

# Using Compression and Swelling Indices to Characterize Expansive Soils



Sergio Andrew Manigniavy, Yosra Bouassida, Dalel Azaiez,  
and Mounir Bouassida

**Abstract** Expansive soils are a worldwide problem. The volume variation of this soil is depended on its moisture content. A new approach to characterize this kind of soil is based on the oedometer test results, performed on compressible soils, either expansive or non-expansive. The  $C_c/C_s$  ratio is determined, where  $C_c$  is the compression index and  $C_s$  is the swelling index. Zones delimited by a  $C_c/C_s$  value and a swelling pressure ( $\sigma_s$ ) value are identified to differentiate expansive soils from non-expansive soils. When  $C_c/C_s$  ratio is higher or equal to 15, the swelling pressure is practically equal to zero.

**Keywords** Expansive soils · Characterization · Oedometer test · Compression index · Swelling index

## 1 Introduction

Expansive soils are globally widespread geological and natural hazard. This type of soil is currently found in arid or semi-arid areas. It can cause several damages to constructions. Clays, in particular the montmorillonite, are belong to the expansive soils. The shrink-swell behavior of this latter develops according to the variation of water content. Therefore, the expansive soils topic is of high interest for the six continents: Africa, Asia, Europe, Oceania, North and South America.

To understand the behavior of this category of soils, researchers are looking to suitable approaches to characterize it and to mitigate the swelling phenomenon.

The change in volume of expansive soils depends on the water content. The clay structure and the saturation of soils take a major place in this phenomenon. The liaison between montmorillonite clay particles is weak. During the swelling process, the water molecules and other cations carried by the water force the passage between

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S. A. Manigniavy (✉) · Y. Bouassida · D. Azaiez · M. Bouassida  
Ecole Nationale d'Ingénieurs de Tunis, Laboratoire d'Ingénierie Géotechnique et de Géorisque,  
Université de Tunis El Manar, LR14ES03, Tunis, Tunisia  
e-mail: [sergioandrew.manigniavy@etudiant-enit.utm.tn](mailto:sergioandrew.manigniavy@etudiant-enit.utm.tn)

clay particles by pushing them apart. This leads to an increase in swelling pressure [6].

Several buildings are constructed on swelling clays and represent damages that are due to the swelling phenomenon in the North of Africa, in particular in Tunisia and Algeria. Therefore, a research program to characterize expansive soils suitably and to formulate countermeasures and construction methods is needed to help civil engineers in the safe design and construction of foundations on the swelling soils [1].

## 2 About Expansive Soils

The shrink-swell behavior of clays is an extremely destructive phenomenon and leads to huge repair costs. Therefore, it is crucial to find methods to characterize expansive soils.

First, expansive soils are one of the most hazardous natural disaster [2]. Slope instability, tunnel collapse, differential heavy and buckling of building, fissures on structures and destruction of hydraulic structures can result from the presence of swelling soils [6].

Second, around the world, a lot of money is wasted due to extensive damage to buildings caused by the effect of swelling phenomenon every year. In many countries, financial assessment of the extra-costs, like repairing and maintenance, due to swelling soil problems has not yet been carried out. In Sudan, the cost of damage to buildings and light structures due to swelling soils is estimated more than 6 million dollars [14]. Many countries are affected by the damage of this problematic soil: in United States, losses due to expansive soils are about 13 billion dollars in damage to buildings, roads, airports and other infrastructures each year [15]. In United Kingdom and Saudi Arabia, this cost varies in the range of 300 to 450 million dollars [5, 16].

Third, to deal with this type of soil, there are some improvements proposed, like the use of granular materials, chemical and soil mixture treatments. The granular piles technique is a practical and promising technique. Their installation is possible at any season. The reduction in swelling provided by the use of a granular piles varied from 10 to 45% [10]. The use of a granular material as a separation layer between the foundation and an expansive soil revealed a potential solution to reduce the swelling effect [1]. In addition, noted also that chemical treatments revealed of interest as well. According to Mahamedi and Khemissa [12], mixture of swelling clay with respectively cement and lime in an amount of 10% reduces the swelling potential and decreases liquid limit by 41 and 43% respectively. Soil sensitivity to water has been reduced by the lime treatment. This is due to decrease of moisture content after lime hydration [11]. As cement contains about 60% lime, mixing with cement gives approximately the same result as mixing with lime. Moreover, according to Gueddouda et al. [7], about the soil mixture, the addition of dune sand leads to an important reduction of the swelling parameters. With 45% sand, for the swelling potential, this reduction is about 65% and for the swelling pressure exceeds 85%.

This addition is involved in the increase of the pore size in the swelling soil mass that is owed to the reduction of these expansion effects. The evolution of suction is proportional to that of shear strength. Further, Tiwari et al. [18] recommended the use of coir geotextile which reduces the swelling pressure by about 27% and also reduces the speed of swelling. It is noted that, approximately, the same results are found with a silica fume treated coir geotextile. A reduction of 55% for the swelling pressure and 79% for the percentage of expansion are observed when using a coir geotextile treated with lime. Finally, according to Kalantari [9], the three most commonly used techniques are the soil substitution, use of enough strong structures and the separation between the structure and the swelling clay.

### 3 Characterization Methods

Due to damages caused by expansive soils, several researchers made an effort to develop approaches to characterize this type of soil in order to know it better and to prevent the problems it can cause. Sridharan and Prakash [17] proposed two kinds of characterization methods:

- by identifying the soil mineralogy using X-ray diffraction analysis, differential thermal analysis, dye adsorption, chemical analysis and scanning electron microscopy;
- by inferential testing using indirect or direct methods.

There are some indirect methods: clay fraction method, Atterberg limits tests and activity  $A_c$  method. Some classifications are referred to direct methods like the oedometer swell test, free swell tests and suction method.

### 4 Approach to Characterize Expansive Soils from Oedometer Test Results

Compression index ( $C_c$ ) and swelling index ( $C_s$ ) are currently determined from oedometer tests, which performed with submerged specimens to ensure a full saturation during the experiments. By an oedometer test, both indices  $C_c$  and  $C_s$ , can be measured for any compressible soil, either expansive or non-expansive.

The data used for this study are oedometer test results provided by specialized geotechnical engineering offices or published by researchers in technical papers. The method to characterize expansive soils using the  $C_c/C_s$  ratio relied on data collected from four case studies, comprising twenty-nine specimens from Tunisia, Algeria, Canada and United States. These data are presented in Table 1. The  $C_c/C_s$  ratio is an indicator of the change in volume quantifying the degree of soil compression versus swelling [1]. This volume variation is linked the swelling pressure ( $\sigma_s$ ).

**Table 1** Oedometer test results (update of Bouassida et al. [1])

Country	Site	Sample	Cc	Cs	Cc/Cs	$\sigma_s$ (kPa)	Expansive	Non-expansive
Tunisia	Béja	BH1	0.160	0.024	6.667	110	x	
		BH2	0.140	0.026	5.385	230	x	
		BH3	0.150	0.018	8.333	90	x	
		BH4	0.180	0.037	4.865	120	x	
		BH5	0.160	0.035	4.571	140	x	
		BH6	0.140	0.010	14.000	40		x
		BH7	0.150	0.012	12.500	40		x
		BH8	0.130	0.019	6.842	140	x	
		BH9	0.220	0.030	7.333	130	x	
		BH10	0.180	0.039	4.615	80	x	
		G109-BH1-2	0.226	0.086	2.628	204	x	
		G109-BH1-3	0.176	0.035	5.029	108	x	
		Centre Urbain du Nord—Tunis	0.158	0.012	13.167	0		x
		BH1-US1-1	0.123	0.009	13.667	0		x
		BH1-US1-2	0.129	0.008	16.125	0		x
		BH2-US2-1	0.129	0.008	16.125	0		x
		BH1-US11	0.097	0.022	4.409	90	x	
		BH1-US12	0.040	0.004	10.000	95	x	
		BH1-US13	0.124	0.021	5.905	220	x	
		BH1-US14	0.114	0.027	4.222	185	x	
		BH2-US21	0.173	0.009	19.222	0		x
		BH3-US31	0.055	0.003	18.333	0		x

(continued)

Table 1 (continued)

Country	Site	Sample	Cc	Cs	Cc/Cs	$\sigma_s$ (kPa)	Expansive	Non-expansive
		BH3-US33	0.156	0.040	3.900	275	x	
	Jardin El Menzah 1—Tunis	BH1-US1	0.140	0.017	8.235	160	x	
		BH1-US2	0.140	0.025	5.600	190	x	
		BH2-US2	0.140	0.017	8.235	150	x	
		BH3-US2	0.140	0.011	12.727	20		x
		BH4-US1	0.190	0.041	4.634	70	x	
		BH4-US3	0.200	0.061	3.279	180	x	
Algeria	Médéa <sup>a</sup>	S-1-1	0.140	0.045	3.111	400	x	
		S-4-1	0.400	0.100	4.000	70	x	
		S-4-3	0.350	0.140	2.500	80	x	
		S-10-1	0.150	0.100	1.500	420	x	
		S-10-2	0.080	0.070	1.143	800	x	
USA	Louisiana	–	0.360	0.110	3.273	170	x	
Canada	Lake Agassiz	B	0.73	0.23	3.174	54	x	
	Northern Alberta	C	0.12	0.07	1.714	429	x	
	Regina <sup>a</sup>	D	0.17	0.05	3.400	965	x	
		E-1	0.1	0.04	2.500	547	x	
		E-2	0.08	0.04	2.000	526	x	

<sup>a</sup> Updated; BH: borehole; US: undisturbed sample; S: sample

The variation of swelling pressure with respect to the  $C_c/C_s$  ratio from the data, given by Table 1, is shown in Fig. 1. From this figure, non-expansive soils are in the side where  $C_c/C_s$  ratio is above 10 and the swelling pressure is under 50 kPa. The swelling pressure of expansive soils belong to the side where  $C_c/C_s$  ratio is under 10, is higher than 50 kPa. This approach is approved by Chen [3] and Coduto [4] who affirmed that when the swelling pressure is under 50 kPa, the swell potential is low, hence insignificant. Furthermore, when  $C_c/C_s$  ratio is higher than 15, the swelling pressure is practically equal to zero. A classification between expansive and non-expansive soils is shown in Table 2. If the compression index ( $C_c$ ) is about 10 times larger than the swelling index ( $C_s$ ), then the swelling potential of this soil is low. For Tunisian non-expansive soils, the swelling index is around or lower than 0.010. So, this value represents the low degree of soil to swell in North Tunisia. Note that all non-expansive Tunisian soils in Table 1 or in Fig. 1 are sandy or silty clays which may approve that the mixture of sand or silt with a swelling clay can reduce the soil swelling potential.

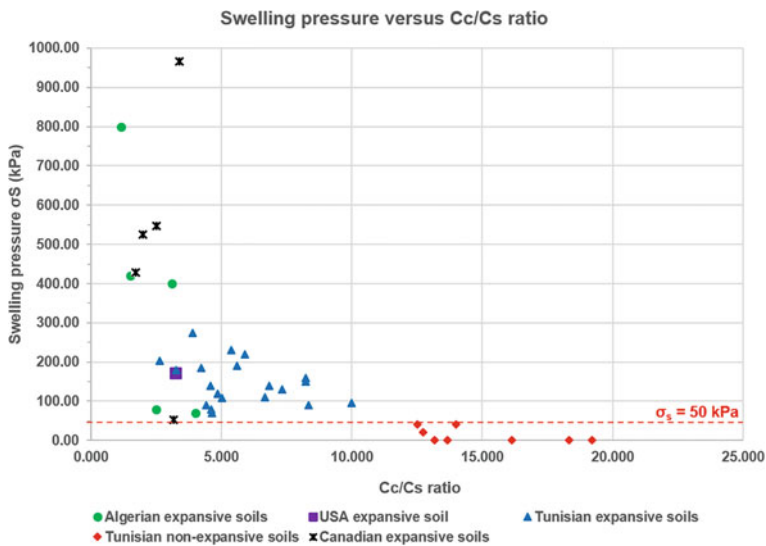


Fig. 1 Swelling pressure versus  $C_c/C_s$  ratio (updated from Bouassida et al. [1])

Table 2 Classification of expansive soils using oedometer test results [1]

Type of soil	$C_c/C_s$	$\sigma_s$ (kPa)
Expansive	<10	>50
Non-expansive	>10	<50

## 5 Conclusion

The objective of this work is to characterize expansive soils using oedometer test results. This method is related to compression and swelling indices and carried out with thirty-nine (39) data from two continents, North America and Africa. The soil is considered to be non-expansive when the swelling pressure is under 50 kPa. If the  $C_c/C_s$  ratio is less than 10, Civil engineer should not underestimate the swelling pressure of the soil and should take it into their calculations. And, they should not forget the shrink—swell behavior of the soil.

The perspective of this work is to collect a lot of oedometer test results to have more precision in this characterization method and also to estimate the swelling pressure of a soil from these data.

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**Dr. Mounir Bouassida** is a professor of civil engineering at the National Engineering School of Tunis (ENIT) of the University of Tunis El Manar where he earned his B.S., M.S., Ph.D., and doctorate of sciences diplomas, all in civil engineering. He co-supervised 23 Ph.D. and 32 Masters of Science graduates. His research focused on soil improvement techniques and the behavior of soft clays. Dr. Bouassida is the (co)author of more than 100 papers in refereed international journals; 180 conference papers including 27 keynote lectures and several book chapters. Further he co-authored three books and three patents as well as book series conferences.

He is Associate Editor of Innovative Infrastructure Innovative Solutions and Ground Improvement (ICE) journals, Geotechnical-Geological journal, International Journal of Geosynthetics and Ground Engineering and the GE section of the Frontiers and Built Environment journal.

As a 2006 Fulbright scholar, Dr Bouassida elaborated a novel methodology for the design of foundations on reinforced soil by columns. He is a co-developer of the software Columns 1.01 used for the design of column-reinforced foundations. He was awarded the 2006 S. Prakash Prize for Excellence in the practice of geotechnical engineering.

In 2008, Dr Bouassida launched a Tunisian consulting office in geotechnical engineering, SIMPRO. As such, he contributed for the design of more than hundred projects.

Prof. Bouassida held the office of the vice president of ISSMGE for Africa (2005–2009) and then and appointed member of the ISSMGE board (2017–2022). He benefited from grants as a visiting-invited professor in several institutions in the USA, Canada, Europe, Australia and Asia. In 2018, he became a Director of the International Press-In Association.

Since 2019, the launch of the You Tube channel « Mounir Bouassida » gained lot of interest from than 1430 subscribers. Fifty nine uploaded videos, in English and French, to this channel cover themes focusing on soil mechanics, modelling and the study of the behavior of geotechnical engineering structures.