Recovery of Rare Earth Elements from Nd-Fe-B Magnet Through Selective Chlorination Using Zinc Chloride



Kyung-Hwan Lim, Chan Choi, Gyeonghye Moon, Tae-Hyuk Lee, and Jungshin Kang

Abstract The selective recovery of rare earth elements from Nd-Fe-B magnets through a novel selective chlorination process using zinc chloride was investigated. A Nd-Fe-B magnet powder and zinc chloride mixture in an alumina crucible was positioned in a gas-tight quartz tube. This quartz tube was placed in an electric furnace preheated to 1000 K for 1.5 h for the reactions. After the experiments, a mixture of metallic iron and neodymium chloride was produced owing to the selective chlorination of rare earth elements in the magnet powder. In addition, the chlorination efficiencies of neodymium, dysprosium, and praseodymium were 96.5%, 57.2%, and 97.6%, respectively, under certain conditions. Therefore, it was demonstrated that the novel selective chlorination using zinc chloride developed in this study is feasible for the efficient recycling of Nd-Fe-B magnets.

Keywords Nd-Fe-B magnet \cdot Selective chlorination \cdot Recovery of rare earth elements

Introduction

Neodymium (Nd)-iron (Fe)-boron (B) magnets with addition of small amount of dysprosium (Dy) have excellent properties such as high coercivity even at high temperatures [1]. Because of these properties, Nd magnets can be used in various applications such as hybrid and electric cars. The demand for green cars is expected

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to increase in the future to meet the need of carbon dioxide (CO_2) gas emission reduction; therefore, the utilization of Nd magnets will increase.

Rare earth elements (REEs) are extracted from several mineral resources such as bastnaesite, monazite, and ion adsorption deposits. Among REEs, light rare earth elements (LREEs), such as Nd and praseodymium (Pr), are extracted from bastnaesite and monazite. These mineral resources are abundant in nature and also distributed around the world [2]. However, heavy rare earth elements (HREEs), such as Dy and terbium (Tb), can only be extracted economically from ion adsorption deposits in the southern parts of China [2]. This is the one reason that China monopolizes the world production of REEs.

During the extraction of LREEs from monazite, environmental threats and radiation risks are encountered, because monazite contains radioactive elements such as uranium (U) and thorium (Th) [2]. Therefore, proper treatments of these radioactive elements generated during the extraction are necessary to preserve the environment. In contrast, ion adsorption deposits contain very little amount of radioactive elements because these elements are washed out because of weathering [2]. However, there are still environmental concerns during the extraction of REEs because they are extracted via elution using ammonium sulfate ((NH₄)₂SO₄).

To produce REEs with preservation of environment, recycling of spent Nd magnets is required. However, only Nd scraps generated in magnet production plants are commercially used as feedstock for recycling because these scraps contain a large amount of REEs and processing costs are minimum [2, 3]. Although spent Nd magnets are not recycled at present, it is necessary to develop an efficient and environmentally sound process for the recovery of REEs from spent magnets when the increase of the use of Nd magnets is considered.

Numerous methods have been developed to recover REEs from spent magnets [4–9]. Among those, the selective recovery of REEs through the chlorination of spent magnets using metal chloride is promising [8, 9]. When the selective chlorination of spent magnets using ferrous chloride (FeCl₂) or magnesium chloride (MgCl₂) is utilized, only REEs are recovered as chloride without chlorination of Fe in magnets. Shirayama reported that Nd in a spent magnet was selectively chlorinated to neodymium chloride (NdCl₃) by reacting with MgCl₂ at 1273 K [8]. In addition, approximately 80% of Nd and Dy was recovered from the initial magnet after the reactions for 12 h [8]. Hua reported that the rate-determining step of the selective chlorination using MgCl₂ is the diffusion of MgCl₂ into an ash layer consisting of Fe metal remained [10].

In this study, a selective chlorination process using zinc chloride $(ZnCl_2)$ was investigated to recover REEs from Nd magnets, as shown in Fig. 1 [11]. When $ZnCl_2$ is used as the chlorinating agent, reaction temperature can be decreased because of its low melting point. In addition, the reaction rate can be increased because low melting temperature of zinc (Zn) metal produced by the chlorination reaction is alloyed with the ash layer of Fe metal. Furthermore, rare earth chlorides such as NdCl₃ can be separated from the residue obtained after selective chlorination by utilizing different vapor pressures at high temperatures.

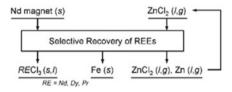


Fig. 1 Flowchart of the selective chlorination of Nd magnet using ZnCl₂ investigated in this study

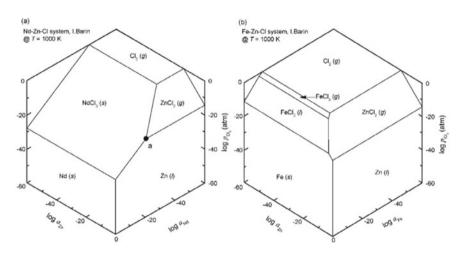


Fig. 2 Chemical potential diagrams of the **a** Nd–Zn–Cl and **b** Fe–Zn–Cl systems at 1000 K (the boiling point of ZnCl₂ is 999.5 K [12] or 1005 K [14] depending on the reference consulted, Reprinted by permission from Springer Nature: Springer, *Journal of Sustainable Metallurgy*, Selective Chlorination of Rare Earth Elements from a Nd–Fe–B Magnet Using Zinc Chloride [15]

Mechanisms of Selective Chlorination of Nd-Fe-B Magnet Using ZnCl₂

Figure 2a, b show the chemical potential diagrams of Nd–Zn–Cl and Fe–Zn–Cl systems, respectively, at 1000 K [12, 13]. ZnCl₂ (*l*,*g*) equilibrates with Zn (*l*) and NdCl₃ (*s*) at point a in Fig. 2a while Nd (*s*) does not coexist with ZnCl₂ (*l*,*g*) at 1000 K. Therefore, when a sufficient amount of ZnCl₂ is used as a chlorinating agent, Nd in the magnets will be chlorinated to NdCl₃ by reacting with ZnCl₂ at 1000 K, as shown in Eq. (1). In addition, Dy and Pr in the magnets also will be chlorinated to dysprosium chloride (DyCl₃) and praseodymium chloride (PrCl₃) by reacting with ZnCl₂ at 1000 K, as shown in Eqs. (2) and (3), respectively. On the other hand, the chemical equilibrium point for FeCl_x (x = 2,3, l,g), ZnCl₂ (*l*,*g*), and Zn (*l*) does not exist, as shown in Fig. 2b. As a result, even though a sufficient amount of ZnCl₂ is used for the reactions, Fe in magnets will not be chlorinated

$$2Nd(s, in Nd-Fe-B magnet) + 3ZnCl_2(l, g) = 2NdCl_3(s) + 3Zn(l)$$

$$\Delta G_r^{\circ} = -785.0 \text{ kJ at } 1000 \text{ K} [12]$$
(1)
$$2Dy(s, in Nd-Fe-B magnet) + 3ZnCl_2(l, g) = 2DyCl_3(l) + 3Zn(l)$$

$$\Delta G_r^{\circ} = -676.0 \text{ kJ at } 1000 \text{ K} [12]$$
(2)
$$2Pr (s, in Nd-Fe-B magnet) + 3ZnCl_2(l, g) = 2PrCl_3(s) + 3Zn(l)$$

$$\Delta G_r^{\circ} = -811.6 \text{ kJ at } 1000 \text{ K} [12]$$
(3)

Experimental

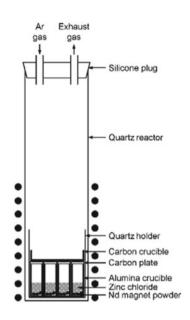
Figure 3 shows a schematic of the experimental apparatus, and Table 1 lists the experimental of the selective chlorination process using $ZnCl_2$ at 1000 K for 1.5 h. A mixture of Nd-Fe-B magnet powder and anhydrous $ZnCl_2$ placed in an alumina (Al_2O_3) crucibles was positioned in a quartz holder inside a glove box. Afterward, the quartz holder was removed from the glove box and placed at the bottom of a gas-tight quartz reactor. The gas inside the reactor was replaced with Ar gas through evacuation and filling of Ar gas. The pressure inside the reactor was maintained at 1 atm during the experiments by flowing Ar gas. After the completion of atmosphere control, the reaction time was finished, the reactor was immediately removed from the furnace and cooled to room temperature. The samples obtained after the selective chlorination reaction were subjected to deionized (DI) water leaching at room temperature for 0.5 h, and the residues obtained after the leaching were dried at 343 K for 0.5 h.

Table 1	Experimental
condition	ns of the selective
chlorinat	ion process using
ZnCl ₂ at	1000 K for 1.5 h

Exp. no ^a	Weight of magnet, w _{magnet} /g	Particle size, $d_{\text{magnet}}/\mu m$	Reaction time, <i>t</i> _r /h
190812b-1	1.000	<75	1.5
190812b-2	1.003	75–150	1.5
190812b-3	1.001	150-300	1.5
190812b-4	1.000	300-600	1.5

a Experimental conditions;

Weight of zinc chloride, $w \operatorname{ZnCl}_2 = 2.72 \text{ g}$ Reaction temperature, T = 1000 K Fig. 3 Schematic of the experimental apparatus (Reprinted by permission from Springer Nature: Springer, *Journal of Sustainable Metallurgy*, Selective Chlorination of Rare Earth Elements from a Nd-Fe-B Magnet Using Zinc Chloride, Kyung-Hwan Lim et al. 2021)



Results and Discussion

Table 2 lists the composition of the Nd magnet used as feedstock. In addition, Fig. 4 shows the results of XRD analysis of the residues obtained after the selective chlorination reactions without water leaching. As expected from the thermodynamic analysis, NdCl₃ and Fe (Zn) were identified after the experiments. DyCl₃ and PrCl₃ were not identified because the feedstock contains low concentrations of these elements, as shown in Table 2.

Further, Fig. 5 shows the influence of the particle size of the feedstock on the chlorination efficiencies of Nd, Dy, and Pr after the experiments. When the particle size of the feedstock used for selective chlorination using ZnCl₂ increased from <75 μ m to 300–600 μ m, the chlorination efficiencies of Nd, Dy, and Pr increased from 93.8%, 36.3%, and 96.0% to 96.5%, 57.2%, and 97.6%, respectively. In addition, the total chlorination efficiency of Nd, Dy, and Pr was 92.1% when the particle size of the feedstock was 300–600 μ m. As the particle size decreased, the chlorination efficiencies of REEs decreased because the concentration of oxygen in the feedstock increased from 0.188 mass% at 300–600 μ m to 0.467 mass% at <75 μ m. REEs in

	Concentration of element <i>i</i> , C_i (mass%) ^a					
	Nd	Dy	Pr	Fe		
Nd magnet feed	20.7	3.71	6.62	66.5		

Table 2 Composition of the Nd-Fe-B magnet used as feedstock

^a Determined by ICP-MS and ICP-OES analysis

the magnet powder feedstock easily react with oxygen during processing because these elements are reactive. However, the oxides of REEs could not be chlorinated to rare earth chlorides by reacting with $ZnCl_2$ at 1000 K. For example, when the oxides of Nd and Dy react with $ZnCl_2$ at 1000 K, neodymium oxychloride (NdOCl) and dysprosium oxychloride (DyOCl) are produced, as shown in Eqs. (4) and (5), respectively [12, 15]. As a result, the chlorination efficiencies of REEs increased when the particle size of the feedstock was increased.

$$Nd_{2}O_{3}(s) + ZnCl_{2}(l, g) = 2NdOCl(s) + ZnO(s)$$

$$\Delta G_{r}^{\circ} = -81.3 \text{ kJ at } 1000\text{K} [12]$$

$$Dy_{2}O_{3}(s) + ZnCl_{2}(l, g) = 2DyOCl(s) + ZnO(s)$$
(4)

$$\Delta G_{*}^{\circ} = -4.2 \text{ kJ at } 1000 \text{K} [12, 15]$$

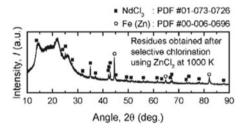
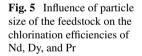
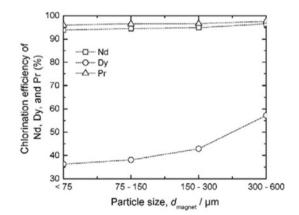


Fig. 4 Results of XRD analysis of the residues obtained after the selective chlorination reactions (Reprinted by permission from Springer Nature: Springer, *Journal of Sustainable Metallurgy*, Selective Chlorination of Rare Earth Elements from a Nd-Fe-B Magnet Using Zinc Chloride, (Kyung-Hwan Lim et al. 2021)





Conclusions

The selective chlorination process using ZnCl₂ to recover Nd, Dy, and Pr from Nd magnets was investigated in this study. When the Nd magnet reacted with ZnCl₂ at 1000 K, Nd in the feedstock chlorinated to NdCl₃; however, Fe in the feedstock did not. In addition, the chlorination efficiencies of Nd, Dy, and Pr reached 96.5%, 57.2%, and 97.6%, respectively, when the particle size of the feedstock used for the chlorination reaction at 1000 K for 1.5 h was 300–600 μ m. As a result, 92.1% of REEs was recovered from the Nd magnets through the selective chlorination process.

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