

# Data-Driven Identification of Rayleigh-Damped Second-Order Systems



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**Abstract** In this paper, we present a data-driven approach to identify second-order systems, having internal Rayleigh damping. This means that the damping matrix is given as a linear combination of the mass and stiffness matrices. These systems typically appear when performing various engineering studies, e.g., vibrational and structural analysis. In an experimental set-up, the frequency response of a system can be measured via various approaches, for instance, by measuring the vibrations using an accelerometer. As a consequence, given frequency samples, the identification of the underlying system relies on rational approximation. To that aim, we propose an identification of the corresponding second-order system, extending the Loewner framework for this class of systems. The efficiency of the proposed method is demonstrated by means of various numerical benchmarks.

**Keywords** Data-driven modeling · Second-order systems · Model reduction · Loewner framework · Mechanical systems

## 1 Introduction

In this paper, we discuss a data-driven identification framework for a class of second-order (SO) systems of the form:

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$$\Sigma_{\text{SO}} := \begin{cases} \mathbf{M}\ddot{\mathbf{x}}(t) + \mathbf{D}\dot{\mathbf{x}}(t) + \mathbf{K}\mathbf{x}(t) = \mathbf{B}\mathbf{u}(t), \\ \mathbf{y}(t) = \mathbf{C}\mathbf{x}(t), \end{cases} \quad (1)$$

where  $\mathbf{x}(t) \in \mathbb{R}^n$  is the state vector,  $\mathbf{u}(t) \in \mathbb{R}^m$  are the inputs,  $\mathbf{y}(t) \in \mathbb{R}^p$  are the outputs or measurements, and  $\mathbf{M}, \mathbf{D}, \mathbf{K} \in \mathbb{R}^{n \times n}$  are, respectively, the mass matrix, the damping matrix and the stiffness matrix,  $\mathbf{B} \in \mathbb{R}^{n \times m}$  and  $\mathbf{C} \in \mathbb{R}^{p \times n}$ . For simplicity, we address the problem for single-input single-output (SISO) systems, i.e.,  $m = p = 1$ . The multiple-input multiple-output (MIMO) generalization is straightforward and can be done by following the lines of the MIMO extension of the classical Loewner framework [20] based on tangential interpolation. Such systems arise in many engineering applications, including vibration analysis [21], structural dynamics [10] and electric circuits. We denote the SO systems (1) by  $\Sigma_{\text{SO}} = (\mathbf{M}, \mathbf{D}, \mathbf{K}, \mathbf{B}, \mathbf{C})$ . Moreover, we assume a zero inhomogeneous condition, i.e.,  $\mathbf{x}(0) = \dot{\mathbf{x}}(0) = 0$ . Hence, by means of the Laplace transform, the input-output behavior of the system  $\Sigma_{\text{SO}}$  is associated with the transfer function as follows:

$$\mathbf{H}_{\text{SO}}(s) = \mathbf{C} (s^2\mathbf{M} + s\mathbf{D} + \mathbf{K})^{-1} \mathbf{B}. \quad (2)$$

Furthermore, throughout the paper, we assume the proportional Rayleigh damping hypothesis, i.e., the damping matrix  $\mathbf{D}$  is given by a linear combination of the mass and stiffness matrices:

$$\mathbf{D} = \alpha\mathbf{M} + \beta\mathbf{K}, \quad (3)$$

for  $\alpha, \beta \geq 0$ . This hypothesis is often considered in engineering application, where the damper is numerically constructed in order to avoid non-dampened oscillations, see [21, Chapter 7] for more details. Recent applications of the Rayleigh damping hypothesis can be found in the fields of guided wave propagation in composite materials [16, 28], earthquake analysis of buildings [11, 12], wind turbine monopiles [6], railway catenary wire systems [24]. Moreover, the Model-Order-Reduction-Wiki (MOR Wiki) presents several large-scale benchmarks of Rayleigh damped second order systems, such as the butterfly gyroscope [25] and the recently developed artificial fishtail [33].

In the past twenty years, model order reduction of SO systems has been investigated extensively; see for instance [8, 22, 29] for balancing-type methods, and [3, 4, 7, 36] for moment matching and  $\mathcal{H}_2$ -optimality based methods. Recently, the authors in [30] provided an extensive comparison among common methods for SO model order reduction applied to a large-scale mechanical artificial fishtail model. In all of the above-mentioned works, the authors suppose that they have access to the matrices, defining the original systems and the reduced-order systems are constructed via Petrov-Galerkin projections. Thus, the main goal is to find projection matrices  $\mathbf{V}, \mathbf{W} \in \mathbb{R}^{n \times r}$ , leading to the SO reduced-order system

$$\hat{\mathbf{H}}_{\text{SO}}(s) = \hat{\mathbf{C}} \left( s^2\hat{\mathbf{M}} + s\hat{\mathbf{D}} + \hat{\mathbf{K}} \right)^{-1} \hat{\mathbf{B}}, \quad (4)$$

with  $\hat{\mathbf{M}} = \mathbf{W}^T \mathbf{M} \mathbf{V}$ ,  $\hat{\mathbf{D}} = \mathbf{W}^T \mathbf{D} \mathbf{V}$ ,  $\hat{\mathbf{K}} = \mathbf{W}^T \mathbf{K} \mathbf{V}$ ,  $\hat{\mathbf{B}} = \mathbf{W}^T \mathbf{B}$  and  $\hat{\mathbf{C}} = \mathbf{C} \mathbf{V}$ .

However, it is not necessary that the realization is given or is feasible to obtain; thus, we suppose that the original system realization may not be available. Instead, we assume to have access only to frequency domain data, e.g., arising from experiments or numerical simulations. More precisely, we are interested in solving the following problem.

**Problem 1** (*SO data-driven identification*) Given interpolation data

$$\{(\sigma_i, \omega_i) \mid \sigma_i \in \mathbb{C} \text{ and } \omega_i \in \mathbb{C}, i = 1, \dots, \rho\}, \quad (5)$$

construct a SO realization  $\Sigma_{\text{SO}} = (\mathbf{M}, \mathbf{D}, \mathbf{K}, \mathbf{B}, \mathbf{C})$  of appropriate dimensions, satisfying the proportional Rayleigh damping hypothesis, i.e.,

$$\mathbf{D} = \alpha \mathbf{M} + \beta \mathbf{K},$$

whose transfer function  $\mathbf{H}_{\text{SO}}(s) := \mathbf{C}(s^2 \mathbf{M} + s \mathbf{D} + \mathbf{K})^{-1} \mathbf{B}$  satisfies the interpolation conditions, i.e.,

$$\mathbf{H}_{\text{SO}}(\sigma_i) = \omega_i, \quad i = 1, \dots, \rho. \quad (6)$$

Problem 1 corresponds to an identification problem which aims at determining a SO realization that not only interpolates at given measurements, but also satisfies the Rayleigh damping hypothesis. A similar problem for time-delay systems was studied in [27] and [31]. Furthermore, we would like to mention that a data-driven approach for structured non-parametric systems has been studied in [32]. However, the construction of the structured reduced-order system is not a straightforward task.

The purpose of this paper is thus to extend the application domain of the Loewner framework established in [19, 20] to SO systems. With this aim, a new SO Loewner framework is developed, yielding a Rayleigh damped SO system of the form (2) that interpolates at given frequency measurements.

The rest of the paper is organized as follows. Section 2 recalls some preliminary results on the rational interpolation Loewner framework from [20]. Section 3 contains the main contribution of this paper, i.e., the extension of these results to the class of Rayleigh damped SO systems. Firstly, one assumes the knowledge of the Rayleigh damping parameters,  $\alpha$  and  $\beta$ , and derives the Loewner matrices for SO systems. Then, a heuristic procedure is presented, originally proposed in [31] in the context of time-delay systems, enabling us to estimate the parameters  $\alpha$  and  $\beta$ . Also, we discuss the case of more general damping strategies. Finally, Sect. 4 illustrates the proposed framework by numerical examples and Sect. 5 concludes the paper.

## 2 Classical Loewner Framework

In this section, we briefly recall the Loewner framework [20]. A first-order (FO) system  $\Sigma_{\text{FO}} = (\mathbf{E}, \mathbf{A}, \mathbf{B}, \mathbf{C})$  is a dynamical system of the form:

$$\Sigma_{\text{FO}} := \begin{cases} \mathbf{E}\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t), & \mathbf{x}(0) = 0, \\ \mathbf{y}(t) = \mathbf{C}\mathbf{x}(t), \end{cases} \quad (7)$$

with  $\mathbf{E}, \mathbf{A} \in \mathbb{R}^{n \times n}$ ,  $\mathbf{B} \in \mathbb{R}^{n \times m}$  and  $\mathbf{C} \in \mathbb{R}^{p \times n}$ , and the leading dimension  $n$  is the order of the system. For clarity of exposition, we focus for now on the single-input single-output (SISO) case, i.e., when  $m = p = 1$ . The system (7) is associated with the transfer function given by

$$\mathbf{H}_{\text{FO}}(s) = \mathbf{C}(s\mathbf{E} - \mathbf{A})^{-1}\mathbf{B}. \quad (8)$$

There exist several MOR techniques for first-order systems such as explicit moment matching [35, 37], implicit moment matching using Krylov subspaces [13, 17], Sylvester equations based method [15], extensions for MIMO systems [14]. We refer the reader to the books [2, 5] for more details. However, our goal lies in the identification of linear systems using only the frequency data. Hence, the identification problem, in its SISO form, is stated as follows.

**Problem 2** (*First-order data-driven model reduction*) Given interpolation data

$$\{(\sigma_i, \boldsymbol{\omega}_i) \mid \sigma_i \in \mathbb{C} \text{ and } \boldsymbol{\omega}_i \in \mathbb{C}, i = 1, \dots, \rho\} \quad (9)$$

construct a minimal-order realization  $\Sigma = (\mathbf{E}, \mathbf{A}, \mathbf{B}, \mathbf{C})$  of appropriate dimensions, whose transfer function  $\mathbf{H}_{\text{FO}}(s) = \mathbf{C}(s\mathbf{E} - \mathbf{A})^{-1}\mathbf{B}$  satisfies the interpolation conditions

$$\mathbf{H}_{\text{FO}}(\sigma_i) = \boldsymbol{\omega}_i, i = 1, \dots, \rho. \quad (10)$$

A wide range of methods has been developed to solve Problem 2, e.g., vector fitting [18], the AAA algorithm [23] and the Loewner framework [20]. In this paper, we focus on the latter approach and, in what follows, we recall some of the results contained therein. Firstly, we assume that the number of interpolation data is even, i.e.,  $\rho = 2\ell$ , and as a result, the data can be partitioned in two disjoint sets as follows:

$$\text{right interpolation set } \mathcal{P}_r : \{(\lambda_i, \mathbf{w}_i) \mid \lambda_i \in \mathbb{C} \text{ and } \mathbf{w}_i, i = 1, \dots, \ell\}, \text{ and} \quad (11a)$$

$$\text{left interpolation set } \mathcal{P}_l : \{(\mu_j, \mathbf{v}_j) \mid \mu_j \in \mathbb{C} \text{ and } \mathbf{v}_j \in \mathbb{C}, j = 1, \dots, \ell\}. \quad (11b)$$

Using this partition, we associate the following Loewner matrices.

**Definition 1** (Loewner matrices [20]) Given the right  $\mathcal{P}_r$  and left  $\mathcal{P}_l$  interpolation sets, we associate them with the Loewner matrix  $\mathbb{L}$  and shifted Loewner matrix  $\mathbb{L}_\sigma$  given by

$$\mathbb{L} = \begin{pmatrix} \frac{\mathbf{v}_1 - \mathbf{w}_1}{\mu_1 - \lambda_1} & \dots & \frac{\mathbf{v}_\ell - \mathbf{w}_\ell}{\mu_1 - \lambda_\ell} \\ \vdots & \ddots & \vdots \\ \frac{\mathbf{v}_\ell - \mathbf{w}_1}{\mu_\ell - \lambda_1} & \dots & \frac{\mathbf{v}_\ell - \mathbf{w}_\ell}{\mu_\ell - \lambda_\ell} \end{pmatrix}, \quad \mathbb{L}_\sigma = \begin{pmatrix} \frac{\mu_1 \mathbf{v}_1 - \lambda_1 \mathbf{w}_1}{\mu_1 - \lambda_1} & \dots & \frac{\mu_1 \mathbf{v}_1 - \lambda_\ell \mathbf{w}_\ell}{\mu_1 - \lambda_\ell} \\ \vdots & \ddots & \vdots \\ \frac{\mu_\ell \mathbf{v}_\ell - \lambda_1 \mathbf{w}_1}{\mu_\ell - \lambda_1} & \dots & \frac{\mu_\ell \mathbf{v}_\ell - \lambda_\ell \mathbf{w}_\ell}{\mu_\ell - \lambda_\ell} \end{pmatrix}. \quad (12)$$

**Remark 1** The Loewner matrix  $\mathbb{L}$  was introduced in [1]. As shown therein, its usefulness derives from the fact that its rank is equal to the order of the minimal realization  $\mathbf{H}_{FO}$  satisfying the interpolation conditions in (10). Hence, it reveals the complexity of the reduced-order model solving Problem 2.

Next, let us introduce the following matrices associated with the interpolation problem as follows:

$$\begin{cases} \mathbf{\Lambda} = \text{diag}(\lambda_1, \dots, \lambda_\ell) \in \mathbb{C}^{\ell \times \ell} \\ \hat{\mathbf{H}}(\mathbf{\Lambda}) = [\mathbf{w}_1 \dots \mathbf{w}_\ell]^T \in \mathbb{C}^{\ell \times 1} \end{cases} \quad \text{and} \quad \begin{cases} \mathbf{M} = \text{diag}(\mu_1, \dots, \mu_\ell) \in \mathbb{C}^{\ell \times \ell} \\ \hat{\mathbf{H}}(\mathbf{M}) = [\mathbf{v}_1 \dots \mathbf{v}_\ell]^T \in \mathbb{C}^{\ell \times 1} \end{cases} \quad (13)$$

Also, let  $\mathbf{1} \in \mathbb{R}^{\ell \times 1}$  be the column vector with all entries equal to one. Hence, the Loewner matrices satisfy the following Sylvester equations

$$\mathbf{M}\mathbb{L} - \mathbb{L}\mathbf{\Lambda} = \hat{\mathbf{H}}(\mathbf{M})\mathbf{1}^T - \mathbf{1}\hat{\mathbf{H}}(\mathbf{\Lambda})^T, \quad \text{and} \quad (14a)$$

$$\mathbf{M}\mathbb{L}_\sigma - \mathbb{L}_\sigma\mathbf{\Lambda} = \mathbf{M}\hat{\mathbf{H}}(\mathbf{M})\mathbf{1}^T - \mathbf{1}\hat{\mathbf{H}}(\mathbf{\Lambda})\mathbf{\Lambda}. \quad (14b)$$

An elegant solution for Problem 2 based on the Loewner pair  $(\mathbb{L}, \mathbb{L}_\sigma)$  was proposed in [20]. This is summarized in the following theorem.

**Theorem 1** (Loewner framework [20]) Let  $\mathbb{L}$  and  $\mathbb{L}_\sigma$  be the Loewner matrices associated with the partition in (13). If  $(\mathbb{L}_\sigma, \mathbb{L})$  is a regular pencil with no  $\mu_i$  or  $\lambda_j$  being an eigenvalue, then the matrices

$$\hat{\mathbf{E}} = -\mathbb{L}, \quad \hat{\mathbf{A}} = -\mathbb{L}_\sigma, \quad \hat{\mathbf{B}} = \hat{\mathbf{H}}(\mathbf{M}), \quad \hat{\mathbf{C}} = \hat{\mathbf{H}}(\mathbf{\Lambda})^T,$$

provides a realization  $\hat{\Sigma}_{FO} = (\hat{\mathbf{E}}, \hat{\mathbf{A}}, \hat{\mathbf{B}}, \hat{\mathbf{C}})$  for a minimal order interpolant of Problem 2, i.e., the transfer function

$$\hat{\mathbf{H}}_{FO}(s) = \mathbf{W}(s\mathbb{L}_\sigma - \mathbb{L})^{-1}\mathbf{V}$$

satisfies the interpolation conditions in (10).

Theorem 1 allows to obtain a FO system  $\hat{\mathbf{H}} = (\hat{\mathbf{E}}, \hat{\mathbf{A}}, \hat{\mathbf{B}}, \hat{\mathbf{C}})$  whose transfer function interpolates right and left data as stated in Problem 2. However, when more data than necessary are provided, then the hypothesis of Theorem 1 may not be satisfied. Hence, a singular-value decomposition (SVD) based procedure has been proposed in [20] to find an FO system interpolating the frequency data.

Next, recall that a SO system  $\Sigma_{\text{SO}} = (\mathbf{M}, \mathbf{D}, \mathbf{K}, \mathbf{B}, \mathbf{C})$  can be written as a first-order realization, for instance, as follows:

$$\mathbf{H}_{\text{SO\_FO}}(s) = \mathbf{C}(s\mathbf{E} - \mathcal{A})^{-1}\mathcal{B},$$

where

$$\mathcal{E} = \begin{bmatrix} \mathbf{I} & \mathbf{0} \\ \mathbf{0} & \mathbf{M} \end{bmatrix}, \quad \mathcal{A} = \begin{bmatrix} \mathbf{0} & \mathbf{I} \\ -\mathbf{K} & -\mathbf{D} \end{bmatrix}, \quad \mathcal{B} = \begin{bmatrix} \mathbf{0} \\ \mathbf{B} \end{bmatrix} \quad \text{and} \quad \mathbf{C} = [\mathbf{C} \ \mathbf{0}].$$

As a consequence, the classical Loewner framework presented in Sect. 2 can be employed to find a first-order realization. However, the intrinsic SO structure will not be preserved in the identified model. But the classical Loewner framework yields an information about the order of a SO realization fitting the data, which is outlined in the following remark.

**Remark 2** (*Order of SO model*) Let us suppose that the frequency data in Problem 2 and let  $\mathbb{L}$  be a Loewner matrix given in (12) constructed with this data. Then, the order of the SO system fitting the data equals  $\frac{1}{2}\text{rank}(\mathbb{L})$ .

In the following section, we discuss an extension of the Loewner framework for the class of Rayleigh damped SO systems.

### 3 Second-Order Loewner Framework

This section contains our main contribution, which presents an extension of the Loewner framework to the class of SO Rayleigh damped systems (1). Here, we also assume that the number of interpolation data is even, i.e.,  $\rho = 2\ell$ , and the data is partitioned into two disjoint sets as in (11a) and (11b). Moreover, the data is organized into the matrices  $\mathbf{\Lambda}$ ,  $\hat{\mathbf{H}}(\mathbf{\Lambda})$ ,  $\mathcal{M}$ ,  $\hat{\mathbf{H}}(\mathcal{M})$  as in (13). This section is divided into four parts. The first one aims at finding the matrix equations which encode the general SO systems satisfying the interpolation conditions. In the second one, we assume to have a priori knowledge of the Rayleigh damping parameters  $\alpha$  and  $\beta$  and we derive the equivalents of the Loewner matrices (12) and Theorem 1 to the class of SO Rayleigh damped systems. The third part is dedicated to proposing a heuristic procedure to estimate the parameters  $\alpha$  and  $\beta$  using the frequency data available. Finally, in the fourth part, we briefly discuss the case of more general dampings.

### 3.1 Second-Order Loewner Matrices

In what follows, we assume that Problem 1 has a minimal order  $r$  solution  $\mathbf{H}_{SO}^*$ , given by

$$\mathbf{H}_{SO}^*(s) = \mathbf{C}^* (s^2 \mathbf{M}^* + s \mathbf{D}^* + \mathbf{K}^*)^{-1} \mathbf{B}^*, \quad (15)$$

with  $\mathbf{D}^* = \alpha \mathbf{M}^* + \beta \mathbf{K}^*$ . Here, we also assume that the coefficients  $\alpha$  and  $\beta$  from the Rayleigh damping hypothesis are known. Then, later in this section, we will show how to construct a realization equivalent to  $\mathbf{H}_{SO}^*(s)$  that only depends on the frequency data. To that aim, let us first recall a result from [4] enabling projection-based structured preserving model reduction.

**Theorem 2** (Structure preserving SO model reduction [4]) *Consider the SO transfer function  $\mathbf{H}_{SO}(s)$  as given in (2). For given interpolation points  $\lambda_i$  and  $\mu_i$ ,  $i \in \{1, \dots, \ell\}$ , let the projection matrices  $\mathbf{V}$  and  $\mathbf{W}$  be as follows:*

$$\mathbf{V} = \left[ (\lambda_1^2 \mathbf{M} + \lambda_1 \mathbf{D} + \mathbf{K})^{-1} \mathbf{B}, \dots, (\lambda_\ell^2 \mathbf{M} + \lambda_\ell \mathbf{D} + \mathbf{K})^{-1} \mathbf{B} \right] \quad (16a)$$

$$\mathbf{W} = \left[ (\mu_1^2 \mathbf{M} + \mu_1 \mathbf{D} + \mathbf{K})^{-T} \mathbf{C}^T, \dots, (\mu_\ell^2 \mathbf{M} + \mu_\ell \mathbf{D} + \mathbf{K})^{-T} \mathbf{C}^T \right] \quad (16b)$$

Then, the reduced-order model  $\hat{\mathbf{H}}_{SO}(s)$  constructed by Petrov-Galerkin projection as in (4) satisfies the interpolation conditions

$$\mathbf{H}_{SO}(\lambda_i) = \hat{\mathbf{H}}_{SO}(\lambda_i) \quad \text{and} \quad \mathbf{H}_{SO}(\mu_i) = \hat{\mathbf{H}}_{SO}(\mu_i), \quad \text{for } i = 1, \dots, \ell.$$

The above theorem allows us to construct a SO reduced-order model by interpolation. Let us apply this theorem to the SO system  $\mathbf{H}_{SO}^*(s)$  (15). For this, we will construct the matrix  $\mathbf{V}$  using the interpolation points in  $\mathbf{\Lambda}$ , and the matrix  $\mathbf{W}$  using the interpolation points in  $\mathbf{M}$ . As a consequence,  $\mathbf{V}$  and  $\mathbf{W}$  are, respectively, the solutions of the following matrix equations

$$\mathbf{M}^* \mathbf{V} \mathbf{\Lambda}^2 + \mathbf{D}^* \mathbf{V} \mathbf{\Lambda} + \mathbf{K}^* \mathbf{V} = \mathbf{B}^* \mathbb{1}^T, \quad \text{and} \quad (17a)$$

$$\mathbf{M}^2 \mathbf{W}^T \mathbf{M}^* + \mathbf{M} \mathbf{W}^T \mathbf{D}^* + \mathbf{W}^T \mathbf{K}^* = \mathbb{1} \mathbf{C}^*, \quad (17b)$$

Multiplying Eq. (17a) on the left by  $\mathbf{W}^T$  and Eq. (17b) on the right by  $\mathbf{V}$ , respectively, one obtains

$$\begin{aligned} \mathbf{W}^T \mathbf{M}^* \mathbf{V} \mathbf{\Lambda}^2 + \mathbf{W}^T \mathbf{D}^* \mathbf{V} \mathbf{\Lambda} + \mathbf{W}^T \mathbf{K}^* \mathbf{V} &= \mathbf{W}^T \mathbf{B}^* \mathbb{1}^T, \\ \mathbf{M}^2 \mathbf{W}^T \mathbf{M}^* \mathbf{V} + \mathbf{M} \mathbf{W}^T \mathbf{D}^* \mathbf{V} + \mathbf{W}^T \mathbf{K}^* \mathbf{V} &= \mathbb{1} \mathbf{C}^* \mathbf{V}. \end{aligned}$$

If we set

$$\hat{\mathbf{M}} = \mathbf{W}^T \mathbf{M}^* \mathbf{V}, \quad \hat{\mathbf{D}} = \mathbf{W}^T \mathbf{D}^* \mathbf{V}, \quad \hat{\mathbf{K}} = \mathbf{W}^T \mathbf{K}^* \mathbf{V}, \quad (18a)$$

$$\hat{\mathbf{B}} = \mathbf{W}^T \mathbf{B}^* = \hat{\mathbf{H}}(\mathcal{M}), \quad \text{and} \quad \hat{\mathbf{C}} = \mathbf{C}^* \mathbf{V} = \hat{\mathbf{H}}(\Lambda)^T, \quad (18b)$$

then the SO system  $\hat{\mathbf{H}}_{\text{SO}} = (\hat{\mathbf{M}}, \hat{\mathbf{D}}, \hat{\mathbf{K}}, \hat{\mathbf{B}}, \hat{\mathbf{C}})$  is the reduced-order model obtained by Theorem 2, satisfying the interpolation conditions from Problem 1. Hence, we can rewrite the above equations as follows:

$$\hat{\mathbf{M}}\Lambda^2 + \hat{\mathbf{D}}\Lambda + \hat{\mathbf{K}} = \hat{\mathbf{H}}(\mathcal{M})\mathbb{1}^T, \quad (19a)$$

$$\mathcal{M}^2\hat{\mathbf{M}} + \mathcal{M}\hat{\mathbf{D}} + \hat{\mathbf{K}} = \mathbb{1}\hat{\mathbf{H}}(\Lambda)^T. \quad (19b)$$

Equations in (19) give a relationship between the matrices  $\hat{\mathbf{M}}, \hat{\mathbf{D}}$  and  $\hat{\mathbf{K}}$ , which are the unknowns we are willing to identify, and the interpolation data encoded by  $\Lambda, \hat{\mathbf{H}}(\Lambda), \hat{\mathbf{M}}$  and  $\hat{\mathbf{H}}(\mathcal{M})$ . However, as discussed in [32], it corresponds to an underdetermined system on the unknowns.

### 3.2 Identification of Rayleigh-Damped Second-Order Systems

From now on, we will assume the Rayleigh damping hypothesis, i.e.,  $\hat{\mathbf{D}} = \alpha\hat{\mathbf{M}} + \beta\hat{\mathbf{K}}$ . As a consequence, the system of equations in (19) becomes

$$\hat{\mathbf{M}}(\Lambda^2 + \alpha\Lambda) + \hat{\mathbf{K}}(\beta\Lambda + \mathbf{I}) = \hat{\mathbf{H}}(\mathcal{M})\mathbb{1}^T, \quad (20a)$$

$$(\mathcal{M}^2 + \alpha\mathcal{M})\hat{\mathbf{M}} + (\beta\mathcal{M} + \mathbf{I})\hat{\mathbf{K}} = \mathbb{1}\hat{\mathbf{H}}(\Lambda)^T. \quad (20b)$$

Notice that the above equations can be solved for  $\hat{\mathbf{M}}$  and  $\hat{\mathbf{K}}$ . However, in order to have an analytic expression for the matrices of the reduced-order system in a similar way as for the Loewner matrices (12), we need to introduce the following change of variables:

$$\mathbb{L}^{\text{SO}} := -(\mathbf{I} + \beta\mathcal{M})\hat{\mathbf{M}}(\mathbf{I} + \beta\Lambda), \quad \mathbb{L}_\sigma^{\text{SO}} := (\mathbf{I} + \beta\mathcal{M})\hat{\mathbf{K}}(\mathbf{I} + \beta\Lambda), \quad (21a)$$

$$\hat{\mathbf{B}}^{\text{SO}} := (\mathbf{I} + \beta\mathcal{M})\hat{\mathbf{H}}(\mathcal{M}), \quad \text{and} \quad \hat{\mathbf{C}}^{\text{SO}} := \hat{\mathbf{H}}(\Lambda)^T(\mathbf{I} + \beta\Lambda). \quad (21b)$$

Notice that the two realizations

$$\hat{\Sigma}_{\text{SO}} = (\hat{\mathbf{M}}, \alpha\hat{\mathbf{M}} + \beta\hat{\mathbf{K}}, \hat{\mathbf{K}}, \hat{\mathbf{B}}, \hat{\mathbf{C}}) \quad \text{and} \quad \hat{\Sigma}_{\text{SO}}^{\text{Loew}} = (-\mathbb{L}^{\text{SO}}, -\alpha\mathbb{L}^{\text{SO}} + \beta\mathbb{L}_\sigma^{\text{SO}}, \mathbb{L}_\sigma^{\text{SO}}, \hat{\mathbf{B}}^{\text{SO}}, \hat{\mathbf{C}}^{\text{SO}})$$

are equivalent, i.e., they represent the same transfer function. Hence, the realization  $\hat{\mathbf{H}}_{\text{SO}}^{\text{Loew}}$  also satisfies the interpolation conditions from Problem 1. Additionally, by a simple computation, we obtain that the matrices  $\mathbb{L}^{\text{SO}}$  and  $\mathbb{L}_\sigma^{\text{SO}}$  satisfy the following equations



$$\begin{aligned}\mathbb{L}^{\text{SO}}\mathcal{F}(\mathbf{\Lambda}) - \mathbb{L}_{\sigma}^{\text{SO}} &= -\mathcal{D}(\mathbf{M})\hat{\mathbf{H}}(\mathbf{M})\mathbb{1}^T, \\ \mathcal{F}(\mathbf{M})\mathbb{L}^{\text{SO}} - \mathbb{L}_{\sigma}^{\text{SO}} &= -\mathbb{1}\hat{\mathbf{H}}(\mathbf{\Lambda})^T\mathcal{D}(\mathbf{\Lambda}),\end{aligned}$$

where, for a given matrix  $\mathbf{\Omega}$ ,  $\mathcal{F}(\mathbf{\Omega}) := (\mathbf{I} + \beta\mathbf{\Omega})^{-1}(\mathbf{\Omega}^2 + \alpha\mathbf{\Omega})$  and  $\mathcal{D}(\mathbf{\Omega}) := (\mathbf{I} + \beta\mathbf{\Omega})$ . As a consequence,

$$\mathbb{L}^{\text{SO}}\mathcal{F}(\mathbf{\Lambda}) - \mathcal{F}(\mathbf{M})\mathbb{L}^{\text{SO}} = \mathbb{1}\hat{\mathbf{H}}(\mathbf{\Lambda})^T\mathcal{D}(\mathbf{\Lambda}) - \mathcal{D}(\mathbf{M})\hat{\mathbf{H}}(\mathbf{M})\mathbb{1}^T, \quad (22a)$$

$$\mathbb{L}_{\sigma}^{\text{SO}}\mathcal{F}(\mathbf{\Lambda}) - \mathcal{F}(\mathbf{M})\mathbb{L}_{\sigma}^{\text{SO}} = \mathbb{1}\hat{\mathbf{H}}(\mathbf{\Lambda})^T\mathcal{N}(\mathbf{\Lambda}) - \mathcal{N}(\mathbf{M})\hat{\mathbf{H}}(\mathbf{M})\mathbb{1}^T, \quad (22b)$$

where, for a given matrix  $\mathbf{\Omega}$ ,  $\mathcal{N}(\mathbf{\Omega}) := (\mathbf{\Omega}^2 + \alpha\mathbf{\Omega})$ . Notice that the Sylvester equations (22) are equivalent to (14a) for the case of SO systems. Hence, using those equations, one can derive analytic expressions of  $\mathbb{L}^{\text{SO}}$  and  $\mathbb{L}_{\sigma}^{\text{SO}}$ .

**Definition 2** (SO Loewner matrices) Let us suppose  $\alpha$  and  $\beta$  are known and let

$$d(s) := 1 + s\beta, \quad n(s) := s^2 + \alpha s, \quad \text{and} \quad f(s) := \frac{n(s)}{d(s)},$$

be scalar functions. Then the SO Loewner matrices, namely, the SO Loewner matrix  $\mathbb{L}^{\text{SO}}$  and the shifted Loewner matrix  $\mathbb{L}_{\sigma}^{\text{SO}}$  are given by

$$\mathbb{L}^{\text{SO}} = \begin{pmatrix} \frac{d(\mu_1)\mathbf{v}_1 - d(\lambda_1)\mathbf{w}_1}{f(\mu_1) - f(\lambda_1)} & \cdots & \frac{d(\mu_1)\mathbf{v}_1 - d(\lambda_\ell)\mathbf{w}_\ell}{f(\mu_1) - f(\lambda_\ell)} \\ \vdots & \ddots & \vdots \\ \frac{d(\mu_\ell)\mathbf{v}_\ell - d(\lambda_1)\mathbf{w}_1}{f(\mu_\ell) - f(\lambda_1)} & \cdots & \frac{d(\mu_\ell)\mathbf{v}_\ell - d(\lambda_\ell)\mathbf{w}_\ell}{f(\mu_\ell) - f(\lambda_\ell)} \end{pmatrix}, \quad (23)$$

$$\mathbb{L}_{\sigma}^{\text{SO}} = \begin{pmatrix} \frac{n(\mu_1)\mathbf{v}_1 - n(\lambda_1)\mathbf{w}_1}{f(\mu_1) - f(\lambda_1)} & \cdots & \frac{n(\mu_1)\mathbf{v}_1 - n(\lambda_\ell)\mathbf{w}_\ell}{f(\mu_1) - f(\lambda_\ell)} \\ \vdots & \ddots & \vdots \\ \frac{n(\mu_\ell)\mathbf{v}_\ell - n(\lambda_1)\mathbf{w}_1}{f(\mu_\ell) - f(\lambda_1)} & \cdots & \frac{n(\mu_\ell)\mathbf{v}_\ell - n(\lambda_\ell)\mathbf{w}_\ell}{f(\mu_\ell) - f(\lambda_\ell)} \end{pmatrix}. \quad (24)$$

Moreover, by construction

$$\mathbb{L}^{\text{SO}} = -(\mathbf{I} + \beta\mathbf{M})\hat{\mathbf{M}}(\mathbf{I} + \beta\mathbf{\Lambda}) = -(\mathbf{I} + \beta\mathbf{M})\mathbf{W}^T\mathbf{M}^*\mathbf{V}(\mathbf{I} + \beta\mathbf{\Lambda}).$$

Thus, the following remark holds.

**Remark 3** If we have sufficient interpolation data, then  $\text{rank}(\mathbf{V}) = \text{rank}(\mathbf{W}) = r$ . As a consequence, the rank of the SO Loewner matrix  $\mathbb{L}^{\text{SO}}$  gives us the order of the Rayleigh damped SO minimal realization interpolating the points, since

$\text{rank}(\mathbb{L}^{SO}) = \text{rank}(\mathbf{W}^T \mathbf{M}^* \mathbf{V}) = \text{rank}(\mathbf{M}^*) = \text{order of the minimal SO interpolant.}$

We are now able to state the analogue result to Theorem 1 for Rayleigh-damped SO systems.

**Theorem 3** (SO data-driven identification) *Assume that  $\mu_i \neq \lambda_j$  for all  $i, j = 1, \dots, \ell$ . Additionally, suppose that  $(s^2 + \alpha s)\mathbb{L}^{SO} + (\beta s + 1)\mathbb{L}_\sigma^{SO}$  is invertible for all  $s = \{\lambda_1, \dots, \lambda_\ell\} \cup \{\mu_1, \dots, \mu_\ell\}$ . Then,*

$$\hat{\mathbf{M}} = -\mathbb{L}^{SO}, \quad \hat{\mathbf{K}} = \mathbb{L}_\sigma^{SO}, \quad \hat{\mathbf{B}}^{SO} = (\mathbf{I} + \beta \mathbf{M}) \hat{\mathbf{H}}(\mathbf{M}) \quad \hat{\mathbf{C}}^{SO} = \hat{\mathbf{H}}(\mathbf{\Lambda})^T (\mathbf{I} + \beta \mathbf{\Lambda}),$$

and  $\hat{\mathbf{D}} = \alpha \hat{\mathbf{M}} + \beta \hat{\mathbf{K}}$  satisfy the interpolation conditions from Problem 1.

Theorem 3 allow us to identify a Rayleigh-damped SO from a given interpolation data set (5). As a consequence, it gives a solution for the Problem 1 whenever the constants  $\alpha$  and  $\beta$  are assumed to be known.

We now consider the case where more data than necessary are provided, which is realistic for applications. In this case, the assumptions of the above theorem are not satisfied; thus, one needs to project onto the column span and the row span of a linear combination of the two Loewner matrices. More precisely, let the following assumption be satisfied:

$$\text{rank}\left(\begin{bmatrix} \mathbb{L}^{SO} & \mathbb{L}_\sigma^{SO} \end{bmatrix}\right) = \text{rank}\left(\begin{bmatrix} \mathbb{L}^{SO} \\ \mathbb{L}_\sigma^{SO} \end{bmatrix}\right) = r \quad (25)$$

Then, we consider the compact SVDs

$$\begin{bmatrix} \mathbb{L}^{SO} & \mathbb{L}_\sigma^{SO} \end{bmatrix} = \mathbf{Y}_\rho \mathbf{\Sigma}_l \tilde{\mathbf{V}}^T \quad \text{and} \quad \begin{bmatrix} \mathbb{L}^{SO} \\ \mathbb{L}_\sigma^{SO} \end{bmatrix} = \tilde{\mathbf{W}} \mathbf{\Sigma}_r \mathbf{X}_\rho^T. \quad (26)$$

Using the projection matrices  $\mathbf{V}_\rho$  and  $\mathbf{W}_\rho$ , we are able to remove the redundancy in the data by means of the following result.

**Theorem 4** *The SO realization  $\hat{\mathbf{\Sigma}}_{SO} = (\hat{\mathbf{M}}, \hat{\mathbf{D}}, \hat{\mathbf{K}}, \hat{\mathbf{B}}, \hat{\mathbf{C}})$  of a minimal interpolant of Problem 1 is given as:*

$$\hat{\mathbf{M}} = -\mathbf{Y}_\rho^T \mathbb{L}^{SO} \mathbf{X}_\rho, \quad \hat{\mathbf{K}} = \mathbf{Y}_\rho^T \mathbb{L}_\sigma^{SO} \mathbf{X}_\rho, \quad \hat{\mathbf{D}} = \alpha \hat{\mathbf{M}} + \beta \hat{\mathbf{K}}, \quad (27a)$$

$$\hat{\mathbf{B}} = \mathbf{Y}_\rho^T \hat{\mathbf{B}}^{SO}, \quad \text{and} \quad \hat{\mathbf{C}} = \hat{\mathbf{C}}^{SO} \mathbf{X}_\rho. \quad (27b)$$

Depending on whether  $r$  in (25) is the exact or approximate rank, we obtain either an interpolant or an approximate interpolant of the data, respectively.

### 3.3 Optimizing Parameters

In the previous section, we have shown how to construct a SO realization for given transfer function measurements and a priori knowledge of the parameters  $\alpha$  and  $\beta$  from the Rayleigh damping hypothesis. However, there are several cases, where exact values of  $\alpha$  and  $\beta$  are not known but we rather can have a hint of the range for the parameters, i.e.,  $\alpha \in \mathcal{R}_\alpha$  and  $\beta \in \mathcal{R}_\beta$ . Therefore, as done for delay systems in [31], we also propose a heuristic optimization approach to obtain the parameters  $\alpha$  and  $\beta$  for SO systems, satisfying the Rayleigh damping hypothesis. For this purpose, we split the data training  $\mathcal{D}_{\text{training}}$  and test set  $\mathcal{D}_{\text{test}}$ , e.g., in the ratio 80:20. Hence, we ideally aim at solving the optimization as follows:

$$\min_{\alpha \in \mathcal{R}_\alpha, \beta \in \mathcal{R}_\beta} \mathcal{J}(\alpha, \beta) \quad (28)$$

where

$$\mathcal{J}(\alpha, \beta) := \sum_{(\sigma_k, v_k) \in \mathcal{D}_{\text{test}}} \left\| \hat{\mathbf{H}}_{\text{SO}}(\sigma_k \alpha, \beta) - v_k \right\|^2 + \sum_{(\mu_k, w_k) \in \mathcal{D}_{\text{test}}} \left\| \hat{\mathbf{H}}_{\text{SO}}(\mu_k \alpha, \beta) - w_k \right\|^2,$$

where  $\hat{\mathbf{H}}_{\text{SO}}$  is constructed using only the training data. However, the optimization problem (28) is non-convex, and solving it is a challenging task. Therefore, we seek to solve a relaxed problem. For this purpose, in the paper, we make a 2-D grid for the parameters  $\alpha$  and  $\beta$  in given intervals. Then, we seek to determine the parameters on the grid where the function  $\mathcal{J}(\alpha, \beta)$  is minimized. Nonetheless, solving the optimization problem (28) needs future investigation and so we leave it as a possible future research problem.

### 3.4 A Note on More General Damping Structures

As stated before, the general SO interpolating system has its matrices  $\hat{\mathbf{M}}$ ,  $\hat{\mathbf{D}}$  and  $\hat{\mathbf{K}}$  satisfying an underdetermined system given by (19). Once we assume the Rayleigh damping hypothesis, the system of equations becomes determined and an analytical solution is given by the SO Loewner matrices  $\mathbb{L}^{\text{SO}}$  and  $\mathbb{L}_\sigma^{\text{SO}}$ .

In a more general set-up, we may consider the damping to have a more general structure depending on the matrices  $\hat{\mathbf{M}}$  and  $\hat{\mathbf{K}}$ . One possible way is to assume the damping matrix  $\hat{\mathbf{D}}$  to be described as

$$\hat{\mathbf{D}} = \hat{\mathbf{M}}^{\frac{1}{2}} g \left( \hat{\mathbf{M}}^{-\frac{1}{2}} \hat{\mathbf{K}} \hat{\mathbf{M}}^{-\frac{1}{2}} \right) \hat{\mathbf{M}}^{\frac{1}{2}}, \quad (29)$$

where  $g$  is an analytic function on the positive real axis. It is worth noticing that the Rayleigh damping hypothesis is obtained if we consider  $g(s) = \alpha + \beta s$ . Another

usual choice of damping is the so-called critical damping given by

$$\hat{\mathbf{D}}_{Crit} = 2\alpha\hat{\mathbf{M}}^{\frac{1}{2}} \left( \hat{\mathbf{M}}^{-\frac{1}{2}} \hat{\mathbf{K}} \hat{\mathbf{M}}^{-\frac{1}{2}} \right)^{\frac{1}{2}} \hat{\mathbf{M}}^{\frac{1}{2}},$$

with  $\alpha \in [0.02, 0.1]$ , see [26, 34]. In this case, the damping is obtained with  $g(s) = 2\alpha\sqrt{s}$ .

Hence, if we assume the damping to be given as in (29), then the system of equations in (19) becomes

$$\hat{\mathbf{M}}\boldsymbol{\Lambda}^2 + \hat{\mathbf{M}}^{\frac{1}{2}}g \left( \hat{\mathbf{M}}^{-\frac{1}{2}} \hat{\mathbf{K}} \hat{\mathbf{M}}^{-\frac{1}{2}} \right) \hat{\mathbf{M}}^{\frac{1}{2}}\boldsymbol{\Lambda} + \hat{\mathbf{K}} = \hat{\mathbf{H}}(\mathcal{M})\mathbb{1}^T, \quad (30a)$$

$$\mathcal{M}^2\hat{\mathbf{M}} + \mathcal{M}\hat{\mathbf{M}}^{\frac{1}{2}}g \left( \hat{\mathbf{M}}^{-\frac{1}{2}} \hat{\mathbf{K}} \hat{\mathbf{M}}^{-\frac{1}{2}} \right) \hat{\mathbf{M}}^{\frac{1}{2}} + \hat{\mathbf{K}} = \mathbb{1}\hat{\mathbf{H}}(\boldsymbol{\Lambda})^T. \quad (30b)$$

Notice that in system (30), the number of unknowns matches the number of equations. However, depending on the nature of the function  $g$ , this will lead to a system of nonlinear equations and further investigation is needed to find conditions for the existence (and uniqueness) of a solution and numerical solvers for nonlinear matrix equations. Additionally, in the general case, the Petrov-Galerkin approximation of the damping model would no longer be the damping model of the Petrov-Galerkin approximation, except for the very restricted case where

$$\mathbf{W}^T g(\mathbf{Q}) \mathbf{V} = g(\mathbf{W}^T \mathbf{Q} \mathbf{V})$$

with  $\mathbf{V}, \mathbf{W} \in \mathbb{R}^{n \times r}$  being the projection matrices and  $\mathbf{Q} \in \mathbb{R}^{n \times n}$ . Notice that this happens for the Rayleigh damping, but it is non longer true for the critical damping. Future work will be dedicated on further analysis and numerical methods for these general dampings.

## 4 Numerical Results

In this section, we illustrate the efficiency of the proposed methods via several numerical examples, arising in various applications. All the simulations are done on a CPU 2.6GHz intel® Core™i5, 8 GB 1600MHz DDR3, MATLAB® 9.1.0.441655 (R2016b).

### 4.1 Demo Example

At first, we discuss an artificial example to illustrate the proposed method. Let us consider a SO system of order  $n = 2$ ,  $\boldsymbol{\Sigma}_{SO} = (\mathbf{M}, \mathbf{D}, \mathbf{K}, \mathbf{B}, \mathbf{C})$  whose matrices are given by:

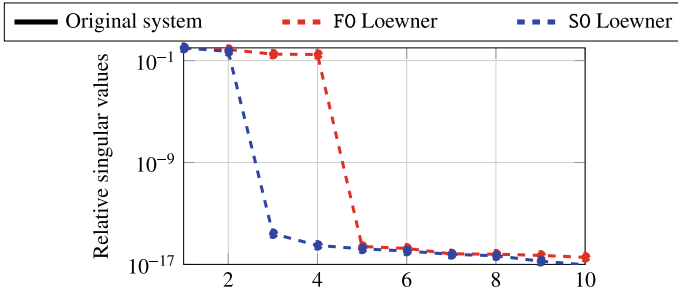


Fig. 1 Demo example: Decay of the singular values for the FO and SO Loewner matrices

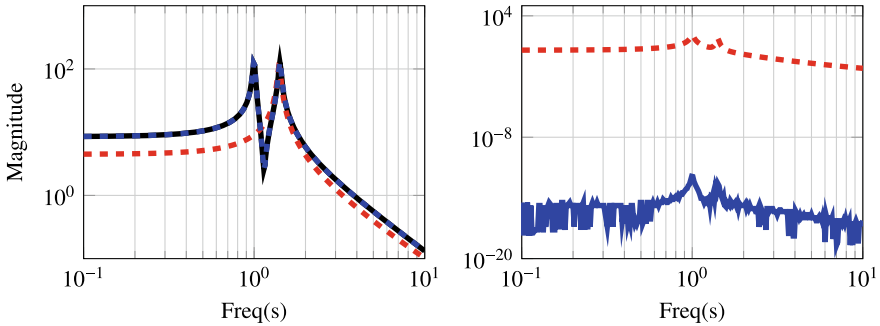


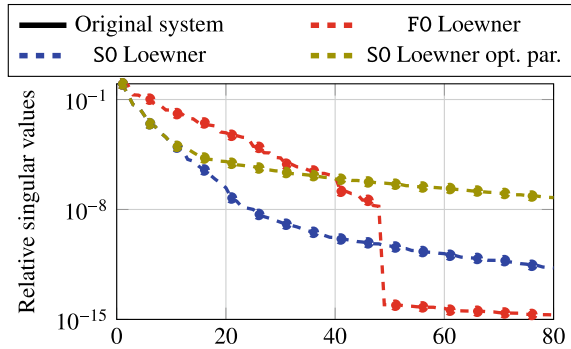
Fig. 2 Demo example: The figure on the left shows the Bode plot of the original system and the FO and SO reduced-order models. The figure on the right shows the Bode plot of the error between the original and reduced-order systems

$$\mathbf{M} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \quad \mathbf{K} = \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix}, \quad \mathbf{D} = \alpha \mathbf{M} + \beta \mathbf{M}, \quad \text{and} \quad \mathbf{B}^T = \mathbf{C} = [2 \ 3],$$

with  $\alpha = 0.01$  and  $\beta = 0.02$ . We collect 20 samples  $(\sigma_j, \hat{\mathbf{H}}_{\text{SO}}(\sigma_j))$ , for  $\sigma_j \in \iota[10^{-1}, 10^1]$  logarithmically spaced. Then, we construct the FO and SO Loewner matrices in (12) and (23), receptively.

In Fig. 1, we plot the decay of the singular values of the  $\mathbb{L}$  and  $\mathbb{L}^{\text{SO}}$  matrices. It can be observed that  $\text{rank}(\mathbb{L}) = 4$  and  $\text{rank}(\mathbb{L}^{\text{SO}}) = 2$ , as expected. Indeed, the demo system has a minimal SO realization of order 2 and a minimal FO realization of order 4. By applying the SVD procedure, we construct two reduced-order models of order 2, one for FO and the other for SO. We compare the transfer functions of the original and reduced-order systems, and the results are plotted in Fig. 2. The figure shows that the error between the original and SO reduced-order system is of the level of machine precision, which means that the SO approach has recovered an equivalent realization of the original model. Additionally, the FO reduced system of order 2 was not able to mimic the same behavior of the original system, showing that a larger order is required in this case.

**Fig. 3** Build example: Decay of the singular values for the FO Loewner matrix and for SO Loewner matrices



### 4.2 Building Example

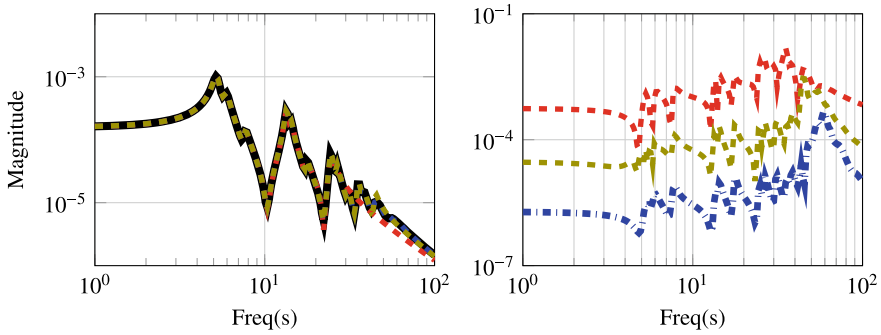
Let us now consider the building model from the SLICOT library [9]. It describes the displacement of a multi-storey building, for example, during an earthquake. It is a FO system of order  $r = 48$ , whose dynamics comes from a mechanical system. The Rayleigh damping coefficients here are  $\alpha \approx 0.4947$  and  $\beta \approx 0.0011$ .

For this example, we collect 200 samples  $\mathbf{H}(i\omega)$ , with  $\omega \in [10^0, 10^2]$ . Then, we build the FO and SO Loewner matrices in (12) and (23), respectively. Additionally, using the heuristic procedure in Sect. 3.3, we constructed the reduced model assuming we do not know a priori the parameters  $\alpha$  and  $\beta$ . After this procedure, we obtain  $\alpha^* = 0.495$  and  $\beta^* = 0.001$ , which are fairly close to the original parameters.

In Fig. 3, we plot the decay of the singular values of the FO Loewner matrix, the SO Loewner matrix for the original parameters  $\alpha$  and  $\beta$ , and the SO Loewner matrix for the estimated parameters  $\alpha$  and  $\beta$ . The decay of the singular values for the SO Loewner matrix with original parameters is faster than for the FO Loewner matrix. However, for the SO Loewner matrix with estimated parameters, the decay of singular values starts fast and then becomes slower. This shows that if the parameters  $\alpha$  and  $\beta$  are not well identified, a higher reduced-order will be needed to interpolate the data. By applying the SVD procedure, we construct three reduced-order models of order 16. We compare the transfer functions of the original and reduced-order systems, and the results are plotted in Fig. 4. This figure shows that for the SO Loewner approach (original parameters or with estimated parameters) outperform the classical Loewner framework.

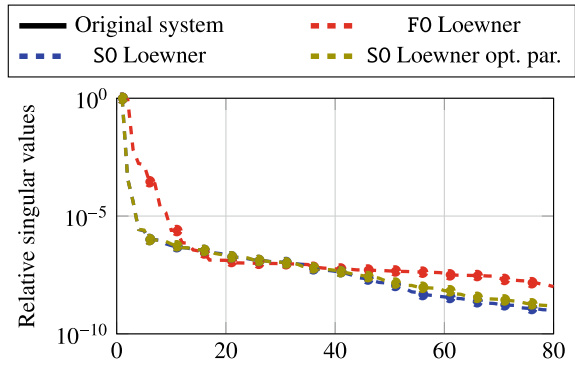
### 4.3 Artificial Fishtail

As the last example, we consider the artificial fishtail model presented in [30]. This model comes from a finite-element discretization of the continuous mechanics model of an artificial fishtail. After discretization, the finite-dimensional system has a SO



**Fig. 4** Build example: The figure on the left shows the Bode plot of the original system and the FO and SO reduced-order models. The figure on the right shows the Bode plot of the error between the original and reduced-order systems

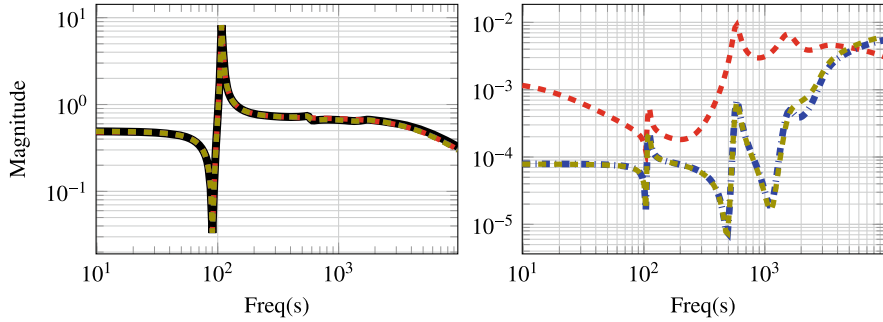
**Fig. 5** Fishtail example: Decay of the singular values for the FO Loewner matrix and for SO Loewner matrices



realization of order 779, 232. For this model, the Rayleigh damping is chosen with parameters  $\alpha = 1.0 \cdot 10^{-4}$ ,  $\beta = 2 \cdot 10^{-4}$ . It is a MIMO system, but for the numerical application, here we consider only the first transfer function, i.e., from  $u_1$  to  $y_1$ .

For this example, we collect 200 samples  $\mathbf{H}(i\omega)$ , with  $\omega \in [10^1, 10^4]$ . Then, we build FO and SO Loewner matrices in (12) and (23), respectively. Additionally, we also compute the reduced model using the heuristic procedure in Sect. 3.3, for which we obtain the estimated parameters  $\alpha^* \approx 1.19 \cdot 10^{-4}$  and  $\beta^* \approx 2 \cdot 10^{-4}$ .

In Fig. 5, we plot the decay of the singular values of the FO Loewner matrix, the SO Loewner matrix for the original parameters  $\alpha$  and  $\beta$ , and the SO Loewner matrix for the estimated parameters  $\alpha^*$  and  $\beta^*$ . By applying the SVD procedure, we construct three reduced-order models of order 8. We compare the transfer functions of the original and reduced-order systems, and the results are plotted in Fig. 6. This figure shows that the SO Loewner approach with original parameters and SO Loewner with estimated parameters outperform the classical Loewner framework.



**Fig. 6** Fishtail example: The figure on the left shows the Bode plot of the original system and the FO and SO reduced-order models. The figure on the right shows the Bode plot of the error between the original and reduced-order systems

## 5 Conclusions

In this paper, we have studied the problem of the identification of Rayleigh-damped second-order systems from frequency data. To that aim, we propose modified SO Loewner matrices which are the key tools to construct a realization interpolating the given data. Additionally, in the case of redundant data, an SVD-based scheme is presented to construct reduced-order models. Moreover, a heuristic optimization problem is sketched to estimate the damping parameters. Finally, we have illustrated the efficiency of the proposed approach in some numerical examples, and we compared the results with the classical Loewner framework.

It is important to emphasize that the current work does not intend to solve the general second-order identification problem. As stated in Sect. 3, the problem of identifying a general second-order system leads to an underdetermined system. Hence, in order to have a unique solution, some other constraints should be added to the problem. As an example, other damping structures could be considered, as discussed in Subsection 3.4. However, this case might lead to nonlinear matrix equations and further analysis and dedicated numerical solvers need to be developed. We leave this topic for future research.

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