

Development of New Precursors for One-Part Alkali-Activated Geopolymer Using Industrial Wastes



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Abstract Conventional two-part alkali activation has many drawbacks: the hazardous activating solution, which makes it less friendly to handle and the absence in long-term availability of its main precursors such as fly ash and ground granulated furnace slag. This research aimed to develop a one-part alkali-activated cement, which is free of chemical solutions. A blend of alumina-silicate rich materials with adequate alkaline content to minimise the limitations associated with the current (AAC) relating to source materials was utilised. At the same time, applying alternative activation methods such as thermo-mechanical activation, alkali-thermal activation or thermo-chemical activation of new (AAC) precursors were investigated. Materials were analysed in terms of their physical, chemical and metallurgical properties to understand the changes after thermal activation. Enhanced compressive strength was recorded from individual thermal activation of the materials at 450 °C and 950 °C.

Keywords One-part geopolymer · Alkali activation · Thermal activation

1 Introduction

Recently, Alkali-Activated Cement (AAC) or geopolymer cement has attracted global considerations for its high engineering and mechanical properties. Conventional two-part AAC is produced by activating solid alumina-silicate sources with alkali metal (Na or K) or alkaline earth (Ca or Mg) hydroxide or silicate solution from a sequence of dissolution–reorientation–solidification reactions [1, 2]. However, this process of manufacturing has many drawbacks including chemical handling difficulties and hazards from these solutions which in terms of rising impracticality of using these novel materials for in situ applications. Therefore the need for

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one-part dry AAC that just needs water to create a binding material started to be very significant [3]. This means that AAC can be similar to OPC but with exceptional engineering and ecological properties. One-part AAC can be synthesised by providing sources of (alkali+silicate+aluminate) as solid powder form with utilising various assisted activation methods such as thermal (calcination), mechanical (grinding) or combination of both methods. A wide range of alumina-silicate materials can be incorporated in the process including (natural and artificial) pozzolans and industrial (by-products and wastes). Sturm, Gluth [4] synthesised one-part Geopolymer mix by mixing calcined (600 °C) Rice Husk Ash and solid sodium aluminate which was considered as an activator in the system as it is easy to dissolve on water. Therefore, water just added to the binder with a water/binder ratio 0.5. The samples were cured in open moulds for an 80 °C to increase the reactivity of the mixtures. The obtained compressive strength was 30 Mpa after one day curing. Alkaline source can be either (Na, K or Ca, Mg), however, past studies proved that using CaO or Ca (OH)₂ can be alternative activators as these sources are cheaper than (NaOH or KOH) [5, 6]. Kim, Jun [6] used synthetic commercial CaO solid powder to create cement-free binder with ground granulated blast furnace slag as Si/Al source material. After comparing with Ca (OH)₂, CaO activator was discovered to present developed mechanical properties with 53 MPa strength of 56 days because of the fabrication of additional C-S-H than Ca (OH)₂.

In this research, attempts were targeting towards synthesising a dry one-part AAC utilising a waste material from quick lime production which is mostly rich in alkaline source (CaO) instead of the commercial synthetic CaO chemical powder which was used by past studies. This lime waste (LW) is used to activate the source of alumina-silicate (Al/Si) materials offered by a blend of metakaolin (MK) and a natural pozzolan material from volcanic tuff (NP).

2 Materials and Experimental Work

2.1 Material Characterisation

Initially, all materials were assessed and characterised to evaluate their chemical and physical properties. Table 1 shows the physical properties of materials including specific surface area, alkalinity and density. MK and NP having higher surface area

Table 1 Physical properties of undisturbed materials

Material	Specific surface area (Blaine) (m ² /g)	pH	Density (g/cm ³)
MK	19.6	6	2.69
NP	17.2	6	2.57
LW	10.1	12.3	2.7

than LW which has high alkalinity with pH of 12.3 is favourable for alkalination of MK and NP. The specific surface area was determined by Blaine Air Permeability Apparatus according to the British standard (EN 196-6). Mineralogy of materials was evaluated by X-Ray Diffraction (XRD) and Thermogravimetric analysis (TGA) methods. XRD has been conducted for undisturbed materials and after calcination with two levels 450 °C and 950 °C.

Particle size distribution (PSD) was determined by a laser diffraction particle size analyzer as displayed in Table 2. MK and NP were nearly similar with (D_{50}) is 7.88 and 9.68 μm , respectively. Conversely, LW was coarser with D_{50} 15.9 μm .

All materials were provided by local suppliers in the UK. Materials were characterised chemically to determine their composition by using X-Ray fluorescence (XRF) as shown in Table 3. MK and NP are mostly composed of SiO_2 and Al_2O_3 with fewer amounts of CaO , Na_2O , K_2O and MgO in NP. In contrast, LW is mostly rich in CaO of 80.1 Wt. % with small amounts of SiO_2 and Na_2O .

Table 2 Particle size distribution (PSD) of starting materials

	Amount (%)	Mean (μm)	Median (μm)	S.D (μm)	C.V	d10 (μm)	d50 (μm)	d90 (μm)
LW	100	23.6	15.9	22.1	93.70%	0.965	15.9	59.6
MK	100	13.9	7.88	15.2	110%	1.2	7.88	38
NP	100	15.1	9.68	14.5	95.70%	0.972	9.68	39
(Average)	100	17.5	11.2	17.3	99.60%	1.05	11.2	45.5
(C.V.)	0.00%	30.20%	37.90%	24.50%	8.70%	12.80%	37.90%	26.80%
(Maximum)	100	23.6	15.9	22.1	110%	1.2	15.9	59.6
(Minimum)	100	13.9	7.88	14.5	93.70%	0.965	7.88	38

Table 3 Chemical composition of undisturbed materials by XRF

Component	MK	NP	LW
SiO_2	46.2	46.6	14.6
Al_2O_3	33	18.6	0.27
Fe_2O_3	0.9	3.8	0.1
CaO	0.3	4.5	80.1
Na_2O	0.9	3.9	1.8
K_2O	0.4	6	0.5
MgO	0.1	4.2	0.6
TiO_2	1.6	0.6	0.1

Table 4 Mixing proportions of blends

Mix ID	Binder contents	Calcined constituent
M1	35%MK 35%LW 30%NP	NP
M2	35%MK 35%LW 30%NP	MK
M3	35%MK 35%LW 30%NP	LW
M4	35%MK 35%LW 30%NP	NP, MK, LW

2.2 Tests Preparation and Procedures

The mixing method was followed consistent with the requirements of (BS EN 196-1:2016). Water/binder ratio w/b was fixed of 0.45 for all the mortars after exploring the appropriate w/b for the selected materials. Primarily, 0.55 ratio was chosen but it was found that the mortars were very workable. Consequently, it was decreased to 0.45 and mortars with suitable uniformity was attained at this stage. Mortars were mixed using sand passing through 2.0 mm BS sieve with a specific gravity of 2.62 with mixing ratio (1:2). The mortars were mixed using Hobart mixer and cast in steel moulds of prisms with (40 mm × 40 mm × 160 mm). Mortars were blended in ternary procedure with magnitudes as shown underneath in Table 4. The mortars were cured in hot water curing regime to improve the reactivity and the hydration rate of the mortars and to avoid possible problems such as efflorescence and micro-cracking at this stage which can lead to a reduction in compressive strength [7]. The curing temperature was fixed to 50 °C for 7 days and then cured in normal 20 °C water until 28 days. This curing procedure was selected based on past reports and studies that proved the best curing temperatures for alkali-activated cement [8, 9].

The calcination of materials in muffle furnace was individually to assess the influence of each material on the mixture's properties. Two levels of calcination were based (950 and 450 °C) for 2 h with 20 °C/min calcining rate. Calcination temperatures were chosen depending on the characterisation (XRD & TGA) results which presented that most phase's changes take place at these levels.

3 Results and Discussions

3.1 Mineralogical Analysis

It is noticeable from the diffractions of MK in Fig. 1 that MK encompasses of minerals comprising kaolinite and quartz in main phases. Minor phases involve mullite, anatas and illite. Noteworthy decrease and even disappearance of kaolinite and quartz peaks were noted after both levels of calcination indicating semi-transformation of material to an amorphous phase.

In Fig. 2, XRD spectrums of NP which shows vast transformation of crystalline to

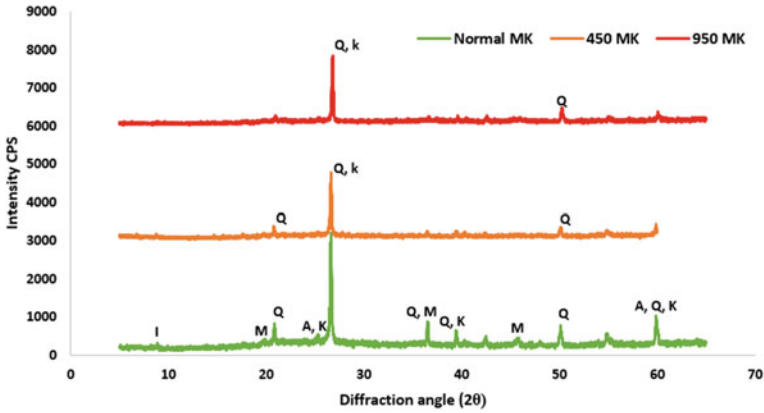


Fig. 1 XRD of MK before and after calcination. Q: Quartz (SiO_2), K: kaolinite ($\text{Al}_2\text{Si}_2\text{O}_5(\text{OH})_4$), M: Mullite $\text{Al}_6\text{Si}_2\text{O}_{13}$, A: Anatas (TiO_2), I: Illite ($\text{K,H}_3\text{O}(\text{Al,Mg,Fe})_2(\text{Si,Al})_4\text{O}_{10}[(\text{OH})_2,(\text{H}_2\text{O})]$)

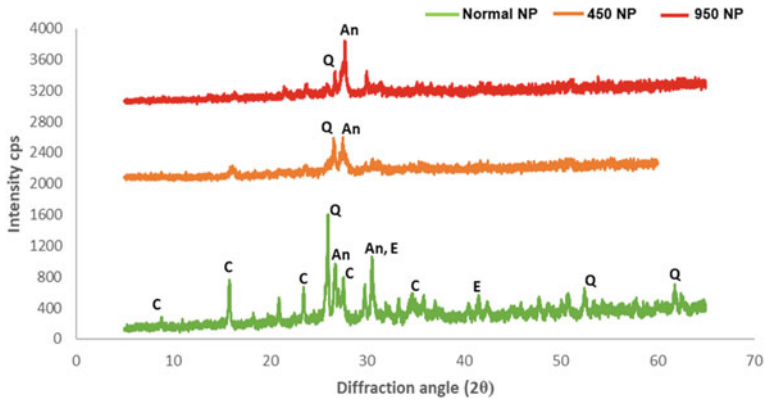


Fig. 2 XRD of NP before and after calcination. Q: Quartz (SiO_2), C: Clinoptilolite ($\text{KNa}_2\text{Ca}_2(\text{SiO}_{29}\text{Al}_7)\text{O}_{72}\cdot 24\text{H}_2\text{O}$), An: Anorthite ($\text{CaAl}_2\text{Si}_2\text{O}_8$), E: Edenite ($\text{Ca}_2\text{NaMg}_5(\text{AlSi}_7)\text{O}_{22}(\text{OH})_2$)

amorphous phases through the loss of Clinoptilolite and Anorthite peaks. Moreover, substantial decreasing in crystalline quartz at 950 °C calcination level.

Figure 3 displays the diffraction patterns of LW which can be seen clearly that the strong crystalline diffraction peak of lime (CaO) in LW was reduced significantly when calcined to 450 °C and entirely disappeared in 950 °C calcination. The presence of new diffraction peaks at new angles of calcined LW at 950 °C representing the formulation of new compounds but composed of same elements of undisturbed LW (CaO, SiO_2 and Na_2O) in form of wollastonite minerals [10, 11].

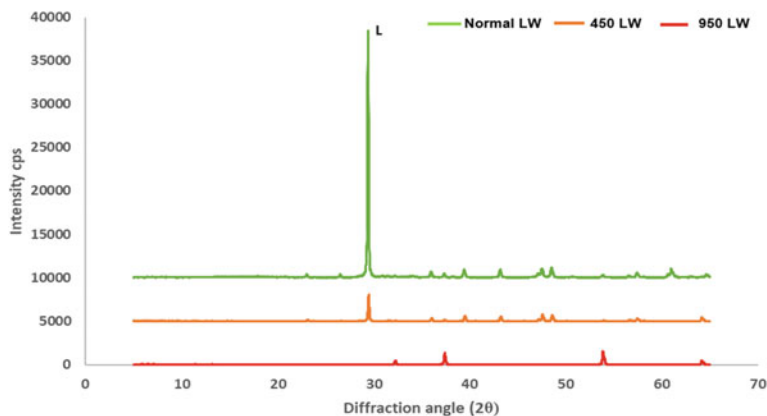


Fig. 3 XRD of LW before and after calcination. L: Lime (CaO)

3.2 Thermogravimetric Analysis (TGA)

TG-DTA thermal analysis was used to assess the thermal behaviour of raw materials when calcined to higher temperatures up to 900 °C. Figure 4a displays mass loss of NP up to 7% from initial weight when calcined from room temperature to 900 °C. While DTA curve is indicating exothermic concavity at 250 °C tailed by an endothermic drop in the curve reaching around 450 °C representing a start of phase's conversion process at this temperature. DTA curve of MK has revealed minor phase change about 700 °C as in Fig. 4b. Weight loss of LW started to drop intensely at 620 °C with 35% from the original weight with an intense and severe exothermic peak of DTA curve as demonstrated in Fig. 4c. This peak accredited to the disappearance of (CaO) crystalline peak in XRD of calcined LW.

3.3 Compressive Strength

Figure 5 shows compressive strength of mortars after individual calcination for 950 °C. A higher strength was gained from M3 that consists of calcined LW with 27.3 MPa in 28 days. This strength is attributed to the large transformation to vitreous mineralogy and disappearance of crystalline CaO peak because of calcination to 950 °C. Reduced dissolution of alumina-silicate compounds from NP and MK due to high amounts of amorphous compounds and lesser amounts of CaO when all materials calcined led to a fall of strength in M4.

Both XRD and TG-DTA results have shown that changes in phases of this ternary blend components starting in temperatures ranging from 350–500 °C. Hence, blends were mixed after calcination of 450 °C with the same method of proportioning that is mentioned in Table 4. Noticeably as shown in Fig. 6, comparative strength was

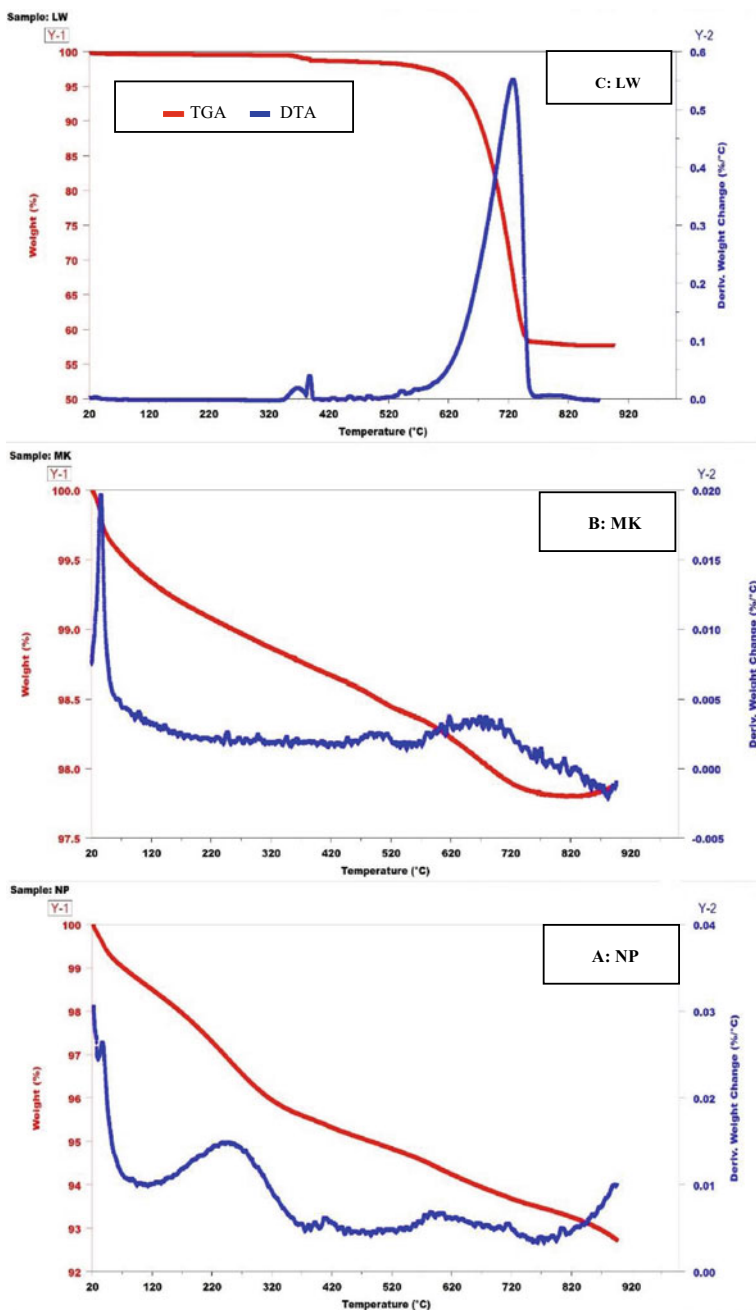


Fig. 4 TG-DTA analysis of A: NP, B: MK, C: LW

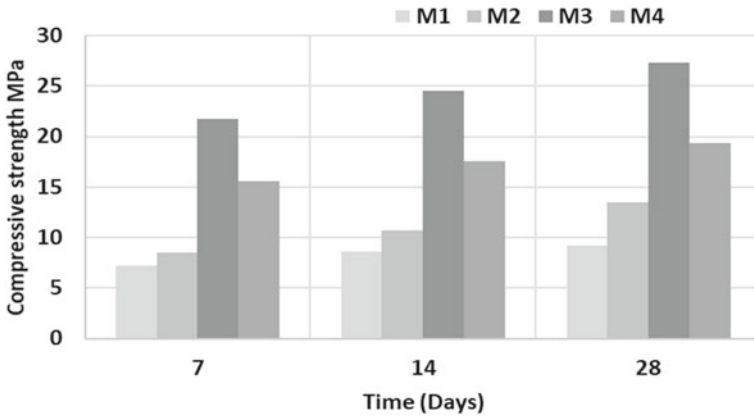


Fig. 5 Compressive strength after 950 °C calcination

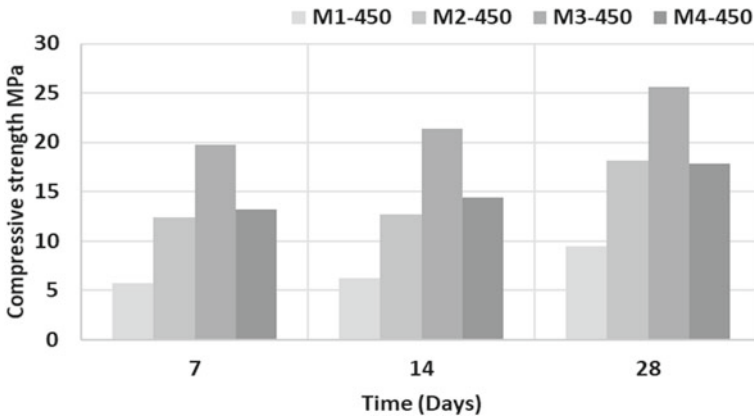


Fig. 6 Compressive strength after 450 °C calcination

obtained at this level of calcination with developed strength reached for 25.6 MPa at 28 d for M3-450 that has LW of 35%. This comparable growth of strength is attributed to mineralogical and chemical variations that were remarked in both XRD and DT-TGA results which designated that most diffraction patterns were starting to convert before and around 450 °C.

4 Conclusions

- Calcination was chosen assisted thermal activation for producing one-part AAC from a combination of alkali alumina-silicate materials. Calcination of materials

was conducted to 450 and 950 °C individually to assess the contribution of each material.

- Raw materials were characterised physically and chemically. Mineralogy and thermal behaviour and change due to calcination were assessed.
- Maximum compressive strength was recorded of 27.3 MPa in 28 d for mortar containing calcined (LW) of 950 °C. Relative compressive strength was gained at 450 °C calcination level demonstrating that reactivity of materials started to increase at this temperature.
- This strong growth was attributed to the massive conversion of LW mineralogy to be amorphous which initiated by calcination which was considered as an assisted activation factor.
- The outcomes of the study have shown that lime waste (LW) has high probability to be solid alkaline activator if treated correctly and its impurities are removed.

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