mobility separator, and an oaTOF analyzer has been marketed by Waters as Synapt series of instruments (Fig. 4.91) [118, 281]. Additionally, this instrument incorporates a RF-ring electrode device in the interface region from ion source to the first mass-analyzing quadrupole. We will resume this topic in the context of interface design for electrospray ionization (Sect. 12.2).

Waters was the first company to offer IMS-tandem MS combinations and still seems to have the widest range of IM-MS instruments. More recently, Agilent (6560 Ion Mobility Q-TOF LC/MS) as well as Bruker with a new concept of *trapped ion mobility* (timsTOF) have also included this type of instrumentation in their portfolio. The designs are becoming more diverse as the technique receives more widespread use. Nonetheless, all IMS-tandem MS instruments rely on oaTOF as the final stage of mass analysis due to its unique combination of acquisition rate and resolving power.

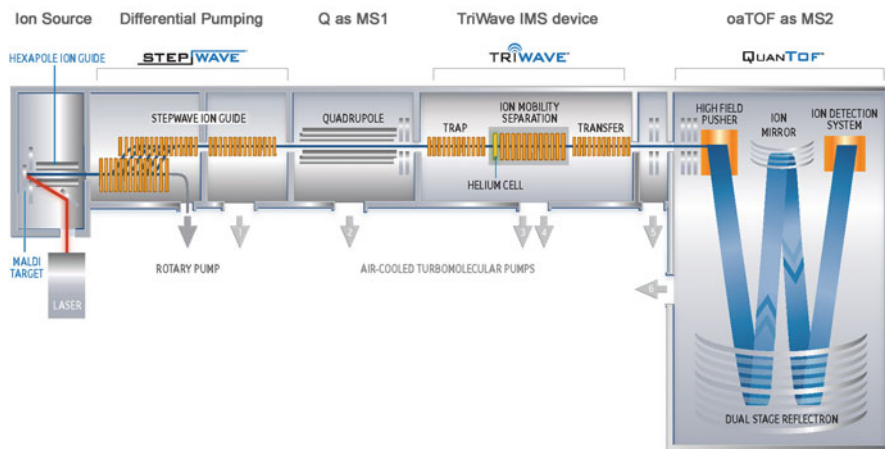


Fig. 4.91 The Waters Synapt G2-Si, a Q-IMS-*oaTOF* hybrid, here shown with MALDI source. The combination of three ring ion guide sections is used to build a complete IMS device comprising a trap at the entrance to supply ion packages, the IMS itself, and an ion guide for transfer to the mass analyzer (cf. *TriWave* in Fig. 4.89) (Adapted with permission. Courtesy of Waters MS Technologies)

4.10.5 Overview of Hybrid Instrumentation Including IM-MS

Classification

Mass spectrometers composed of different types of mass analyzers and ion-guiding devices are termed *hybrid instruments*. The components are combined in a way as to obtain mass spectrometers uniting the advantages of each subunit they are composed of. Thus, hybrids incorporate mass-analyzing, ion-guiding, ion-accumulating, ion separating, and ion-focusing elements in a way that ensures the most versatile and yet economic solution to obtaining a certain type of instrument.

Types of IMS

Drift tube ion mobility (DT-IMS) is the classical form of IMS. *Travelling-wave ion mobility* (TW-IMS) has been introduced and is marketed by Waters. In addition, there are *field asymmetric ion mobility* (FAIMS) and *differential ion mobility* (DMS) [282–284]. FAIMS devices are very compact and can externally be fitted to existing instruments with electrospray interface.

Relevant Representatives of Hybrid Instruments

Most newly introduced mass spectrometers are hybrid instruments in one way or another. Typically, they are designed as tandem mass spectrometers with a low-resolving first stage of m/z analysis (MS1) for precursor ion selection, e.g., Q, QIT, or LIT, and a high-resolving second stage for product ion analysis (MS2), e.g., *oaTOF*, Orbitrap, or FT-ICR.

Another family of hybrids includes ion mobility separation either in front of the mass spectrometer section or between MS1 and MS2. More widespread acceptance of IM-MS and instrument design by different manufacturers is leading to an increased diversity of instrumentation and modes of operation. Due to speed and sensitivity requirements, all dedicated IMS-tandem MS instruments rely on oaTOF as the final stage of mass analysis due to its unique combination of acquisition rate, duty cycle, and resolving power.

4.11 Ion Detection

The simplest detector is a *Faraday cup*, i.e., an electrode where the ions deposit their charge. The electric current flowing away from that electrode results in a voltage when passing through a resistor of high impedance. Faraday cups are still in use to measure abundance ratios with highest accuracy in *isotope ratio mass spectrometry* (IR-MS) [285]. Early in the era of Mattauch-Herzog-type instruments, the *photographic plate* has been the standard detection system (Sect. 4.3.5). With the advent of scanning mass spectrometers, *secondary electron multipliers* (SEM) became predominant [286]. These rely on the emission of secondary electrons from surfaces upon impact of energetic ions. Ion-counting detectors are not used in FT-ICR and Orbitrap instruments where *image current detection* is employed instead.

4.11.1 Analog-to-Digital Conversion

Ion packages of adjacent m/z values hit the detector very shortly after each other causing the signal to change at very high frequency. This requires the use of GHz-frequency digitizers for *analog-to-digital conversion*. Obviously, the final peak shape directly depends on the speed of the *analog-to-digital converter* (ADC) [45].

In case of an 8-bit ADC, for example, the intensity of the detector output is converted into a numerical value of 0–255 [287]. The *dynamic range* is the ratio obtained by dividing the intensity of the most intense signal by that of the weakest while both are correctly detected in the same spectrum. To improve the small dynamic range delivered by 8-bit ADCs (0–255), several tens to a few hundred single spectra are usually summed up. Most recent TOF and oaTOF instruments are therefore equipped with 8-bit or even 10-bit ADCs to provide a dynamic range of 10^4 – 10^5 after summation of several individual spectra.

Slower scanning instruments such as quadrupole, quadrupole ion trap, and magnetic sector instruments are typically equipped with 16–20-bit ADCs corresponding to intensity values of 0–65,535 (2^{16} –1) and 0–1,048,575 (2^{20} –1),

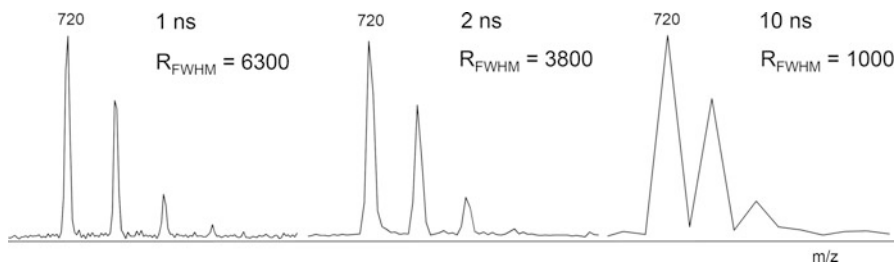


Fig. 4.92 The [60]fullerene molecular ion peak depicted at different settings of the dwell time per data point of the analog-to-digital converter obtained on the aforementioned instrument after PIE upgrade. At 1 ns per data point (1 GHz) the peaks are well resolved and resolution is limited by the analyzer. At 2 ns (500 MHz) some broadening occurs. At 10 ns (100 MHz) peak shapes are reduced to triangles because detection provides just about two points per m/z

respectively. This explains their advantage when a high linear dynamic range is required, e.g., for quantitation.

4.11.2 Digitization Rate

In particular, the resolving power of advanced TOF analyzers creates a need for high-speed ADCs. Modern TOF instruments incorporate 8-bit ADCs with a digitization rate of 4–5 GHz to suit their resolving power of up to $R = 45,000$. The *digitization rate* or *sampling rate* of an ADC may be reported as dwell time per data point, e.g., 1 ns, or as sampling frequency, e.g., 1 GHz (Fig. 4.92). Data points are also shown on a spectrum in Sect. 11.5.

General relevance

These considerations concerning the digitization rate are in no way restricted to TOF instruments but apply to any process of data acquisition. As a rule of thumb, good peak shapes require 6–10 data points per peak. This rule applies analogously to the number of single spectra per eluting chromatographic peak.

4.11.3 Time-to-Digital Conversion

Time-to-digital converters (TDC) had been employed in some early oaTOF instruments instead of analog-to-digital converters because of the much higher speed of TDCs. Speed in terms of sampling rate is needed to reach the high resolution of oaTOF analyzers, and speed in terms of data flow is a prerequisite to handle the enormous number of spectra per second. However, a TDC is a pulse-counting device that offers only 1 bit dynamic range (value 0 or 1) [287]. Detector–

TDC combinations easily suffer from saturation effects as they cannot distinguish the arrival of a single ion from that of several ions arriving simultaneously. The TDC response is therefore not proportional to ion flux. Thus, summation of many single spectra is also necessary to obtain a higher dynamic range via improved signal statistics. Nevertheless, the result is still unsatisfactory for quantitative analysis and for correct isotopic patterns. Furthermore, the dead time between subsequent counting events causes the second of a pair of ions having almost equal arrival times to remain undetected. Dead time effects within ion packages of a given m/z even cause m/z values to shift to the low-mass side (detection of early incoming ions only), which makes empirical dead-time corrections necessary for accurate mass measurements [287, 288].

4.11.4 Discrete Dynode Electron Multipliers

When an energetic particle impinges on the surface of a metal or a semiconductor, secondary electrons are emitted from that surface. The ease of such an emission is determined by the *electron(ic) work function* of the respective material, e.g., BeCu alloy oxide ($w_e \approx 2.4$ eV) [289]. The higher the velocity of the impacting particle [286, 290] and the lower the electron work function of the surface, the larger the number of secondary electrons. If an electrode opposite to the location of emission is held at more positive potential, all emitted electrons will be accelerated towards and hit that surface where they in turn cause the release of several electrons each. The avalanche of electrons produced over 12–18 discrete dynode stages held at about 100 V more positive potential each causes an electric current large enough to be detected by a sensitive preamplifier. Such a detector is called *secondary electron multiplier* (SEM, Fig. 4.93) [291]. The dynodes are normally cup-shaped, but stacks of Venetian blind-like dynodes have also been in use. Due to a certain air sensitivity of the emissive layer and in order to prevent arcing due to the high voltage, electron multipliers require operation in high vacuum.

The ion currents actually reaching the first dynode are chiefly in the picoampere range, but may span over a 10^{-18} – 10^{-9} A range. Depending on the applied voltage, SEMs provide a gain of 10^6 – 10^8 [291]. The resulting current at the electron trap is the input of a nearby preamplifier providing another 10^6 – 10^9 gain. Its output current is then converted to a voltage signal which finally can be translated to an intensity value by means of an analog-to-digital converter (ADC).

How many ions per peak? A singly-charged ion corresponds to a charge of 1.6×10^{-19} C, and 1 A is equal to 1 C s^{-1} . Thus, an ion current of 10^{-15} A = 10^{-15} C s⁻¹ is provided by about 6000 ions per second. If the detection of these ions during a scan in a GC-MS run taking 1 s over the m/z 40–400 range yields a mass spectrum consisting of some 30–60 peaks, this corresponds to 100–200 ions per peak. Such conditions define the detection limit of a scanning mass spectrometer.

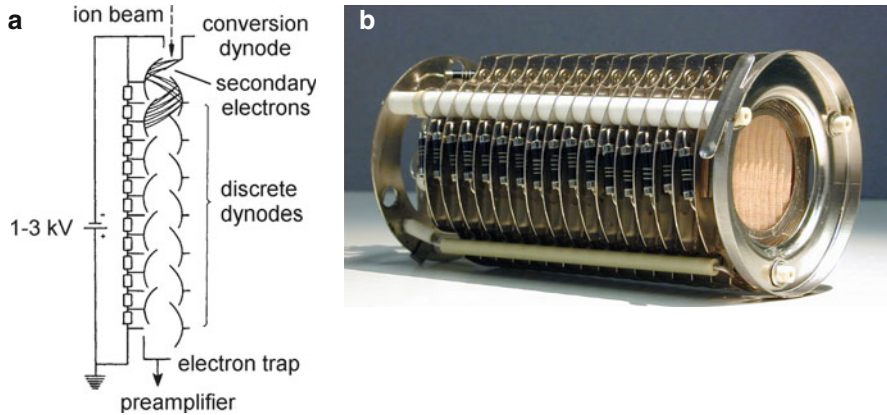


Fig. 4.93 Discrete dynode electron multipliers. (a) Schematic of a 14-stage SEM. (b) An old-fashioned 16-stage Venetian blind-type SEM clearly showing the resistors and ceramics insulators between the stacking dynodes at its side ((a) Adapted from Ref. [292] by permission. © Springer-Verlag Heidelberg, 1991)

Replacement may be on order

All types of secondary electron multipliers have limited life-time. They can deliver 0.1–10 C of extracted charge and are also limited by beam-induced destruction of the first dynode.

4.11.5 Channel Electron Multipliers

The cascade of secondary electrons can also be produced in a continuous tube. Such detectors, known as *channel electron multipliers* (CEM) or just *channeltrons*, are more compact and less expensive than discrete dynode SEMs. CEMs are preferably used in benchtop instruments. Their gain depends on the length-to-diameter ratio with an optimum ratio around 40–80 [293]. In a CEM, the high voltage drops continuously from the ion entrance to the electron exit of the tube requiring a sufficiently high resistance of the semiconducting material to withstand high voltage of about 2 kV. This is accomplished by an emissive layer of silicon dioxide overlying a conductive layer of lead oxide on the supporting heavily lead-doped glass tube [291, 294]. Straight CEMs are unstable at gains exceeding 10^4 because positive ions created inside by EI of residual gas are accelerated towards the input side of the tube where they randomly contribute to the signal causing spurious output pulses [294, 295]. A curved design shortens the free path for ion acceleration thereby suppressing noise from this so-called *ion-feedback*. Curved CEMs provide gains of up to 10^8 (Figs. 4.94 and 4.95).

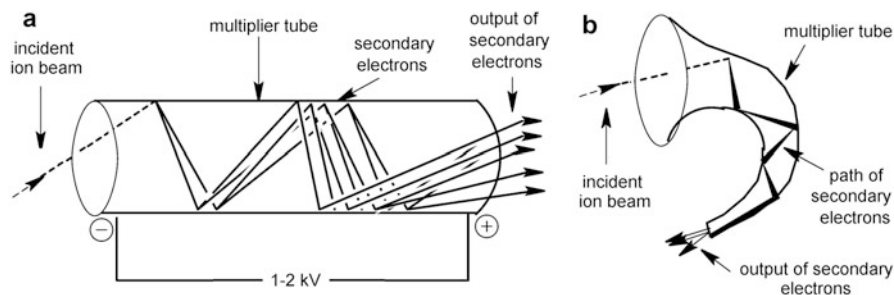


Fig. 4.94 Linear channel electron multiplier (a) and curved channel electron multiplier (b) (By courtesy of Waters Corporation, MS Technologies, Manchester, UK)



Fig. 4.95 Channeltron multiplier. Ions or electrons from a conversion dynode would enter from the left side. Amplification of secondary electrons occurs down the bent tube

Counting all sorts

Ion counting detectors also produce signals upon impact of energetic neutrals, electrons, or photons. Therefore, care has to be taken, not to allow other particles than the mass-analyzed ions to hit the detector.

4.11.6 Microchannel Plates

An extreme reduction of the size of a linear channeltron tube to some micrometers in diameter can be achieved. The cross section of such a single tube is by far too small to be of any use, however, millions of these tubes put together in a “bundle” yield a *channel electron multiplier array*; more common terms are *microchannel plate* or *multichannel plate* (MCP, Fig. 4.96). To avoid that the ions enter the microchannels parallel to their axis, these are inclined by some degrees from the perpendicular to the plate’s surface. The gain of an MCP is 10^3 – 10^4 , i.e., much lower than that of a SEM or CEM. Instead of a single MCP, two MCPs are often sandwiched together in such a way that the small angles oppose each other

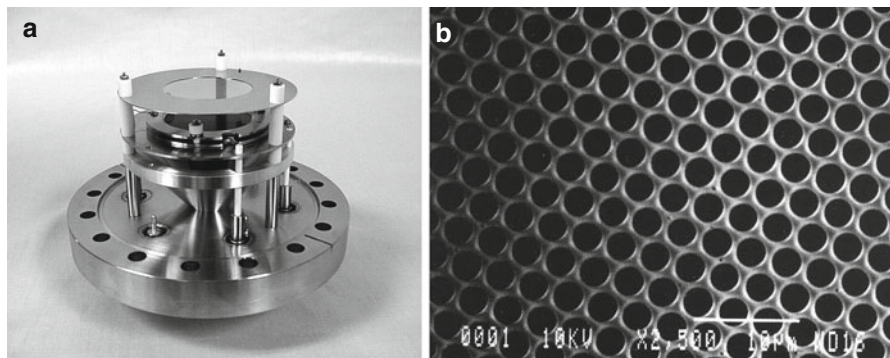


Fig. 4.96 MCP detector (top inner, glossy disk) mounted on top of a flange (a) and SEM micrograph of a high-resolving MCP showing channels of 2 μm diameter (b) (By courtesy of (a) R.M. Jordan Company, Grass Valley, CA and of (b) Burle Industries, Baesweiler)

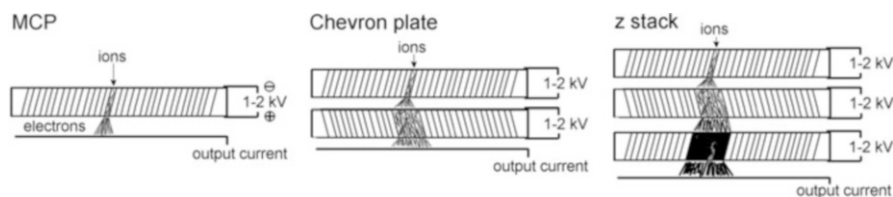


Fig. 4.97 Stacking of MCPs to increase gain. *From left:* single MCP, Chevron plate, and z-stack configuration. Note the loss of spatial resolution upon stacking

(*Chevron plate*, Fig. 4.97) to obtain gains of 10^6 – 10^7 . Occasionally, even three MCPs are stacked analogously (*z-stack*, gain up to 10^8) [295, 296].

MCPs are produced as round plates of various sizes. Those of 2–5 cm in diameter are typically employed in mass spectrometers. An MCP may either be operated to give an integral output for all incident ions during a certain time interval, or the location of the impact may be conserved by connecting sectors of the MCP to individual registration channels. The first setup is more widespread, e.g., in TOF-MS to detect the electron current every nanosecond while the ions are arriving at the detector. The second setup can be used for imaging purposes, e.g., to construct an array detector (below).

4.11.7 Post-acceleration and Conversion Dynode

Discrimination of slower ions as compared to faster ions is observed with SEMs [297], CEMs, and MCPs as well [293, 298, 299]. This means a reduction in sensitivity upon reduction of the acceleration voltage of a mass spectrometer, and of course, with increasing ion mass. *Post-acceleration detectors* can reduce such effects and especially help to improve the sensitivity for high-mass ions [290, 299]. In post-

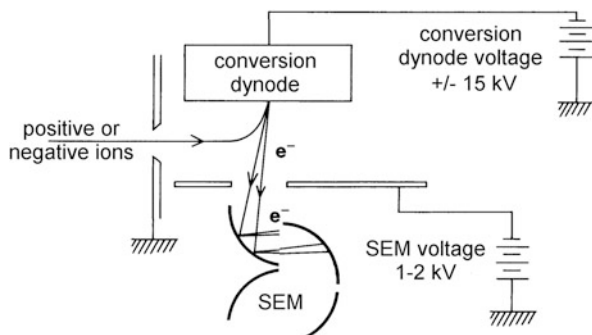


Fig. 4.98 Detector configuration with conversion dynode (By courtesy of JEOL, Tokyo)

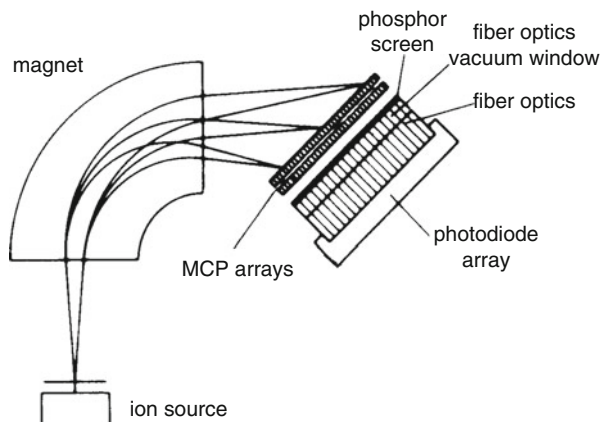
acceleration detectors the ions are accelerated immediately in front of the detector by a voltage of 10–30 kV before they hit the first dynode or the first MCP.

The electron output of ion-counting detectors is usually measured with reference to ground potential, i.e., the first dynode is set to negative high voltage as to achieve acceleration of the electrons down the dynode assembly. In case of sector or TOF instruments, the deceleration of keV negative ions by the detector voltage is of comparatively minor importance. However, the slow ions exiting from quadrupole mass analyzers would stop before they reached the detector. Therefore, *conversion dynodes* are frequently placed in front of the SEM or CEM (Fig. 4.98) [291]. These are robust electrodes set to high potential (5–20 kV) of a polarity suitable to attract the ions actually exiting from the mass analyzer. Their impact on the conversion dynode creates secondary ions or electrons that can be used for subsequent detection. A conversion dynode detector also serves as a post-acceleration detector and gives almost equal sensitivity for positive and negative ion detection. In addition, neutrals and photons cannot reach the detector if the conversion dynode is placed out of the line of sight.

4.11.8 Focal Plane Detectors

Magnetic sector instruments are scanning devices usually focusing ions of one m/z value after the other onto a point detector. However, the mass-dispersive element of these instruments, i.e., the magnetic sector, is capable of producing an image of several neighboring m/z values simultaneously. *Focal plane detectors* (FPD) or *array detectors*, as they are often termed, can detect a small m/z range, i.e., ± 2 –5% of the center mass, at a time [293, 300, 301]. The ions impinging along the focal plane on the surface of an MCP (usually a Chevron plate) are converted to electrons. The electrons from the backside of the MCP stack are then converted into photons by a phosphor screen, and the light image is guided onto a photodiode array or a CCD detector by means of a fiber optical device. Such a multichannel electro-optical detection system typically improves sensitivity or signal-to-noise

Fig. 4.99 Array detector in the focal plane of a magnetic sector to detect a small mass range simultaneously (By courtesy of Thermo Electron (Bremen) GmbH)



ratio, respectively, by a factor of 20–100, because less of the ion current is lost without being detected and fluctuations in the ion current are compensated [302, 303].

The resolution of an FPD is theoretically limited by the number of channels (512–2048). In practice, it is even less because the image suffers some broadening as it passes from the first MCP to the photodiode array (Fig. 4.99). Therefore, instruments with FPD can normally be switched from FPD to SEM detection, e.g., by vertical electrostatic deflection of the ion beam (Finnigan MAT900). Furthermore, quadrupole lenses or an inhomogeneous ESA behind the magnet are employed to achieve variable dispersion, i.e., to zoom the m/z range of simultaneous detection. Recent developments point towards fully integrated FPDs on a silicon chip [304].

4.12 Vacuum Technology

Vacuum systems are integral parts of any mass spectrometer, but vacuum technology definitely is a field of its own [305–309]. Thus the discussion of mass spectrometer vacuum systems will be restricted to the very basics.

4.12.1 Basic Mass Spectrometer Vacuum System

Generally, two pumping stages are employed to generate the high vacuum of a mass spectrometer. Usually, *rotary vane pumps* having *pumping speeds* of about $4\text{--}16\text{ m}^3\text{ h}^{-1}$ are used to generate a medium vacuum of several Pascals. They are then connected to high-vacuum pumps in a way that their high-pressure side exhales into the medium vacuum of the rotary vane pumps, i.e., they are operated as *backing pumps*. This way, each pumping stage contributes a compression of some $10^4\text{--}10^5$ to the total factor of $10^9\text{--}10^{10}$ between atmospheric pressure and the

Table 4.3 Pressure ranges in vacuum technology

Pressure range [Pa]	Pressure range [mbar]	Pressure range [mtorr]	Vacuum	Gas flow
10^5 – 10^2	1 bar–1 mbar	750 torr–750 mtorr	Rough vacuum (RV)	Viscous flow
10^2 – 10^{-1}	1 – 10^{-3}	750–0.75	Medium vacuum (MV)	Knudsen flow
10^{-1} – 10^{-5}	10^{-3} – 10^{-7}	0.75 – 7.5×10^{-5}	High vacuum (HV)	Molecular flow
$<10^{-5}$	$<10^{-7}$	$<7.5 \times 10^{-5}$	Ultrahigh vacuum (UHV)	Molecular flow

high vacuum of 10^{-4} – 10^{-5} Pa (Table 4.3). The high-vacuum pumps can either be *turbomolecular pumps*, *oil diffusion pumps*, or *cryopumps* [310, 311].

Typical vacuum system The vacuum system of non-benchtop mass spectrometers consists of one to three rotary vane pumps and two or three turbo pumps. Rotary vane pumps are used for the inlet system(s) and as backing pumps for the turbo pumps. One turbo pump is mounted to the ion source housing, another one or two are operated at the analyzer. Thereby, a differentially pumped system is provided where local changes in pressure, e.g., from reagent gas in CI or collision gas in CID, do not notably influence the whole vacuum chamber.

4.12.2 High Vacuum Pumps

Turbomolecular pumps or *turbo pumps* having pumping speeds of 200–500 l s⁻¹ are currently the standard high vacuum pumps in mass spectrometry. A high-speed rotor (50,000–60,000 rpm) is employed to transport the molecules out of the *vacuum manifold* (*vacuum chamber*). Turbo pumps can be switched on and off in minutes, have low power consumption (about 100 W), and thus can be operated either air- or water cooled. Furthermore, they provide clean, in particular oil-free, high vacuum, are compact, and can be mounted either vertically below or horizontally at the sides of the vacuum manifold. Their disadvantages are the risk of sudden damage (similar to hard disk drives) and potential high frequency noise. Fortunately, modern turbo pumps run for many years and their noise is negligible.

Special turbo pump designs provide more than one port to allow for their simultaneous connection to different pressure regions, e.g., ca. 10^{-5} mbar and ca. 10^{-3} mbar. Such multistage turbo pumps are very useful as one unit is able to support differential pumping of atmospheric pressure ionization interfaces.

Furthermore, newer turbo pumps are equipped with magnetic bearings rather than with oil-lubricated bearings. This cuts down on maintenance, as the yearly exchange of lubricant becomes needless and also guarantees oil-free high vacuum.

Recent turbo pump designs also accept higher pressure at their exhaust thereby allowing for replacement of rotary vane pumps by membrane pumps. This results in

truly oil-free vacuum and offers more comfortable maintenance of the roughing pumps.

Oil diffusion pumps offer high pumping speeds (600–2000 l s^{-1}) at the cost of high power consumption (0.4–2 kW) and the need for a strong cooling water flow. The oil (perfluoropolypropylene glycols; Fomblin™, Santovac™) is thermally evaporated and the oil vapor supplies transport of gas molecules that enter it by diffusion. The gas-loaded oil vapor is condensed and the gas is removed from the liquid by the action of the backing pump. As diffusion pumps have no moving mechanical parts they are highly reliable and extremely silent. However, elongated use as well as sudden venting causes severe oil contaminations of the vacuum manifold. Diffusion pumps have almost been abandoned from modern mass spectrometers.

Cryopumps adsorb (freeze) residual gas to a surface cooled to the temperature of liquid nitrogen. They are highly efficient and provide clean vacuum, but cannot be operated without interruptions to recover the adsorber. Cryopumps are typically operated in combination with turbo pumps because they are only started after high-vacuum conditions are reached. Otherwise, the adsorber would soon be saturated.

4.13 Purchasing an Instrument

To some of us it can unexpectedly happen that we are faced with the task of having to buy a mass spectrometer, eventually for ourselves or on behalf of someone else. References to certain commercial instruments made in this chapter were in no way intended to preclude such a 100,000–1,000,000 € decision. The below guide may be useful in selecting an instrument that meets your requirements best.

Purpose

Define the tasks the mass spectrometer is going to be acquired for:

- Need for one dedicated or for several ionization methods?
- GC-MS, LC-MS, or ion mobility separation required?
- High resolution and accurate mass needed?
- Is tandem MS an issue or even a must?
- What sensitivity is needed?
- Is quantitative work important?
- Are you going to do mass spectral imaging?

Budget

Check your budget. A powerful and versatile second-hand machine from a proven company can be better than a toy-like single-purpose benchtop system.

Contact Sales

Get into contact with sales persons of all manufacturers offering suitable systems. Compare prices and modalities of customer training and support. Try to get information concerning longevity and product cycle (5, 10, 15 years?).

Demonstration

Make appointments for demonstration of those instruments that are likely to be acquired, e.g., for the top three of your ranking. Do not use completely unknown samples for this purpose. Otherwise, problems associated with your analyte might erroneously be regarded as a lack of instrumental performance.

Data System

Modern instruments form a unit with their data system. Does this offer the features you want? Does it allow for customization, “manual” settings, or corrections?

Analyzing Data

The software provided for analyzing the data is also of high relevance. Can you customize plots, lists, and reports, obtain molecular formulas, extract

Table 4.4 Rough estimates correlating instrumentation and factors affecting its cost

	Acquisition		Installation room requirements		Operation and long-term usage	
	Price of instrument	Footprint and weight	Power consumption, air conditioning load	Qualification of personnel	Maintenance	
Time-of-flight	S–L	S–L	S–M	S–L	S–L	S–L
Magnetic sector	L–XL	L–XL	L–XL	L–XL	L	L
Linear quadrupole	S–M	S–M	S–M	S–M	S–M	S–M
Quadrupole ion trap	S–M	S – M	S–M	S–M	S–M	S–M
Linear quadrupole ion trap	M–L	S–M	S–M	M–L	M	M
Fourier transform-ion cyclotron resonance	XL–XXL	XL–XXL	XL–XXL	L–XL	XL–XXL	XL–XXL
Orbitrap	L–XL	L	L	L–XL	L	L
Quadrupole-TOF hybrid	M–XL	M–L	L	M–L	L	L
Ion mobility-TOF hybrid	XL	L	L	L–XL	L–XL	L–XL

Classified in the format of American dress sizes as S, M, L, XL, XXL

chromatograms, get sophisticated output of data like Kendrick or van Krevelen plots?

Other Opinions

Use independent information from the published literature and ask current users of your top-choice mass spectrometers for the special strengths and shortcomings of those systems.

Investment and Cost of Ownership

Cost is not only affected by the price of acquisition of a mass spectrometer but also by operation in that it may have highly variable requirements of room, power, air conditioning, and operational skills (Table 4.4).

Avoid Buyer's Remorse

Keep in mind that any instrument acquisition inherently presents some compromise – none is perfect. Anyway, try to find the best for your needs and decide to be happy with your purchase afterwards.

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