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# **Biomechanics of Rotator Cuff Injury and Repair**

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# **11.1 Introduction**

Although the rotator cuff tears are more common in older individuals, this kind of pathology also frequently affects athletes and young workers engaged in repetitive overhead activities. The rotator cuff is a complex musculotendinous unit, which plays a major role in glenohumeral joint stability and mobilization. Injuries of the rotator cuff can lead to signifcant functional impairment, resulting in time loss from sport and competition, and, in the more advanced stages, in trouble in performing daily activities. Therefore, fully understand the biomechanical features of

rotator cuff tears and repair is crucial to better manage and address the injuries of rotator cuff. This chapter provide an overview of the normal and injured rotator cuff biomechanics, followed by literature evidence and considerations about the biomechanical concept of the rotator cuff repair.

# **11.2 Biomechanical Properties of the Rotator Cuf**

Rotator cuff is composed by the tendons of four muscles: the supraspinatus, the infraspinatus, the teres minor and the subscapularis. These muscles create compressive forces to stabilize the glenohumeral joint and generate torque to move the humerus [\[1](#page-9-0)]. In particular, the compressive and antagonistic forces of the subscapularis anteriorly and infraspinatus and teres minor posteriorly, imparts a compression on the humeral head into the glenoid, with a mechanism known as "concavity compression" [[2\]](#page-9-1) (Fig. [11.1\)](#page-1-0). This tendinous connection, with the addition of ligaments and bone factors, allows for the articular stability and, at same time, for the humeral motion with respect to the scapula, defning the role for tendons as specifc active restraints during the shoulder movement [[3\]](#page-9-2). The wide range of motion of glenohumeral joint is allowed by the variety of rotational moments of the cuff muscles, whose tendons insert continuously around

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**Fig. 11.1** Concavity compression mechanism. The compressive and antagonistic forces of the subscapularis anteriorly and infraspinatus and teres minor posteriorly, imparts a compression on the humeral head into the glenoid, with a mechanism known as "concavity compression"

the humeral head. The force and the torque that a muscle can generate vary with the position of the joint: at the extremes of the range of motion, the muscles of the rotator cuff are weaker, because they are fully contracted or extended, while the maximal force is in the midrange of their pretension [\[4](#page-9-3)]). The supraspinatus has a major role in humeral elevation at higher glenohumeral angles, while at lower angles the deltoid contribution is higher. The subscapularis and infraspinatus also play a role in abduction during internal and external humeral rotation [\[5](#page-9-4)]. During the arm motion, movements of the scapulothoracic joint are associated with those of glenohumeral joint, performing a complex and coordinated pattern of motions that Codman defned the "scapulohumeral rhythm" [\[6](#page-9-5)]: while under the 90° of humeral elevation scapular and clavicular motion are minimal, beyond the 90° there is upward rotation, posterior tilting and external rotation of the scapula to allow for the full range of motion in the upper extremity [\[7](#page-9-6)].

As in the shoulder there is not a fxed axis of rotation, the functions of the shoulder muscles must be balanced, working together to produce a net torque and neutralize opposed elements: the superior portion of the cuff and the deltoid neutralize the adduction of the latissimus dorsi during pure internal rotation, the posterior cuff and the posterior deltoid muscles neutralize the internal rotation moment of the anterior deltoid during forward elevation without rotation [[5\]](#page-9-4).

The tendons of the rotator cuff are subjected to complex tension loads. Compressive loads stress the cuff between the humeral head and the coracoacromial arch: in vivo subacromial pressure values of 8 mmHg at rest, 39 mmHg at 45° of fexion and 56 with the arm in elevated position with 1 Kg weight held in the hand were reported [\[8](#page-9-7)]. Concentric and eccentric tension loads are produced in abduction against resistance and in active resistance to downward respectively [\[8](#page-9-7)].

# **11.3 Biomechanics of Rotator Cuff Tears**

## **11.3.1 Mechanical Factors in Rotator Cuff Tears**

Rotator cuff tear aetiology is multifactorial: the role of extrinsic factors, which have been classically considered among the causes of rotator cuff tears, takes alongside to that of intrinsic factors, such as biologic degeneration and deficit of vascularisation [[3\]](#page-9-2). The extrinsic theory dominated the pathophysiology of the rotator cuff tears and the impingement syndrome for decades. In 1931, Meyer suggested that tears of the rotator cuff could develop secondary to attrition due to the friction between the rotator cuff and the under surface of the acromion [\[9](#page-9-8)]. In the 1972, Neer

introduced the theory of subacromial impingement, describing it as a mechanical phenomenon corresponding to impingement of the rotator cuff tendon beneath the anterior-inferior acromion [\[10\]](#page-9-9). Neer observed that this condition affected mainly the supraspinatus tendon insertion on the greater tuberosity, and that occurred when the shoulder was placed in forward fexion and external rotation. Moreover, he observed that this condition presupposed an anatomic irregularity of the acromion and the presence of bony spurs in the site of coracoacromial ligament insertion on the acromion [\[10](#page-9-9)]. The correlation between the acromial shape and the cuff disease was supported by subsequent cadaveric studies, in which a higher prevalence of full-thickness tears of the rotator cuff was noted in association with the hooked or type III acromion [\[11](#page-9-10), [12\]](#page-9-11). However, later, acromial impingement was found not to be the primary cause of rotator cuff tears [[3,](#page-9-2) [5,](#page-9-4) [13\]](#page-9-12): it resulted associated with changes on the bursal side of the rotator cuff tears which is less frequently affected than the intra-tendinous or articular side [[14\]](#page-9-13), and the acromioplasty procedures did not avoid the occurrence of rotator cuff tears, leading to damage of tendons in 20% of cases [[15](#page-9-14)]. Furthermore, the morphology of the acromion seemed to be

secondary to pathology of the bursal side of the cuff [[16,](#page-9-15) [17](#page-9-16)]: the cuff degeneration lead to produce an acromial hook, which results in a greater load on the coracoacromial arch producing traction spurs in the coracoacromial ligament [[18](#page-9-17), [19](#page-10-0)]. A contact between rotator cuff and the coracoacromial arch was also reported in normal shoulders in both cadaveric studies and healthy human subject, suggesting that the contact phenomenon between the coracoacromial arch and the rotator cuff was not a pathological but a physiological condition [\[20](#page-10-1), [21](#page-10-2)].

Further bone features has been associated with injuries of the rotator cuff; a glenohumeral joint with a higher acromial coverage index, which is the ratio between the distance from the glenoid plane to the acromion and the distance from the glenoid plane to the lateral aspect of the humeral head, is associated with an increased risk of rotator cuff tear [[22\]](#page-10-3). The angle between the line connecting the inferior border to the superior border of the glenoid fossa, and a second line connecting the inferior border of the glenoid fossa to the most inferolateral point of the acromion, represents the critical shoulder angle (CSA) (Fig. [11.2\)](#page-2-0). Since it combines the measurement of the glenoid inclination and the lateral extension of the acromion, CSA has been

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**Fig. 11.2** Radiologic parameters associated with rotator cuff pathology. The critical shoulder angle (**a**) and the acromial coverage index (**b**)

used to predict the presence of degenerative cuff tears [\[23](#page-10-4)]. In a biomechanical simulation model, a larger CSA has been shown to increase the supraspinatus tendon load at low degrees of abduction compared to a control with a normal CSA [\[24](#page-10-5)].

The mechanism of rotator cuff fatigue damage starts with isolated changes in microstructures and develops into severe matrix disruption and kinked deformation; this degeneration, in addition to biological changes due to aging and overuse, predispose the tendons to failure [\[3](#page-9-2)]. Studies of torn rotator cuff tendons have revealed that degenerative changes also appear medially from the tear, indicating the presence of degeneration before the tear occurs [\[25](#page-10-6), [26\]](#page-10-7). In particular, the critical zone of the rotator cuff, localized at 1 cm medially to the supraspinatus insertion in the tuberculus major, resulted to have a decreased vascularisation [\[27](#page-10-8)]. This feature, associated with increased local pressure during humeral elevation and abduction, may be related with the degeneration process, predisposing the tendons to failure [\[3](#page-9-2)].

In patients who require to achieve a large range of external rotation, such as throwers, defects of the deep surface of the rotator cuff are common. Among these patients, the mechanism of cuff injury is explained by the abutment of the edge of the glenoid against the under surface of the supraspinatus tendon at the extreme of the external rotation [[5\]](#page-9-4).

Rotator cuff tears typically start at the deep surface of the supraspinatus tendon, close to the long head of the biceps. This site is subject to greater loads, even at rest. The complex and coordinated actions of the rotator cuff muscles are coupled in a manner that produces increased strain on the surrounding tendons when a tear in one tendon occurs. For this reason, a tear of one tendon in the rotator cuff could potentially lead to an increased risk for injury in the remaining muscles, determining a pattern that induces the tear progression and extension [[28\]](#page-10-9). The loads are concentred at the margin of the tear, facilitating the extension of the defect. A tear of 60% of the tendon thickness increases of 23.8% the ten-

sile strain in the posterior tendon [\[29](#page-10-10)]. Tears of the articular side of the infraspinatus increase the strain in the middle and superior portions of the supraspinatus. Subsequently, the defects of supraspinatus propagate posteriorly through the reminder of the supraspinatus and the infraspinatus [\[5](#page-9-4)].

## **11.3.2 Biomechanical Efects of Rotator Cuf Tears**

Tears in the rotator cuff result in altered glenohumeral joint mechanics and are frequently associated with loss of strength and stability of the shoulder. However, clear evidence about the relationship between the tear features and the functional outcomes still lack. The superior translation of the humeral head represents the most important biomechanical consequence of the rotator cuff tears, and the main radiograph signs of massive cuff defciency. Large-to-massive tears may lead to rotator cuff tear arthropathy, which implies the development of progressive glenohumeral and acromiohumeral arthritis secondary to the tear, associated with joint pain and reduced humeral elevation [\[30](#page-10-11), [31](#page-10-12)].

When the dynamic function of rotator cuff is compromised by a tear, the external rotation and the elevation are primarily decreased. Burkhart introduced the concept of the rotator cuff cable [\[32](#page-10-13)], a thickened area of the rotator cuff tendon which inserts anteriorly between the anterior insertion of the supraspinatus and superior half insertion of subscapularis, and posteriorly near the inferior insertion of infraspinatus tendon. Burkhart noted that rotator cuff tears that did not involve the cable, such as supraspinatus tears alone, were functional and biomechanically intact, because the cable remained intact [\[33](#page-10-14)].

Regarding the abduction torque, the features of rotator cuff tears which could affect the force transmission are the supraspinatus tendon detachment and the retraction of its muscle. In a cadaveric study [[34](#page-10-15)] the effect of different size and shape of the rotator cuff tear on in vitro force transmission was investigated,

comparing different size of supraspinatus tendon detachment with a defect of tendon substance and muscle retraction: authors reported that only after detachment of the entire width of the supraspinatus tendon, the transmitted force signifcantly decreased; this fnding support the concept of rotator cable, pointing out that the muscle forces are effectively transmitted by the rotator cuff as long as the rotator cable is intact. Furthermore, in this cadaveric study, the simulated muscle retraction resulted in signifcantly greater decrease in transmitted force compared with the isolated detachment of the tendon, showing that rotator cuff muscle retraction contributes substantially to loss of shoulder strength following large rotator cuff ruptures [[34](#page-10-15)].

In order to gain more insight in the effect of rotator cuff tear in shoulder biomechanics, the kinematics of the joint with a defect of the cuff was analysed in literature. In particular, the assessment of humeral head position, external humeral rotation, humeral abduction and associated scapulothoracic rotations were investigated, and the fndings showed that the shoulder kinematics is associated with rotator cuff tear size [[35–](#page-10-16)[37\]](#page-10-17): while isolated tears of supraspinatus had no significant biomechanics consequences, massive cuff tears involving supraspinatus or subscapularis altered signifcantly the kinematics of the shoulder. In a cadaveric study [\[36](#page-10-18)] in which fve shoulder specimens were subjected to different loading conditions with sequentially larger anterosuperior cuff tears, a signifcant increase in anterior-superior and superior translation resulted only after that the anterosuperior tears were extended to the superior half of the subscapularis. No signifcant biomechanical consequences, in contrast, were reported after isolated tears of supraspinatus. These results support the rotator cuff cable concept, suggesting that the preservation or the loss of the anterior cable attachment represents an important determinant of the biomechanics of anterosuperior rotator cuff tears [[36\]](#page-10-18). In line with these fndings, in another cadaveric study, in which the effect of 1 and 3 cm isolated supraspinatus tears on joint kinematics was examined, no signifcant changes were founded in glenohumeral translation [\[38](#page-10-19)].

Regarding the position of humeral head along the superior-inferior and anterior-posterior axis during scapular plane abduction in shoulder with rotator cuff tears, superior migration of humeral head, when the superior shear forces created by the deltoid are no longer effectively opposed, was described in studies employed in vitro static evaluation techniques [\[39](#page-10-20), [40](#page-10-21)] (Fig. [11.3](#page-5-0)).

In a dynamic in vivo study, on the other hand, an inferior dynamic translation was founded during scapular plane humeral abduction [[41\]](#page-10-22). During an in vitro simulation of active shoulder kinematics, the effect of three sequential simulated tears affecting the supraspinatus and the subscapularis during the unconstrained glenohumeral abduction was provided [\[35](#page-10-16)]: authors founded that, as the size of the simulated cuff tear increased, the plane of elevation became signifcantly more posterior at all angles of abduction, and the position of humeral head became more anterior for angle of abduction greater than 50°. No differences, on the other hand, were founded regarding the position of humeral head along the superior-inferior axis [\[35](#page-10-16)]. In an in vivo study in which a 3D to 2D model-toimage registration techniques was provided [[42\]](#page-10-23), a more anterior position of the humeral head centre was founded in shoulder with large-tomassive full-thickness rotator cuff tear than in controls, at internal rotation position during dynamic axial rotation in adducted position. Moreover, authors reported a more medial position of humeral head in patients with rotator cuff tear than in controls at the late phase of dynamic scapular plane abduction [\[42](#page-10-23)]. A recent in vivo three-dimensional bone model of ten shoulders with massive rotator cuff tears showed a significantly higher humeral head position under the 40° of abduction angle than the normal contralateral shoulder [[43\]](#page-10-24).

Regarding the associated scapular kinematics, Authors of the latter study reported a signifcant increase of scapular upward rotation in the initial position at 20° of humeral abduction and at the

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**Fig. 11.3** Humeral head position in shoulder with rotator cuff tear. Rotator cuff tear resulted in superior migration of humeral head among cadaveric static evaluations. (**a**): normal cuff; (**b**): injured cuff

fnal elevation, over 130° of humeral abduction in shoulders with rotator cuff tears [[43\]](#page-10-24). In another kinematics study, the comparison between patients with massive posterior-superior rotator cuff tear and patients with subacromial pain syndrome associated with intact rotator cuff showed a lower humero-thoracic abduction and forward fexion, associated with a marked increase in scapular upward rotation in the rotator cuff injured group [\[37](#page-10-17)]. Furthermore, decline in humeral abduction and increase in scapular upward rotation were founded in simulated massive posterior-superior rotator cuff tear created after a suprascapular nerve block in healthy volunteers [\[44](#page-10-25)]. These results about the posterosuperior massive tears, since the infraspinatus muscle has a direct impact on the glenohumeral joint and does not directly control scapula-thorax motion, suggested that the increased scapular upward rotation (i.e. scapulo-thorax lateral rota-

tion) should be compensatory in nature [\[37](#page-10-17), [44](#page-10-25)] (Fig. [11.4](#page-6-0)).

# **11.4 Biomechanics of Rotator Cuff Repair**

The rotator cuff repair must aim to fully restore the anatomy and function of the rotator cuff tendons.

Regarding isolated supraspinatus lesion, the biomechanical effect of repair was seen by Yu et al. [[45\]](#page-10-26) only at 10° abduction with 60 N loading with an increase in percent inferior force after repair that may represent greater concavity compression and spacer effect, which are both important functions of the supraspinatus. This same increase was not observed with the deltoid loaded to 90 N, which could be a function of the effect of loading producing an offset between the inferior

<span id="page-6-0"></span>

**Fig. 11.4** Scapular associated kinematics in rotator cuff tears. In vivo kinematics studies reported increase in scapular upward rotation (scapula-thorax lateral rotation)

associated with a decreased humeral abduction in shoulders with postero-superior massive rotator cuff tears. **a**: normal cuff; **b**: injured cuff

and superior forces. No changes were seen in the contact area, pressure, or position after repair, suggesting that repair of full-thickness rotator cuff tears does not completely recreate normal glenohumeral biomechanics or that no change existed in the pathologic tear specimens from normal.

By the way, when a tear is large, it may sometimes be diffcult to bring the torn edges back to the original insertion site of the greater tuberosity. In those cases, a medial shift of the insertion site of the cuff tendon is one of the surgical options. According to biomechanical studies by Yamamoto and those by Liu et al., a medial shift of 17 mm or more should be avoided from the functional point of view because it reduces both the moment arm and the range of shoulder motion [\[46](#page-10-27), [47](#page-10-28)].

Several biomechanical studies investigated the effect of different angles anchor insertion and inclination in rotator cuff repair, with the aim to achieve greater pullout strength possible. In 1995 Burkhart introduced the deadman theory [[48\]](#page-11-0), suggesting that an anchor inserted at 45° may show the greatest pullout strength theoretically. However, biomechanical pullout studies, have shown that anchors inserted at 90°, 135° or between 105° and 135° present the greatest pullout strength [\[49](#page-11-1)[–51](#page-11-2)], advancing that the deadman theory depends on the friction of the anchors. In a review associated with additional biomechanical studies, Itoi et al. [[52\]](#page-11-3) reported that the insertion angle of 90° is the strongest for a threated anchor. Furthermore, authors of this latter study

<span id="page-6-1"></span>

**Fig. 11.5** Effect of different angle insertion of suture threated anchors in rotator cuff repair. In order to achieve the best performance of suture threated anchor with strong friction, surgeons must insert the anchor close to the line of pull

showed that the pullout strength depends on the inclination of the anchor, friction of the anchor– bone interface and quality of bone. In particular, the insertion angle of the suture threated anchor should replicate the angle of applied load to ensure the optimum pullout strength [[52\]](#page-11-3). (Fig. [11.5](#page-6-1)).

Regarding the rows of the anchor, there are single, double and triple row repair described, with associated different types of stiches confguration. In a cadaveric study, in which a simple single-row repair construct and a linked single-row construct were compared, no significant differences in ultimate load to failure and resistance to gap formation between the simple and the linked single-row construct were founded [[53](#page-11-4)].

Many biomechanical studies have already clarifed that the use of transosseous equivalent repair for rotator cuff repair was superior to other techniques such as the single- or dual-row technique in terms of contact area or pressure between the rotator cuff tendon and the footprint, and the initial pullout strength [[54](#page-11-5)[–57](#page-11-6)]. Using the transosseous equivalent technique, a greater initial fxation strength may be achieved. However, the tendon itself is inherently elastic. Fixing the torn tendon with the transosseous equivalent repair technique, the tendon may lose its inherent elasticity due to the crossover of the strong sutures. The initial strong fxation is needed to avoid pullout failure after surgery. However, the fxation is required only for the frst few months. Yamamoto et al. [\[57](#page-11-6)] demonstrated that the rotator cuff tendon became stiffer after arthroscopic rotator cuff repair, especially transosseous equivalent repair, by measuring the strain of the supraspinatus tendon using ultrasound elastography. Results showed that the superficial layer of the supraspinatus tendon was stiffer after transosseous equivalent repair than the contralateral side at the fnal follow up [[57\]](#page-11-6). In addition, their study revealed that a high-stress concentration was observed around the insertion sites of the medial row threads.

The tying of the medial knots during transosseous equivalent repair is controversial. There are several biomechanical reports demonstrating biomechanical improvement (ultimate load, contact pressure, and stiffness) by tying the medial row of a transosseous equivalent repair [\[58](#page-11-7), [59\]](#page-11-8). Tamboli et al. [\[60](#page-11-9)] investigated the effects of bite-size horizontal mattress stitch: whereas a 4-mm bite fxed the tendon more tightly but at the cost of decreased ultimate strength, a 10-mm bite conveyed greater ultimate strength but with increased gap and strain. Authors concluded that for transosseous equivalent repair, large stitches are benefcial because the repaired tendon has a higher strength, and the slightly mobile medial knot can be tightened by lateral fxation.

Anatomic and biomechanical cadaveric studies highlighted the structural and functional relationship between superior shoulder capsule and the articular side of rotator cuff suggesting that articular-sided partial-thickness tears include detachment of the superior shoulder capsule from the greater tuberosity  $[61, 62]$  $[61, 62]$  $[61, 62]$ . In a cadaveric study a signifcant increase of anterior and inferior glenohumeral translation was founded after that a tear of superior capsule was performed, compared with the intact capsule state [[62\]](#page-11-11). Satisfactory results were reported about the repair procedure to manage articular-sided partialthickness rotator cuff tear [\[63,](#page-11-12) [64\]](#page-11-13). In a cadaveric analysis of the effect of an articular-sided partial supraspinatus and infraspinatus tear during the simulated late-cocking and acceleration phases of throwing, no signifcant differences in humeral head apex position, internal impingement area or glenohumeral contact pressure were reported compared with the intact condition [\[65](#page-11-14)]. In the same study, authors performed a transtendon repair with two anchors providing a signifcant decrease of external humeral rotation, posterior shift of humeral apex position, decrease of glenohumeral contact pressure at maximum external rotation and decrease of internal impingement area compared with the intact and the torn status during both the two phases of throwing. These results suggested that transtendon repair of an articular-sided partial supraspinatus tear may cause overtightening of the torn tendon and superior capsule, minimizing secondary subacromial and interior impingement, and that careful evaluation of patient individual shoulder laxity should be assessed when the transtendon repair is chosen for address an articular-sided partial tear [\[65](#page-11-14)].

#### **11.4.1 Irreparable Tears**

Rotator cuff tears are defned as irreparable when the lesions cannot be repaired primarily to their insertion on the tuberosities with conventional techniques of surgical release/mobilization, because of their size, retraction, and muscle impairment caused by atrophy and fatty infltration  $[66]$  $[66]$ .

With the aim to better address the massive irreparable rotator cuff tears, Burkhart et al. [\[33](#page-10-14)] introduced the concept of the "suspension bridge" which lead to the development of the functional partial repair: the repair of the whole subscapularis and the inferior half of infraspinatus, without the complete coverage of the defect, can restore the normal shoulder mechanics, recovering the transverse force couples and a stable fulcrum for glenohumeral kinematics [[66\]](#page-11-15).

Several biomechanical studies investigated the infuence of the superior capsule reconstruction on the superior stability of the shoulder joint. Superior capsular reconstruction (SCR) potentially improves function by re-centering the humeral head and improving glenohumeral kine-matics [[67\]](#page-11-16).

Several techniques for performing superior capsule reconstruction have been described, characterized by different type of the graft (fascia lata, extracellular matrix dermal grafts, long head of biceps and tendon allografts), whether performed in an open manner or arthroscopically, the mode of the glenoid and greater tuberosity fxation, and whether the anchors are all inserted before or after passage of the graft [\[67–](#page-11-16)[73\]](#page-11-17).

In a cadaveric study involving eight shoulders, Mihata et al. [[74\]](#page-11-18) compared the superior translations of the proximal humerus in fve conditions: intact rotator cuff, excised supraspinatus, reconstructed supraspinatus using a bridging graft connecting the remnant of the supraspinatus to the greater tuberosity, reconstructed superior capsule with graft attached to the glenoid and the greater tuberosity, reconstructed superior capsule and supraspinatus with the patch [\[74](#page-11-18)]. They demonstrated that excising the supraspinatus tendon resulted in a signifcant increase in the superior translation of the proximal humerus, which was fully restored only when the superior capsule was reconstructed with the graft [\[74](#page-11-18)]. Supraspinatus reconstruction with the graft only resulted in a partial restoration of superior translation [[74\]](#page-11-18). In another biomechanical study, Mihata et al. demonstrated an 8 mm thick fascia lata graft resulted in a greater superior stability than a 4 mm thick graft [[75\]](#page-11-19). A signifcant decrease in superior translation was only witnessed with 8 mm thick graft as compared to the 4 mm thick graft [[75\]](#page-11-19).

When performing SCR, it was also reported that addition of posterior side-to-side suturing between the graft and residual infraspinatus tendon increases the superior stability of the proximal humerus [[76\]](#page-11-20). In a biomechanical study, SCR without posterior side-to-side suturing, did not inhibit glenohumeral superior translation, whereas addition of posterior side-to-side suturing resulted in signifcantly reduced superior translation [\[76](#page-11-20)].

The superior rotator cuff and superior capsule reconstruction technique using long head of biceps (LHB) was also proposed and described in literature. In a biomechanical study by Han et al. the superior capsule reconstruction using LHB permitted to reduced humeral head translation and subacromial contact pressure [[77\]](#page-12-0). Moreover, Authors did not fnd signifcant differences between the isolated SCR using LHB procedure and the side-to-side repair augmentation associated procedure [[77\]](#page-12-0).

Recently, performing acromioplasty with a rotator cuff repair has become a subject of controversy. There have been some clinical reports describing the excellent outcome after cuff repair without acromioplasty [[78,](#page-12-1) [79\]](#page-12-2). According to the 2011 guidelines published by the American Academy of Orthopaedic Surgeons, [[80\]](#page-12-3) the routine acromioplasty is not required at the time of rotator cuff repair. A biomechanical study by Denard et al. [[81\]](#page-12-4) demonstrated that a limited acromioplasty, of 3 mm in thickness, might be enough for decompression while preserving the coracoacromial ligament. Because of variations in the distance between the undersurface of the acromion and the cuff surface, the level of acromioplasty should be decided during surgery on a patient specifc level.

Although the results of routinely acromioplastic are controversial, Mihata et al., investigating the effects of acromioplasty on shoulder biomechanics associated with superior capsule reconstruction [\[82](#page-12-5)], illustrated that adding acromioplasty to SCR with fascia lata signifcantly decreased the subacromial peak contact area compared to SCR without acromioplasty, without altering the humeral head position, superior translation or subacromial peak contact pressure [[82\]](#page-12-5). Based on their fndings the authors suggested that when performing SCR, acromioplasty may help to decrease the postoperative risk of abrasion and tearing of the graft beneath the acromion, without increasing the risk of superior translation [\[82](#page-12-5)].

To treat the irreparable rotator cuff tears the subacromial balloon spacers have been proposed. There is limited biomechanical literature on the subacromial balloon spacer and its ability to manage irreparable rotator cuff tears. Literature is also lacking on the appropriate infation volumes.

The biomechanical study by Singh et al. [\[83](#page-12-6)] found out that the 25-mL balloon displaced the humeral head more inferior than the intact condition with a mean difference statistically signifcant, but it is not likely clinically signifcant. Their study has some limitations and they only tested static abduction.

#### **11.5 Conclusions**

The rotator cuff tears modify shoulder biomechanics radically. Rotator cuff repair allows to restore biomechanics in order to address the clinical impairment. If the tear is not completely reparable, adding superior capsule reconstruction to partial cuff repair could be a good option for young and active patient without rotator cuff tear arthropathy, with the aim to restore the native shoulder biomechanics.

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