Chapter 12 Optimization of Reinforcement Parameters and Turning Conditions for Improving Surface Quality of Hybrid Al-SiC-Red Mud Composite for Automotive and Aerospace Components

Amit Chauhan, Jaswinder Singh, and Saroj Bala

1 Introduction

1.1 Machining of Aluminium Matrix Composites (AMCs)

The demand for AMCs is continuously increasing in automotive sector due to increasing fuel prices and environmental emissions. This may be attributed to low weight and high strength and stiffness of these materials that enhance their load bearing ability (Mistry & Gohil, [2016](#page-23-0); Taha, [2001](#page-25-0)). Therefore, AMCs possess higher abrasion resistance and strength in comparison to monolithic materials (metals and alloys). Due to this, these materials are used to design various automotive components, thereby reducing fuel consumption and emissions of greenhouse gases (GHGs) in the transportation sector. Actually, addition of hard ceramic phase (reinforcements) in the AMCs results in increase in the value of elastic modulus and strength that further improves the working performance of these composites (Bains et al., [2016](#page-22-0); Surappa, [2003\)](#page-25-1). However, selection of optimum values of reinforcement parameters, i.e. volume fraction and particle size, is a key area of interest for the researchers. Actually, AMCs may exhibit different mechanical and wear characteristics at different magnitudes of reinforcement parameters. Currently, hard ceramic reinforcements have been considered to be most compatible for developing

S. Bala PG Department of Physics, SGGS College, Chandigarh, Punjab, India

A. Chauhan (\boxtimes)

Department of Mechanical Engineering, UIET, Panjab University, Chandigarh, Punjab, India e-mail: drchauhan98@pu.ac.in

J. Singh

Department of Mechanical Engineering, UIET, Panjab University Regional Centre, Hoshiarpur, Punjab, India

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high-performance Al composites. However, machining response of the AMCs is considerably deteriorated due to the presence of hard ceramic particles (Muthukrishnan et al., [2007;](#page-23-1) Sathish Kumar et al., [2015](#page-24-0)). Therefore, it becomes imperative to fnd the solution to machining challenges related to the AMCs for widespread use of these materials in the various engineering sectors.

The machining characteristics of the AMCs have been investigated and reviewed by various authors, and it has been revealed that machinability of the AMCs can be improved by evaluating optimum combination of reinforcement parameters and cutting conditions (Behera & Sutradhar, [2012](#page-22-1); Das et al., [2014](#page-22-2); Hiremath et al., [2016\)](#page-23-2). Hiremath et al. [\(2016](#page-23-2)) have studied the turning characteristics (machining forces and surface quality) of the $A16061/B₄C$ composites using polycrystalline crystal diamond (PCD) tools. It was found that the cutting forces reduced with increasing reinforcement ratio due to the presence of micro-voids and pores. The machinability of the developed composites was reduced with increasing values of cutting parameters (feed rate and depth of cut) and decreasing value of turning speed. Das et al. [\(2014](#page-22-2)) have discussed various issues regarding the tool wear of Al/ceramic composites during turning operations. It was revealed that the PCD tools exhibit longer life in comparison to other tool materials as far as machining response of these composite was concerned. The results also indicate that tool wear is increased with increase in the values of the reinforcement parameters (percentage and particle size) and the turning conditions. Further, the depth of cut has the lowest infuence on the tool wear during turning operations. Behera and Sutradhar [\(2012](#page-22-1)) have found that surface fnish of the LM6/SiC composites decreases with an increase in SiC content due to increase in the magnitudes of cutting forces. The machining operations were carried out at different cutting speeds (30–103 m/s) and depth of cuts (0.5–1.5 mm) for the same feed rate (0.05 mm/rev). The machining response of the AMCs was found to be dependent upon the magnitude of cutting parameters. The size of chip was also reduced with an increase in reinforcement content, which was an indication of reduction in ductility of the AMCs.

1.2 Hybrid AMCs (HAMCs) and Their Machining Response

During the last decade, the development of the hybrid HAMCs has attracted attention of the researchers due to their low density and superior mechanical perfor-mance and machinability (Rajmohan et al., [2012;](#page-24-1) Singh, [2016;](#page-24-2) Singh & Chauhan, [2014,](#page-24-3) [2016a,](#page-24-4) [2016b](#page-24-5)). Actually, lubricating properties of secondary reinforcements improve wear and machining response of the hybrid composites. Currently, researchers are focusing on development of high-performance HAMCs for various engineering applications. According to Priyadarshi and Sharma [\(2016](#page-23-3)), process parameters for turning of Al6061-based hybrid composites can be optimized for improved machining response. It has been observed that feed rate and cutting depth are signifcant parameters having identical infuence on machining response of the composites. The cutting speed has been found to exhibit minimal infuence on the cutting force, while the surface quality is improved with an increase in the value of cutting speed. Kumar and Chauhan [\(2015](#page-23-4)) have evaluated the surface roughness response of Al-based hybrid composites (Al/SiC/Gr) and ceramic-reinforced composites (Al/SiC) composites under dry turning conditions. The surface roughness of hybrid composites has been found to be lower than that of the SiC-reinforced composites under all combinations of cutting parameters. The feed rate has been found to be the most infuential factor regarding surface quality of the hybrid composites. Also, a lower value of feed rate is required to obtain minimum surface roughness for these composites. Bajavarajappa ([2009\)](#page-22-3) has found that the Al2219/SiC/Gr hybrid composites exhibit improved machining performance compared with Al/SiC composites. The addition of graphite particles reduces tool wear of developed composites due to reduction in friction coefficient between the tool and the composite. Premnath et al. ([2012\)](#page-22-4) have performed experimental investigations to study the milling characteristics of the hybrid $A1/A1_2O_3/Gr$ composites processed by stir casting route under the infuence of control parameters. The authors have also found optimum values of various process variables such as feed rate (50 mm/min), speed (4500 rpm), depth of cut (0.1 mm) and Al_2O_3 content (15 wt.%) for enhanced machining response of these composites. The optimum values of cutting force and surface fnish were obtained as 132.8 N and 0.28 μm, respectively. It has also been revealed that feed rate is a dominant parameter that controls the cutting mechanism in the machining process. However, a number of scratches and marks were also observed on the machined surface at higher magnitudes of the feed rate.

1.3 Optimization Techniques for Machining Response

It has been observed that machinability of the Al composites can be assessed by investigating various response characteristics such as tool wear, cutting force and surface roughness. Among these, surface roughness of the materials is an important parameter for designing automotive components for wear-resistant applications such as engine components, bearings, clutches and brakes (Bajavarajappa, [2009;](#page-22-3) Kumar & Chauhan, [2015](#page-23-4)). It has been revealed that surface quality obtained during machining determines the ability of the materials to withstand severe wear conditions. Moreover, surface texture of the product signifcantly infuences the reliability and appearance of the product. A number of techniques can be used for optimization of selected variables such as reinforcement ratio, cutting speed and depth and feed rate for obtaining minimum roughness value in a machining process (El-Gallab & Sklad, [1998;](#page-22-5) Suresh et al., [2012\)](#page-25-2). Currently, response surface methodology (RSM) technique has been widely used to analyse experimental data and develop mathematical model for multi-response optimization of machining characteristics of Al composites (Bhushan, [2013](#page-22-6); Kant & Sangwan, [2014;](#page-23-5) Srinivasan et al., [2012\)](#page-25-3). Here, experimental data is obtained by employing design of experiment (DOE) approach, while mathematical model for optimum process parameters can be obtained by using statistical techniques. Further, a comparative analysis

between measured and predicted response can also be made for error estimation and to check the validity of the developed model. Bhushan ([2013\)](#page-22-6) has used RSM technique to study the infuence of the cutting parameters in CNC turning of Al7075/15%SiC composites. Also, multi-objective optimization has been successfully achieved via desirability-based approach. It has been found that power consumption and tool wear are reduced by 13.55% and 22.12%, respectively. Srinivasan et al. [\(2012](#page-25-3)) have also applied desirability-based RSM technique for optimization of machining characteristics such as cutting force, tool wear and surface roughness during machining of $LM25/10\%$ Al₂O₃ composites. Kant and Sangwan [\(2014](#page-23-5)) have optimized cutting parameters for optimization of the surface roughness and the power consumption. Results of all these studies indicate that the RSM technique is quite suitable for optimization of output response for machining operation of the AMCs. Focused techniques of extracting micro- and nanocellulose, treatment and modifcation of cellulose, and classifcation and applications of cellulose are presented by Abdoulhdi A. Borhana Omran. In addition, the work looked into how the reinforcement of micro- and nanocellulose can yield a material with improved performance. Their work highlights performances, limitations and possible areas of improvement to accommodate the broader range of engineering applications (Omran et al., [2021](#page-23-6)). Suriani et al. ([2021b\)](#page-25-4) had presented the limitations of natural fbres such as high moisture absorption, due to repelling nature; low wettability; low thermal stability; and quality variation, which lead to the degradation of composite properties. In this work, a combination of a few common manufacturing defect types illustrating the overview of the impact on the mechanical properties encountered by most of the composite manufacturing industries is presented. Norizan Mohd Nurazzi et al. [\(2021](#page-23-7)) have unveiled the successful development related to CNT accompanied polymer composites. The work highlights the mechanical, thermal and electrical performances of a CNT polymer (both single walled and multiwalled). Their work is a crucial pivot in our current understanding of the altered polymer structure after the addition of CNT.

In recent years the eagerness towards learning of biopolymers and growing concerns related to the depletion of resources gave the idea of using PLA (polylactic acid), a biopolymer to be manufactured globally. Therefore, the effectiveness of natural polymers along with PLA is represented in the works of Ilyas et al. ([2021\)](#page-23-8). This research provides an insight to the recent works in PLA-derived bio-composite, its synthesis and biodegradation and its properties, processes, challenges and prospects. Suriani et al. ([2021a](#page-25-5)) have conducted several tests at different concentrations of PET yarn and magnesium hydroxide as a reinforcement material. The results for horizontal burning test, tensile test and scanning electron micrographs (SEM) revealed at what concentrations the samples were best to be used for various purposes. It was summarized that the fammability and tensile properties of OPEFB fbre-reinforced fre-retardant epoxy composites could be reduced while using the fbre volume contents in a manner up to an optimal loading of 20%, with the values of 11.47 mm/min and 4.29 KPa, respectively (Suriani et al., [2021a\)](#page-25-5). Nurazzi et al. [\(2021](#page-23-9)) has presented a study of natural fbres in the application of ballistics and bulletproof vests and helmets. The article also focuses on the effect of layering and sequencing of natural fbre fabric in the composites to advance the current armour structure system. Alsubari et al. [\(2021](#page-22-7)) has reviewed the drawbacks of loading conditions while using the natural fbres, countered to fbre treatment and hybridization. This study shows the uses of sandwich structure, in a combination of two or more individual components with different properties, which when joined together can give a better performance. The study also shows the application of natural fbre composites in sandwich structures to be minimal. Therefore, their work shines a light on the possibility of using a natural fbre composite in sandwich structure applications. It addresses the mechanical properties and energy-absorbing characteristics of natural fbre-based sandwich structures tested under various compression loads. The results and potential areas of improvement in engineering applications were discussed.

1.4 Novel HAMCs and Objectives of the Study

Although a number of investigations are available for machining characteristics of the AMCs, limited research is available on the investigation of the surface roughness of the HAMCs reinforced with industrial waste materials. However, various types of waste materials like fy ash (FA), red mud (RM), rice husk ash (RHA), etc. have been used for development of lightweight, low-cost and high-performance HAMCs (Rajmohan et al., [2012](#page-24-1); Singh & Chauhan, [2016a](#page-24-4)). The use of these materials can overcome the problem of disposal of waste materials produced in large quantities while reducing the cost of the developed composites. The RM powder is available in abundance at processing sites of the aluminium (available from bauxite ore). Currently, it is being disposed in open land leading to water, soil and air pollution. It is also used in a number of applications such as extraction of metallic elements and cement industry. But, disposal of this waste product in a sustainable manner is still a challenge for the researchers and the scientists. The RM contains oxides of different elements like Fe, Al, Si, Ti, Na and Ca (Singh & Chauhan, [2017a](#page-24-6)). The results of previous studies indicate that the addition of RM powder results in improvement in mechanical and wear properties of HAMCs (Kumar & Megalingam, [2017;](#page-23-10) Singh & Chauhan, [2017b,](#page-24-7) [2018,](#page-24-8) [2019](#page-24-9)). However, machining of SiC- and RM-flled Al composites is not investigated till date. Therefore, Al/SiC/ RM composites are developed in this study and their turning behaviour has been investigated using CNC lathe machine. Also, optimum values of reinforcement and cutting parameters have been obtained for minimum roughness (improved surface finish) of the developed composite. The influence of process variables (reinforcement parameters and cutting conditions) on machinability response (surface roughness) of HAMCs has also been studied by using RSM technique. The composites are produced via liquid metallurgy route, and dry turning operations are carried out to study the surface quality of the developed composites using Taguchi's approach. The infuence of variables on the surface quality of the developed composites has

been studied by using statistical analysis of experimental results and examination of the chips formed during machining of the composites.

2 Materials and Methods

2.1 Materials

In this work, Al2024 was used as a matrix alloy due to its widespread use in the automotive and aerospace industries. The main constituents of this alloy are Al (more than 90%), Cu (about 4%) and Mg (nearly 1.5%) (Rahimi et al., [2015\)](#page-24-10). This alloy was purchased from the local market in the form of thin sheets that can be converted into liquid form at a temperature of 700 °C. The second reinforcement used for fabrication of Al2024 alloy-based hybrid composites was the red-mud powder that is a waste material obtained during production of alumina from the bauxite ore (during Bayer's process). It has been noted that about 1–2 tons of red mud are produced for each ton of the alumina production. Therefore, a million tons (more than 4 million tons) of red mud is produced on daily basis in India that is either stored (for metal recovery or other uses) or released to the waste land. The disposal of this material ultimately leads to soil, water and atmospheric pollution. Therefore, an effective waste disposal of this material will not only reduce the harmful environmental impact, but it will also lead to reduction in the storage/disposal cost. The major elements present in the red-mud powder are Na, Al, Si, Ca, Ti, Fe, S and K with some traces of radioactive elements. The red mud used in the present investigation was brought from aluminium refnery of Hindalco located at Renukoot, Uttar Pradesh, India. It can be observed that the red-mud powder mainly consists of oxides of various elements such as Fe, Al, Si, Ti, Na and Ca that indicates the red mud can be used as a sustainable reinforcement in the Al composites.

2.2 Method

In the present study, casting process was designed in such a way as to reduce particle clustering and porosity in the developed composites. Also, SiC and RM particles were incorporated in the alloy matrix using stir casting set-up. Although stir casting has been found to be an economic and reliable technique, process variables (stirring and casting variables) are required to be selected carefully so as to produce nearly homogeneous composites (Ramanathan et al., [2019](#page-24-11); Singh, [2016](#page-24-2); Singh & Chauhan, [2018\)](#page-24-8). The reinforcements were incorporated in the alloy matrix using an electric furnace and a mechanical impeller. The former was used to heat the alloy above melting temperature, while the latter created the vortex motion required for mixing of the molten alloy and the reinforcements. Figure [12.1](#page-6-0) shows various components

Fig. 12.1 Components of casting machine used for fabrication of composites

Table 12.1 Parameters for the process parameters used for fabrication of composites

Parameter	Value
Melting temperature in the furnace $(^{\circ}C)$	750
SiC fraction $(\%)$	5 (fixed)
Red-mud fraction $(\%)$	5–20 (variable)
Mg fraction $(\%)$	
Preheating temperature of reinforcements $(°C)$	200
Stirring velocity (rpm)	$200 - 250$
Stirring time (min)	30
Preheating temperature of moulds $(^{\circ}C)$	400

of casting machine used for fabrication of the composites. Also, various process parameters selected for fabrication of composite specimens have been presented in Table [12.1](#page-6-1). The mixing of the molten alloy and the reinforcements was carried out in the graphite crucible of the furnace. Further, 1 wt.% of Mg was also added in the alloy melt in order to minimize the particle agglomeration in the composite specimens. After mixing of all the constituents, composites were casted in the preheated steel moulds (cylindrical shape) through the bottom pouring system. The composite specimens were then subjected to heat treatment under T6 conditions for obtaining adequate microstructural properties of the composites. In this process, solution treatment of the specimens was done at a temperature of 500 °C for a time period of 2 h. Thereafter, the specimens were quenched in cold water followed by age hardening at 150° C for 20 h.

2.3 Microstructural Characterization of the Composites

The scanning electron micrographs (SEM) of SiC and RM particles are shown in Fig. [12.2](#page-7-0), indicating that the shape of RM particles is nearly spherical, while SiC particles have sharp edges. Further, SEM image of the Al composites is presented in Fig. $12.3(a)$, indicating that both types of reinforcement particles are present in the composite specimens. The microstructure of composites has been observed to be nearly uniform. This may be due to the optimum conditions selected for casting of the specimens. The agglomeration of particles is also visible at some places that may be attributed to the higher fraction (20 wt.%) of RM particles. Similarly, various constituent particles like Al, Cu, Mg, O, F, Ca, etc. present in the composites are confrmed by electron dispersive spectrum (EDS) analysis as indicated in Fig. [12.3\(b\)](#page-8-0).

2.4 Machining of Composite Samples

The cylindrically extruded cast samples were machined on a CNC lathe machine (Ace Micromatic; model: LT-20XL450) with self-centred three-jaw chuck. The maximum diameter and length of the samples that can be turned on the machine are 190 mm and 224 mm, respectively. The CNC turning lathe used to conduct experiments has a range of spindle speed as 40–4000 rpm. The turning process was designed in accordance with the recommendations of previous investigations

Fig. 12.2 SEM images of the SiC and RM particles

Fig. 12.3 (**a**) SEM image and (**b**) EDS spectrum of developed composites at a RM fraction of 5 wt. $%$

(Pramanik et al., [2008\)](#page-23-11). For this, tungsten-coated carbide medium cutting insert (CCMT 09T304 MT) having the following geometry has been used: positive 80° rhombic with 7° clearance angle. The cost of machining with these inserts is considerably lower in comparison to other inserts like PCD inserts. It has also been found that dry sliding machining is a very popular method due to environmental hazards related to the use of cutting fuid (Goindi & Sarkar, [2017](#page-23-12); Sreejith & Ngoi, [2000\)](#page-25-6). Therefore, machining operations were performed under dry tuning conditions on a CNC lathe machine. These carbide inserts were fxed tightly in the tool holder for turning operations. There were four edges on each insert and each turning operation was carried out with a new edge. The experimental set-up used for turning operations has been shown in Fig. [12.4\(a\),](#page-9-0) while the machined samples of the developed composites have been shown in Fig. [12.4\(b\)](#page-9-0). In this study, the diameter and length of each specimen were prepared as 12 mm and 50 mm, respectively. Three cutting parameters, i.e. depth of cut (0.05–0.2 mm), cutting speed (400–1600 rpm) and feed

Fig. 12.4 (**a**) Experimental set-up for CNC lathe machine used for turning of the specimens and (**b**) machined samples

rate (0.2–0.8 mm/rev), have been selected to investigate the turning behaviour of the hybrid composites. The average roughness (Ra value) of the composite's surface was evaluated using Mitutoyo SS220 roughness tester, which can evaluate roughness value up to 0.01 μm.

3 Experimental Design and Mathematical Modelling

RSM is a statistical tool of mathematical modelling for optimization of the output response for machining of the materials. Therefore, it can be used to evaluate relationship for the output response in terms of input variables. The RSM technique involves three steps (Makadia & Nanavati, [2013](#page-23-13); Song et al., [2019](#page-24-12)):

– In the frst stage, experiments are conducted to evaluate the output response using experimental design approach. This approach uses minimum number of experiments for evaluating the output response, thereby reducing cost involved in the experimental phase of investigations.

- Thereafter, mathematical models are developed based on the outcome of the experiments. The relationship between the process variables is defned and the output response has been expressed as a polynomial equation.
- In the last stage, various statistical techniques like response plots and analysis of variance (ANOVA) have been applied to evaluate the optimum combination of process variables.

Many researchers have used Taguchi's technique of experimental design to investigate machining processes such as drilling, turning and milling since it is economic and less time consuming (Ghani et al., [2005;](#page-22-8) Radhika et al., [2014b\)](#page-24-13). Here, investigations for the surface roughness have been performed under 'smaller the better' category. The signal-to-noise (*S*/*N*) ratio for has been obtained from the following relation (Ross, [1996;](#page-24-14) Roy, [1990;](#page-24-15) Taguchi et al., [1989\)](#page-25-7):

$$
\frac{S}{N} = -10\log\frac{1}{n}\left(\sum y^2\right)
$$
 (12.1)

where '*n'* stands for number of experimental outputs and '*y'* represents the observed data.

In the present study, fve variables (RM fraction and size, cutting depth, feed rate, and cutting speed) have been selected to study the turning behaviour of the hybrid composites. For precise assessment, more than two levels of parameters are required to be selected. In this study, four levels of the process parameters have been selected and details of the parameters have been shown in Table [12.2](#page-10-0).

Based on the selected parameters, L16b plan has been used for evaluating roughness output of the turning process. The turning operations have been conducted as per parametric conditions shown in Table [12.3](#page-11-0). The results for the surface roughness along with *S*/*N* ratios have also been shown in Table [12.3](#page-11-0). Each experiment was performed two times at two different geometric locations, and average values have been taken for further analysis.

Based on experimental results, RSM model has been developed for the surface roughness of composite specimens as a polynomial equation. It has been observed in previous studies that higher-order interactions are insignifcant in engineering problems. Thus, these are not considered in the present case, and surface roughness equation can be written as frst-order polynomial equation as follows:

		Level			
Parameter	Variable code		2	3	4
Red-mud contents $(wt, \%)$	А		10	15	20
Red-mud size (μm)	B	125	88	75	37
Depth of cut (mm)	C	0.05	0.1	0.15	0.2
Feed rate (mm/rev)	D	0.2	0.4	0.6	0.8
Cutting speed (rpm)	E	400	800	1200	1600

Table 12.2 Variables for investigating machining characteristics of Al/SiC/RM composites

		Factor code				Surface roughness (Ra)			S/N ratio (dB)
S. No.	A	B	\mathcal{C}	D	E	R1	R ₂	Average	
1	5	125	0.05	0.2	400	0.47	0.55	0.510	5.8486
$\overline{2}$	5	88	0.10	0.4	800	1.19	0.91	1.050	-0.4237
3	5	75	0.15	0.6	1200	2.43	2.51	2.470	-7.8539
$\overline{4}$	5	37	0.20	0.8	1600	1.88	1.91	1.895	-5.5521
5	10	125	0.10	0.6	1600	1.42	1.28	1.350	-2.6066
6	10	88	0.05	0.8	1200	0.96	1.02	0.990	0.08730
7	10	75	0.20	0.2	800	1.17	1.05	1.120	-0.9843
8	10	37	0.15	0.4	400	1.34	1.08	1.210	-1.6557
9	15	125	0.15	0.8	800	0.97	1.09	1.030	-0.2567
10	15	88	0.20	0.6	400	1.30	1.33	1.315	-2.3785
11	15	75	0.05	0.4	1600	0.71	0.73	0.720	2.8553
12	15	37	0.10	0.2	1200	0.42	0.58	0.500	6.0206
13	20	125	0.20	0.4	1200	0.92	1.02	0.970	0.2645
14	20	88	0.15	0.2	1600	0.80	0.81	0.805	1.4116
15	20	75	0.10	0.8	400	1.37	1.13	1.250	-1.9382
16	20	37	0.05	0.6	800	0.50	0.58	0.540	5.3521

Table 12.3 Experimental layout and results for output response (surface roughness)

$$
SR = b_o + \sum_{i=1}^{k} b_i X_i + \sum_{j=1}^{k} \sum_{i=1}^{k} b_{ij} X_i X_j + e
$$
 (12.2)

where:

SR is the output response.

 b_o , b_i and b_{ii} are the regression coefficients.

Xi and *Xj* represents process variables for *i*th and *j*th terms.

e is the experimental error.

The regression coefficients can be obtained from statistical analysis of the experimental data presented in Table [12.3.](#page-11-0) Further, ANOVA has been used to evaluate the signifcant terms in CNC machining of the developed composites. The value of coefficient of determination (R^2) was determined to validate the mathematical model. As the value of R^2 approaches unity, the better is the fitness of the developed model. The regression correlation developed for the surface roughness in terms of signifcant parameters (main effects and interaction terms) is given below:

 $ASR = 0.9322 - 0.003608A - 0.000146B + 0.2234C + 0.2485D + 0.000029E$ $-0.000799BD + 0.000001BE$. 0 000144 *DE* (12.3)

The values of all the coefficients of significant terms have been evaluated using Minitab-17 software, and Eq. [\(12.3\)](#page-11-1) presents the fnal relation between the average surface roughness (ASR) and significant factors. The value of $R²$ has been found to be greater than 90%, indicating that mathematical model is adequate for evaluating the output response. Here, a correlation graph (between measured and predicted response) and normal probability plot (for residuals) have also been drawn using Minitab-17 software for validating the developed model for surface roughness of the hybrid composites as shown in Fig. 12.5 . Figures $12.5(a)$ and (b) show that all the data points in these graphs are found to be close to the ftted lines with a few exceptions. This shows that the developed model for surface quality of the composites adequately fts the investigated range of parameters.

4 Analysis of Experimental Results

4.1 Ranking of Parameters

The *S*/*N* ratio data has been used to obtain the infuence of input variables. The analysis of *S*/*N* ratio has been done by evaluating the average data for various levels of input variables. The ranks of input variables have been obtained using delta statistics that represents the difference between the highest and lowest values of *S*/*N* ratio related to each variable. The input variable with maximum value of delta is given frst rank. Further, the minimum value of delta indicates the lowest rank for a variable. Table [12.4](#page-14-0) presents results regarding *S*/*N* ratio response for surface roughness of the composites. The delta has been found to be highest for depth of cut (C) parameter. Therefore, the depth of cut has been ranked frst regarding surface roughness of the composites. Further, cutting speed (E) exhibits minimum value of delta, indicating its lowest rank. In order to evaluate the optimum process conditions, response plots are plotted for *S*/*N* ratio. Here, larger value of *S*/*N* ratio is required for minimum variance of output near the desired response. Figure [12.6](#page-14-1) presents main effect plots for *S*/*N* ratio for roughness value of the composites indicating variations in the *S*/*N* ratio with respect to different levels of the parameters. The *S*/*N* ratio has been found to be maximum at a RM fraction (A) of 15 wt.%, RM size (B) of 37 μ m, cutting depth (C) of 0.05 mm, feed rate (D) of 0.2 mm/rev and cutting speed (E) of 800 rpm. Therefore, optimum combination for obtaining minimum value of surface roughness is found to be A3-B4-C1-D1-E2.

4.2 Signifcance of Parameters

Here, ANOVA analysis has been performed for the experimental data for surface roughness with a confdence level of 95% for evaluating the individual contributions of the parameters. All the candidate terms (main and interaction) are analysed

Fig. 12.5 (**a**) Correlation and (**b**) normal probability plots for the developed model for surface roughness of hybrid composites

for a signifcant contribution in the surface roughness response. The *p*-values have been evaluated for all of the candidate terms. The terms with *p*-value lower than 0.05 are signifcant terms regarding surface roughness values of the composites. Table [12.5](#page-15-0) presents the results of ANOVA modelling with a value of R^2 as 0.9589,

Level/factor	A	B	C	D	Е
	-1.99533	1.04121	3.53534	3.07411	-0.03096
	-1.28986	-1.98079	0.26298	0.25961	0.92181
	1.55967	-0.32585	-2.08869	-1.87175	-0.37037
	1.27253	0.81244	-2.16262	-1.91496	-0.97347
Delta	3.55500	3.02200	5.69797	4.98907	1.89528
Rank		4		2	

Table 12.4 *S*/*N* ratio response for roughness value smaller-is-better

Fig. 12.6 Response plots for *S*/*N* ratio for surface roughness for Al2024/SiC/red-mud composites

indicating that the model provides excellent ft for parametric infuence on surface roughness of the composites.

The results presented in Table 12.5 also indicate that RM wt.% (A), depth of cut (C) and feed rate (D) are main factors with signifcant contributions in machining characteristics of the composites since their *p*-values are lower than 0.05. Further, *p*-values of other main factors, i.e. RM size (B) and cutting speed (E), are found to be 0.942 and 0.157, respectively. Therefore, these parameters are considered to be insignifcant for machining response of hybrid composites. Further, *p*-values of B*D, B*E and D*E (interaction terms) are obtained as 0.025, 0.004 and 0.003, respectively. Therefore, these interaction terms are considered to have signifcant effect on the machining response of developed composites. Table [12.6](#page-15-1) presents the individual contribution of all the signifcant parameters (main and interaction effects). Here, cutting depth (C) has maximum contribution of 35.30% on the roughness value. Further, contributions of RM wt.% (A) and feed rate have (D) been

Source	DF	Adj SS	Adj MS	F -value	P -value	Contr. regression
	8	0.007065	0.000883	20.40	0.000	-
A	1	0.002085	0.002085	48.16	0.000	28.65%
B	1	0.000000	0.000000	0.01	0.942	Ω
C	1	0.002494	0.002494	57.62	0.000	33.84%
D	1	0.001958	0.001958	45.24	0.000	26.57%
E	1	0.000109	0.000109	2.51	0.157	1.04%
$B*D$	1	0.000351	0.000351	8.11	0.025	4.76%
$B*E$	1	0.000734	0.000734	16.96	0.004	9.96%
$D*E$	1	0.000838	0.000838	19.37	0.003	11.37%
Error	7	0.000303	0.000043			4.11%
Total	15	0.007368				100%

Table 12.5 Results for ANOVA analysis for surface roughness value

Model summary for transformed response: $S = 0.0065792$, $R^2 = 95.89$, R^2 (adj) = 91.19

Table 12.6 Contribution of significant main factors and the interaction effects for Al2024/SiC/ red-mud composites

Factor code	$\overline{1}$	◡	$D*F$	$D * D$	DAD
Contribution $(\%)$	ግቤ ድ1 27.01	35.30	4.96		11.86

found as 29.51% and 27.71%, respectively. Further, interaction effect of feed rate and cutting velocity (D*E) has a contribution of 11.86% regarding the machining response of the composites. Also, the interaction effects of particle size with cutting speed and feed rate $(B*E$ and $B*D$) have contributions of 10.38% and 4.96%, respectively.

4.3 Infuence of Parameters on Surface Roughness

In previous reports, it has been revealed that surface roughness of the MMCs depends on the variations in the magnitude of cutting force. However, different types of mechanisms like particle fracture, ploughing and chip formation contribute in variations in the cutting force during machining operations (Kumar & Chauhan, [2015;](#page-23-4) Priyadarshi & Sharma, [2016](#page-23-3)). Therefore, variations in surface roughness have been investigated based on the predominant cutting mechanisms in this study. For this, 3D response plots for roughness value w.r.t. RM fraction and other parameters, i.e. particle size, depth of cut, feed rate and cutting velocity, have been generated as shown in Figs. [12.7](#page-16-0)[–12.10.](#page-17-0)

First of all, it has been observed that surface roughness of composite specimens is reduced with increasing value of RM fraction (5–20 wt.%) irrespective of the magnitude of other parameters. This is an indication that surface fnish is improved with an increase in RM fraction in the composites. Actually, RM particles have lubricating characteristics due to which a thin layer is formed at the interface of the

Fig. 12.7 Surface plot for surface roughness vs red-mud content and particle size for the Al2024/ SiC/red-mud composites

Fig. 12.8 Surface plot for surface roughness vs red-mud content and depth of cut for the Al2024/ SiC/red-mud composites

composite sample and the cutting insert (during turning operation) (Roy, [1990\)](#page-24-15). Thus, friction coefficient and heat generated in cutting zone are reduced, which improves the surface quality of the composites with increasing RM fraction. Therefore, the surface fnish is signifcantly improved with an increase in the value

Fig. 12.9 Surface plot for surface roughness vs red-mud content and feed rate for the Al2024/SiC/ red-mud composites

Fig. 12.10 Surface plot for surface roughness vs red-mud content and cutting speed for the Al2024/SiC/red-mud composites

of RM percentage. However, it has also been observed in these plots that this effect has been observed to be reduced at a higher RM fraction (15–20 wt.%). This may be attributed to agglomeration of reinforcement particles at a higher RM percentage (as seen in Fig. 3). This results in particle cracking and debonding during machining operation, ultimately increasing the roughness value of the composites in the turning process (Sekhar & Singh, [2015\)](#page-24-16). As far as the infuence of particle size is concerned, Fig. [12.7](#page-16-0) shows that surface roughness is slightly increased with increasing particle size $(37-125 \text{ }\mu\text{m})$. This is due to the fact that large particles are easily fractured during machining and debonding occurs resulting in a higher roughness value.

In Figs. [12.8](#page-16-1) and [12.9](#page-17-1), it has also been revealed that lower values of feed rate (0.2–0.8 mm/min) and cutting depth (0.05–0.20 mm) are required in order to obtain higher surface fnish of hybrid composites. The increase in the value of the depth of cut increases the particle debonding and surface resistance at work-tool interface (Priyadarshi & Sharma, [2016](#page-23-3)). This results in an increase in the magnitudes of cutting and fractional forces along the tool-chip interface leading to reduced surface fnish. Similar trends have been observed for variations in the surface roughness with respect to feed rate. The higher feed rate results in increase in the speed of introducing the composite surface to the cutting tool, thereby increasing the resistance force offered by the workpiece to the cutting tool. This ultimately decreases the roughness value for the composites with increasing feed rate. Figure [12.10](#page-17-0) also shows that surface roughness is decreased with increasing cutting speed (400–1600 rpm). It has been noticed that a large material fow takes place at a lower cutting speed that increases the frictional force and cutting force at the interface (Kumar & Chauhan, [2015](#page-23-4)). On the other hand, the deformation of the workpiece is less at a higher cutting velocity. Therefore, frictional force and surface temperature are reduced. Thus, better surface fnish of the workpiece is obtained at a higher cutting speed.

In overall, it has been observed in surface plots that surface roughness of the hybrid composites varies signifcantly with respect to reinforcement percentage, cutting depth and feed rate. On the other hand, roughness value varies slightly with change in the values of cutting speed and particle size. These results are in line with those obtained in the ANOVA analysis. Thus, a higher value of reinforcement percentage and speed and minimum values of particle size, cutting depth and feed rate are required for obtaining the minimum value of surface roughness.

4.4 Analysis of Chip Formation

Figure [12.11](#page-19-0) presents the shapes of chips formed during machining of composite samples under different process conditions. To study the infuence of machining parameters (cutting depth and feed rate) on chip formation, reinforcement fraction was taken constant (5 wt.%). The analysis shows that size of the chips increases with increasing magnitudes of cutting parameters. At lower magnitudes of feed rate (0.2 mm/rev) and depth of cut (0.05 mm), short and segmented chips are formed during turning of the composites. It has also been observed that the chips formed are long in size and curly in shape at higher values of cutting depth (0.2 mm) and feed rate (0.8 mm/rev). Actually, composites tend to behave in a brittle manner with increase in the values of cutting parameters. Further, thickness and length of the

Fig. 12.11 Chip formed during turning of Al/SiC/RM composites under different cutting conditions

chips are increased with increasing RM fraction (from 5 wt.% to 20 wt.%). The chips formed at a RM fraction of 20 wt.% are coil spring type having large length. The surface of chips is also smoother and brighter. This is due to reduced interface temperature and favourable chip-tool interaction. The reduction in the interface temperature is an indication of the reduced cutting forces due to self-lubricating characteristics of RM particles present in the hybrid composites (Priyadarshi & Sharma, [2016](#page-23-3)).

To study predominant cutting mechanism, SEM images of the chips formed during turning of hybrid composites have been investigated under different parametric conditions. Figure [12.12](#page-20-0) presents the micrographs of the chips formed under variable parametric conditions, i.e. feed rate, cutting depth and RM fraction (for the same RM size and speed). At higher values of feed (0.6 mm/min) and depth (0.1 mm) and lower fraction of RM particles (10 wt.%), extensive plastic deformation of the composite surface has been noticed. This extensive surface damage and material flow on the chip surface can be clearly observed in Fig. $12.12(a)$. Actually, cutting force required under these conditions is comparatively large resulting in higher temperature and increased thermal softening of the composite surface (Dwivedi et al., [2012\)](#page-22-9). Therefore, surface damage is increased and poor surface fnish is obtained

Fig. 12.12 SEM examination of chips formed during turning of specimens at (**a**) RM fraction of 10 wt.%, cutting depth of 0.10 mm and feed rate of 0.6 mm/rev and (**b**) RM fraction of 15 wt.%, cutting depth of 0.05 mm and feed rate of 0.40 mm/rev, for a cutting speed of 1600 rpm

under these conditions. Further, decrease in the values of cutting parameters, i.e. feed rate (from 0.6 mm/min to 0.4 mm/rev) and cutting depth (from 0.1 mm to 0.05 mm), and increase in RM fraction (from 10 wt.% to 15 wt.%) reduce damage of the composite surface as indicated in Fig. $12.12(b)$. This is due to reduced cutting force required to cut the composite samples. Therefore, machined surface exhibits improved surface fnish under these conditions. Overall, SEM examination reveals that low values of cutting parameters and higher RM fraction improve surface quality of the composites. Therefore, SEM micrographs agree with statistical analysis, i.e. these input variables signifcantly control the machining response of the hybrid composites.

4.5 Confrmation Experiment

In this section, results of the conformation experiment are presented to verify the developed model for improved surface quality of the composites. For this purpose, measured and predicted output of the composites has been compared under optimum combination of parameters. The experimental output for the roughness value has been obtained using standard procedure discussed in Sect. [2,](#page-5-0) while predicted response is calculated using the following equation (Ghani et al., [2005;](#page-22-8) Radhika et al., [2014a;](#page-24-17) Suresh Kumar, [2015\)](#page-25-8):

$$
N_o = \sum_{i=1}^{n} (N_i - N_m) + N_m
$$
 (12.4)

where N_m is aggregate mean *S/N* ratio, N_i is mean obtained at optimum combination of parameters and *n* is number of main design variables. The results of the confrmation experiment conducted at optimum combination of parameters are presented in

	Statistical data		Observed data		
Optimum level of parameters	Output	<i>S/N</i> ratio	Output	<i>S/N</i> ratio	Deviation $(\%)$
$A3-B4-C1-D1-E2$	0.425	7.432	0.405	7.851	4.17
$A3-B4-C2-D1-E3$	0.526	5.581	0.500	6.020	5.2
<i>Improvement</i>			23.45%		

Table 12.7 Comparison of the predicted and observed data for surface roughness of Al2024/SiC/ red-mud composites under optimum conditions

Table [12.7.](#page-21-0) The experimental results are compared with the predicted response and a deviation is obtained up to a level of about 4–5%. Further, a maximum of 6.0202 of *S*/*N* ratio has been obtained under the investigated conditions. Upon comparing the results under optimum combination of parameters obtained in Table [12.7](#page-21-0) (A3-B4-C1-D1-E2) with those obtained in Table [12.3](#page-11-0) (A3-B4-C2-D1-E3), it can be observed that a minimum of 23.45% improvement in the *S*/*N* ratio for roughness value has been obtained by optimization of the various control parameters.

5 Conclusions

The chapter presents the study of surface roughness of the machined surface of Al/ SiC/RM composites under sustainable (dry machining) conditions. The composite specimens are produced via liquid metallurgy route, and turning operations have been performed on these specimens under different parametric conditions. Also, Taguchi's technique has been used for conducting experiments and the average value of surface roughness is obtained using MITUTOYO roughness tester. The results are analysed using statistical techniques for signifcant contributions of parameters in the output response. The conclusions of this study are as follows:

- 1. The 15 wt.% of RM content, 37 μm of particle size, 0.02 mm of cutting depth, 0.2 mm/rev of feed rate and 88 rpm of cutting speed are the optimum parameters for obtaining minimum surface roughness for the composites.
- 2. The depth of cut has maximum infuence of about 33% in the surface characteristics of the Al composites followed by RM wt.% (28% contribution) and feed rate (26% contribution).
- 3. Further, infuence of the parameters has been studied by RSM technique. The presence of RM particles improves the surface characteristics due to increased lubricating effect of these particles at tool-work interface. It has also been noticed that an increase in cutting depth and feed rate degrades the surface characteristics of hybrid composites since the cutting force required to machine the surface is increased under these conditions.
- 4. The chip size changes from segmented type to spiral coil type with increase in the values of depth of cut and feed rate. Further, long and coil spring type chips are produced at relatively higher values of RM fraction in the hybrid composites due to the lubricating effect of the RM particles. SEM examination of chips

formed reveals that low values of cutting parameters and higher red-mud contents improve the surface characteristics of the hybrid composites.

- 5. The confrmation experiment indicates a deviation of 4% in the experimental and the predicted response. A minimum of 23% improvement in the surface quality of the composites is observed under optimum process conditions.
- 6. Overall, it has been revealed that the addition of RM (an industrial waste material) particles helps in improving the machinability of the hybrid composites under dry turning conditions. The results provide adequate information regarding the machining aspects of HAMCs, which can be used in various industrial applications.

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