Chapter 16 Hemodynamic Aspects of Vessel Wall Imaging: 4D Flow



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Introduction

Cardiovascular MRI has undergone substantial developments over the last decades and offers capabilities for evaluating cardiac anatomy and function including the assessment of vascular anatomy and blood flow dynamic. Phase contrast (PC) MRI can be used to measure and quantify pulsatile blood flow in the human vascular system.

The basic principle has already been introduced by Carr and Purcell in 1954 who reported the observation of coherent motion on the MR signal [1] and by Hahn in 1960 who proposed to use nuclear precession to measure the velocity of sea water by means of phase shifts produced by magnetic field gradients [2]. Two decades later, Grant and Back were among the first to investigate the possibility of measuring flow velocity with MRI [3]. They called the technique "NMR rheotomography" and were visionary by remarking that "rheotomography may prove to be particularly useful for the noninvasive diagnosis of cardiovascular defects." Nearly 40 years later, many groups worldwide are using MRI flow measurements for the noninvasive diagnosis of cardiovascular defects. The first in vivo velocity map images and applications were reported in the early 1980s [4–7]. The initial measurement of a through-plane velocity profile in a two-dimensional (2D) slice of water flowing

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through a glass U-tube has evolved, and 2D and time-resolved (ECG-gated "CINE" imaging) PC-MRI has become available on all modern MR systems and is an integral part of clinical protocols assessing blood flow in the heart and large vessels [8–10]. More recently, the combination of CINE PC-MRI with three-dimensional (3D) spatial encoding and three-directional velocity encoding (termed "4D flow MRI") has made possible measurements of 3D blood flow dynamics in a 3D volume and over time (4D = 3D + time) [11–13].

This chapter will review the journey from simple 2D to 4D flow MRI for the advanced quantification and visualization of hemodynamic measures in vessel wall disease. We will describe the fundamental concepts of 4D flow MRI in terms of acquisition, data processing, as well as its applications to the assessment of altered blood flow dynamics in vascular diseases. A special emphasis is on the potential of 4D flow MRI to quantify important characteristics of the vessel wall such as wall shear stress (WSS) or pulse wave velocity (PWV). The chapter will conclude with a discussion of the current role of 4D flow MRI and future directions.

Background

From 2D to 4D Flow Image Acquisition

Flow imaging with MRI is based on the phase contrast (PC) technique, which enables the acquisition of spatially registered information on blood flow velocities simultaneously with morphological data within a single MRI measurement. In current clinical routine, PC-MRI is typically accomplished using methods that resolve two spatial dimensions (2D) in individual slices and encode a single time-resolved component of velocity directed perpendicularly to the 2D slice (through-plane velocity encoding). This approach allows measurements of forward, regurgitant, and shunt flows in congenital and acquired heart disease. In MRI, magnetic field gradient coils can create linearly varying magnetic fields along all three spatial dimensions on top of the main (static) magnetic field B₀. These magnetic field gradients cause spatially varying phase shifts of the source of the MRI signal (¹H proton spins in the human body) depending on the location of the source along the gradient. Spins that move along the direction of the gradient, e.g., flowing blood, acquire a different phase shift than the spins in adjacent static tissue [14].

The phase shift of the static media can be nulled by applying a magnetic field gradient with opposite polarity, whereas a phase shift for the moving spins will accumulate. The combination of both gradients is called a bipolar gradient [4] (see Fig. 16.1).

Using appropriate bipolar velocity encoding gradients, flow-dependent phase changes can be measured by playing out two acquisitions with different velocity dependent signal phase but otherwise identical sequence parameters. Subtraction of the two resulting phase images (i.e., calculation of phase difference images) allows



for the removal of the unknown background phase and calculation of velocity images [9].

With a bipolar gradient applied to the main direction of the blood flow, singledirection (e.g., through-plane) blood flow velocity is measured. Bipolar gradients can also be subsequently applied to two or three orthogonal axes to resolved blood flow velocities in two or three dimensions [15, 16].

To measure temporally resolved pulsatile blood flow velocities, a time-resolved (CINE) measurement can be performed [17, 18]. As illustrated in Fig. 16.2, PC-MRI data acquisition is split over multiple heartbeats, and data acquisition is gated to the cardiac cycle using the ECG signal (e.g., the R-wave) or a pulse oximeter reading. A series of time-resolved (CINE) images is collected representing the dynamics of the pulsatile blood flow during the cardiac cycle. Usually, one-directional ("through-plane") velocity encoding along the predominant blood flow direction is used to quantify blood flow in the heart, through cardiac valves, and in arteries and veins throughout the body. Typical 2D CINE PC-MRI images are illustrated in Fig. 16.2.

For over three decades, 2D CINE PC-MRI has been widely used for flow quantification in the aorta [19], the carotid arteries [20] and the intracranial vessels [21]. For routinely used 2D CINE PC-MRI, a slice for a 2D measurement is manually



Fig. 16.2 In 2D CINE PC-MRI, ECG triggering over multiple R-R intervals is used to acquire a series of time frames over the cardiac cycle. For each time frame, reference MRI raw data (k-space) lines (without bipolar gradient) and velocity encoded k-space lines (with bipolar gradient) are acquired. The number of k-space lines acquired for each time frame is determined by the segmented k-space or turbo field echo factor. After completion, phase contrast magnitude anatomical images and phase difference containing the velocity information are reconstructed. The figure illustrates 2D PC-MRI acquisition at the site of the aortic valve peak systole (top) and diastole (bottom)

positioned perpendicular to a vessel, and blood flow velocity is encoded in one direction through the 2D slice. However, placement of the acquisition plane remains challenging and can lead to the underestimation of peak velocities if misplaced or not orthogonal to the flow of interest. This is a common occurrence in cases involving complex flow and where changes in flow direction occur throughout the cardiac cycle, such as with valvular stenosis, valvular regurgitation, complex congenital

heart disease, or aneurysms. These challenges can be addressed by three-dimensional (3D) PC-MRI with three-directional velocity encoding which can provide comprehensive information on the in vivo 3D blood flow dynamics with full volumetric coverage of the vascular region of interest. Wigström et al. were the first to implement a high spatial resolution and electrocardiogram (ECG)-gated 3D cine phase contrast pulse sequence, currently known as 4D flow MRI (4D = 3D+ time over the cardiac cycle, flow = three-directional velocity encoding) [22].

4D Flow Acquisition Methods and Techniques

Data Acquisition

In 4D flow MRI, velocity is encoded along all three spatial dimensions throughout the cardiac cycle, thus providing a time-resolved 3D velocity field [8, 23, 24]. As shown in Fig. 16.3a, three-directional velocity measurements can be achieved by interleaved four-point velocity encoding which acquires one reference image and three velocity-encoded images along three orthogonal (x, y, z) directions [25–27]. As for 2D CINE PC-MRI, data acquisition is synchronized with the cardiac cycle, and data collection is distributed over multiple cardiac cycles using "k-space segmentation" techniques (only a fraction of the entire 4D flow data is measured during each cardiac cycle; the data is successively collected over multiple RR intervals). For prospective ECG gating, where the acquisition starts after receiving the R signal of the ORS complex, some dead time toward the next R-wave should be reserved to account for heartbeat variations. The late portion of diastole is therefore not measured [17]. With retrospective gating, continuous acquisition is not synchronized to the heartbeat. Each k-space line is time-stamped and retrospectively interpolated to fixed time frames in the cardiac cycle, thereby enabling acquisition of the diastolic phases. After completion of the 4D flow acquisition, four time-resolved (CINE) 3D data sets are generated ("magnitude" data depicting anatomy and three flow data sets representing velocities " V_x , V_y , and V_z ") as illustrated in Fig. 16.3b.

It should be noted that increasing 4D flow spatial resolution by reducing voxel size is possible but is accompanied by a decrease in signal-to-noise ratio (SNR) and thus image quality. Moreover, for volumetric acquisitions such as 4D flow MRI, scan times increase cubically with isotropic voxel size reduction.

An important (user-defined) 4D flow MRI parameter is the velocity encoding sensitivity (VENC), which represents the maximum flow velocity that can be acquired without velocity aliasing. When a velocity in a voxel exceeds VENC, velocity aliasing can occur which is typically visible as a sudden change from high to low velocity within a region of flow (see Fig. 16.4). If aliasing artifacts are present, accurate flow visualization and quantification may be compromised unless antialiasing correction can be successfully performed [28]. It is important to note, however, that velocity noise is directly related to the VENC [8]. Therefore, selecting a high VENC may alleviate the issue of velocity aliasing but will also increase the



C: 3D Blood Flow Visualization & Analysis

B: 4D flow Data



4D = 3 spatial dimensions + time
3 velocity directions



Fig. 16.3 Acquisition of 4D flow MRI data and analysis of hemodynamic metrics in the thoracic aorta of a healthy subject. (a) ECG synchronized 4D Flow MRI data acquisition. For each time frame, four 3D raw data sets are collected to measure three-directional blood flow velocities (v_x , v_y , v_z) with a reference scan and three velocity encoded acquisitions. k-space segmentation is used to collect a subset (N_{seg}) of all required raw data (k-space) lines for each time frame. The selection of N_{seg} determines the temporal resolution and total scan time. (b) 4D flow data comprises information along all three spatial dimensions, three velocity directions, and time in the cardiac cycle. (c) A 3D phase contrast angiogram (3D PC-MRA) can be calculated from 4D flow MRI data to aid visualization and provide a basis for the 3D segmentation of the aorta (orange rendering of aorta). Systolic streamlines allow for visual assessment of flow patterns and placement of analysis planes for retrospective flow quantification. Calculation of a systolic velocity maximum intensity projections (MIP) provides an overview over systolic velocity distribution and allows for volumetric quantification of peak systolic velocity (location of peak velocity is indicated by black circle in the ascending aorta). Advanced vessel wall characteristics can be derived such as systolic 3D wall shear stress (WSS) vectors along the aorta. AAo ascending aorta, DAo descending aorta



Fig. 16.4 (a) Bipolar gradients of higher strength and thus a low-VENC cause (b) aliasing (black arrow) in the phase difference images of the aorta, whereas aliasing is avoided when VENC is tailored to the expected maximum velocity in (c). (d) At a high VENC, the sensitivity to changes in aortic velocities is decreased. AAo ascending aorta, DAo descending aorta

| | k-space segmentation (turbo field echo factor) | (Isotropic) spatial resolution (mm ³) | Temporal resolution (ms) | VENC (cm/s) |
|--------------|---|--|-----------------------------|----------------|
| Heart/aorta | 1–3 | 2.0-3.0 | 20-60 | 150-400 |
| Carotid | 2–3 | 0.8–1.4 | 40-60 | 100-150 |
| Intracranial | 2-4 | 0.5-1.2 | 40-80 | 70–150 |

 Table 16.1
 Typical (ranges of) scan parameters for three different anatomical regions

level of velocity noise in flow velocity images. VENC should thus be chosen as close to the peak velocity as possible. This is often accomplished by performing a fast low-resolution 2D PC-MRI "VENC scout" scan prior to 4D flow MRI to estimate the highest velocity in the vessel of interest and adjust VENC accordingly.

In Fig. 16.4, the principle of VENC is shown for through-plane 2D phase difference images of the aorta with severe velocity aliasing when the VENC is selected too low (high bipolar gradient). Unaliased flow velocities are achieved when the VENC is tailored to the expected maximum velocity (lower bipolar gradient).

In Table 16.1 typical ranges of scan parameters are shown for heart/aorta, carotid, and intracranial 4D flow MRI applications.

Data Acquisitions: Imaging Acceleration Techniques

Long scan times on the order of 10–20 minutes have previously relegated 4D flower MRI to the realm of research. However, current implementations are quickly approaching clinically feasible scan times, on the order of 2–8 minutes. Methodological improvements include echo planar imaging (EPI), where multiple Cartesian readouts are acquired after one excitation to obtain high spatial resolution [29]. Additional imaging acceptation is based on parole imaging such as sensitivity encoding (SENSE) [30, 31], generalized autocalibrating partially parallel acquisitions (GRAPPA) [32], k-t acquisition speed-up techniques (k-t BLAST) [33, 34], k-t GRAPPA [35], k-t principal component analysis (k-t PCA) [36, 37], and

CIRCUS [38]. Another promising technique to accelerate 4D flow MRI is compressed sensing where data is acquired in a sparse and random manner followed by nonlinear recovery of data [39, 40]. For example, aortic 4D flow MRI is now possible with a scan time of less than 2 minutes without substantial degradation of image quality [41].

Data Acquisitions: Non-Cartesian Sampling

An alternative technique that is increasingly used to accelerate 4D flow MRI is radial data sampling combined with undersampling (e.g., PC-VIPR - vastly undersampled isotropic projection reconstruction [42]). Radial sampling has two important advantages over Cartesian readouts: (1) sparse sampling results in streak image instead of fold-over artifacts which allows for higher undersampling factors [42] and (2) the center of k-space is continuously sampled and results in insensitivity to subject motion [43]. As an alternative, spiral k-space sampling can cover the entire k-space uniformly and rapidly [44], allowing for rapid 4D flow MRI velocity measurements [45–47]. However, both radial and spiral sampling are sensitive to eddy current effects which require efficient correction strategies, and image reconstruction is more computationally demanding. Alternatively, radial- and spiral-like trajectories can be implemented on a Cartesian grid, called pseudo-radial and pseudo-spiral trajectories [48, 49]. For example, a recently reported combination of pseudo-Cartesian acquisition schemes coupled with compressed sensing for imaging acceleration has shown great potential for fast and robust pediatric 4D flow MRI [50].

Data Acquisitions: Respiratory Control (Gating, Self-Gating)

For cardiothoracic and abdominal applications, methods for respiration control are needed to prevent image deterioration due to respiratory motion. Early efforts in MRI have focused on gating of the respiratory signal using bellows [51] or navigator echoes in a longitudinal beam placed on the diaphragm [52]. Most methods are based on accepting data in the expiration phase when chest motion is minimal and rejecting data acquired in the inspiration phase when the chest is moving. Other strategies minimize respirator-related image degradation by respiratory ordered phase encoding (ROPE): measurements at inspiration are attributed to the center of k-space, whereas the measurements at expiration are attributed to the edges of k-space [53]. Such strategies have been successfully implemented for 4D flow MRI [54] in combination with navigator gating [55]. Other promising approaches employ self-gating techniques, e.g., cross-correlation with reference breathing motion to identify different respiratory phases [56] or extracting respiratory and cardiac motion signals from additional and repeatedly sampled central k-space data [57].

4D Flow Analysis Methods and Techniques

Preprocessing and Phase Offset Error Corrections

4D flow MRI data are affected by systematic velocity encoding errors caused by magnetic field inhomogeneity, concomitant magnetic fields (Maxwell terms) [58], and eddy currents [59, 60]. Correction of these errors typically includes the identification of image regions that contain static tissue in order to estimate the spatial distribution of background phase offsets (using a first- or second-order fit to the static tissue phase difference data) [61]. Background phase errors can subsequently be removed by subtraction of the estimated offset from the entire velocity data [62].

It is common in 4D flow MRI that the VENC setting is lower than the maximum velocity in the measurement and that velocity aliasing occurs. With the assumption that adjacent pixel velocities in the temporal or slice direction should not differ more than VENC [28], aliased velocities can be automatically detected and corrected [63].

Visualization and Quantification of 4D Flow MRI Hemodynamics

For effective visualization of the information encoded in the large 4D flow MRI data sets (see Fig. 16.3b), many methods have been developed and include velocity vector display in three-dimensional space [64, 65] streamlines [66, 67], and path lines/ particle traces [67].

Figure 16.3c illustrates 4D flow MRI-based evaluation of fundamental (flow, peak velocity) and advanced hemodynamic metrics (wall shear stress, WSS) based on a single acquisition. Visualization of the vascular geometry can be achieved from a 4D flow acquisition by generating a non-contrast 3D PC-MR angiogram (MRA). A surface rendering of the vascular structure of interest (see Fig. 16.3c, left) allows for regional orientation, analysis, and flow visualization. For qualitative visualization of 4D flow MRI data, 3D streamlines or time-resolved 3D path lines can be used for flow pattern visualization. Streamlines represent the instantaneous blood flow vector field for a single cardiac time-frame. For example, Fig. 16.3c illustrates the use of systolic 3D streamlines to visualize the spatial distribution and orientation of blood flow velocities. Color-coding by velocity magnitude facilitates the visual identification of regions with high systolic flow velocities. For visualization of the temporal evolution of 3D blood flow, time-resolved path lines are the method of choice. Time-resolved path lines are best viewed and displayed dynamically (movie mode) to fully appreciate the dynamic information and changes in blood flow over the cardiac cycle. It is important to differentiate between streamlines and path lines since the former represents the instantaneous tangent to the velocity vector at a given time in the cardiac cycle (e.g., peak systole), while the latter resemble traces of the dynamically time-varying blood flow over the cardiac cycle. 4D flow MRI can also be used to derive volumetric and maximum intensity projections (MIPs) of



Fig. 16.5 (a) 3D flow visualization (path lines and with flow quantification in perpendicular 2D analysis planes at standardized locations in the healthy aorta) [68]. (b) 3D segmentation and flow visualization in the circle of Willis of a healthy volunteer. Flow quantification based on perpendicular 2D analysis planes allows for the systematic assessment of blood flow over the cardiac cycle in the entire circle of Willis

peak velocity for easy volumetric identification of peak flow velocities (see Fig. 16.3c).

For quantification of flow in a vessel, 2D analysis planes can be placed at any location along the vessel of interest (Fig. 16.3c) to calculate peak and mean velocities, total flow, net flow, or retrograde flow. Figure 16.5a illustrates aortic 4D flow MRI with subsequent 3D flow visualization (path lines) and flow quantification in six 2D analysis planes distributed along the thoracic aorta. Figure 16.5b depicts an example of comprehensive cerebrovascular 4D flow with 3D blood flow visualization in the large intracranial arteries and quantification of flow-time curves at all major circle of Willis arteries.

Advanced Hemodynamic Vessel Wall Metrics

In addition to 3D blood flow visualization and planar flow quantification, 4D flow MRI offers the opportunity to derive advanced hemodynamic measures such as vorticity [69, 70] and helicity [71, 72], wall shear stress (WSS) [73, 74],

pressure gradients [75, 76], viscous energy loss [77, 78], turbulent kinetic energy [79, 80], or pulse wave velocity (PWV) [81, 82]. This article will focus on the two parameters most relevant for vascular wall characterization: PWV and WSS.

Pulse Wave Velocity

It is well understood that arterial vascular stiffening (i.e., reduction of vessel wall elasticity) can lead to atherosclerosis and the development of vessel wall abnormalities and atherosclerotic plaques. Pulse wave velocity (PWV), the best known surrogate measure for arterial stiffness, is the speed of the pulsatile pressure wave that propagates along arteries in a heartbeat [83-85]. PWV is determined by the elastic modulus of the vessel, the vessel wall thickness, the vessel radius, and the density of blood (Moens-Korteweg equation) [85]. Thus, increased PWV is directly associated increased elastic modulus (i.e., stiffening) and vessel wall thickness. Both processes occur in early atherosclerosis, and PWV is thus considered an important indicator for the onset of this disease. A meta-analysis revealed that increased PWV and thus reduced aortic compliance is a strong predictor of future cardiovascular events and all-cause mortality. Moreover, an increase in aortic PWV by 1 m/s corresponded to an age-, sex-, and risk factor-adjusted risk increase of ca. 15% in total cardiovascular events [86]. Reliable measurement of PWV is thus of high interest, e.g., for monitoring vessel compliance during therapy [87, 88].

Carotid-femoral PWV using tonometry is the current reference standard to measure aortic compliance [89]. This method, however, is prone to errors and does not focus on regional compliance. Time-resolved 2D CINE PC-MRI provides a noninvasive estimate of PWV based on flow waveform measurements in analysis planes and allows focusing on the region of interest in patients, e.g., the thoracic aorta or carotid arteries [90–92]. Transit-time (TT) methods are typically employed to calculate temporal differences of specific flow waveforms features, e.g., timing differences of the foot of the waveform between two locations with known distance, as first described in 1989 for the aortic arch [93]. The accuracy of PWV quantification can be improved by adding velocity encoding directions [81] or using multiple measurement locations [94, 95].

PWV can be retrospectively quantified from 4D flow MRI data based on multiple pulsatile flow waveforms distributed homogenously along the entire course of the vessel. As shown in Fig. 16.6 for 4D flow-based PWV estimation in the thoracic aorta, flow-time curves are automatically extracted for each analysis plane, and a measure of blood travel time (e.g., time-to-foot) is derived. Aortic PWV (in m/s) is determined by a linear fit from data of the entire aorta [82, 96]. However, reliable PWV assessment requires measure of the rapid changes of which can only be achieved with sufficient temporal resolution.



Fig. 16.6 Derivation of aortic pulse wave velocity from 4D flow MRI: (**a**) flow curves are automatically extracted in multiple planes along the aortic centerline. An initial plane #0 is positioned at the proximal asking aorta. Subsequently, all other 2D analysis planes will be positioned downstream in fixed intervals. (**b**) For each analysis plane, flow-time curves are calculated and the timedelay between adjacent planes is derived. (**c**) Aortic PWV (in m/s) is determined by a linear fit from data of the entire aorta. AAo: ascending aorta, DAo: descending aorta

Wall Shear Stress

The three-directional velocity fields can be used to calculate WSS (i.e., the blood shear rate on the endothelial cells that line the vessel wall multiplied by blood viscosity), a known pathophysiological stimulus cited to alter gene expression and endothelial cell function [97]. Altered shear forces at the intimal surface can promote endothelial changes and create areas at risk for vascular remodeling, i.e., when high WSS is sensitized, growth factors and other molecules such as nitric oxide (NO) and matrix metalloproteinases (MMPs) are released to dilate the vessel to restore the normal WSS value [98]. Altered WSS has been associated with the development of vulnerable plaques in the carotid arteries [99], progressive aortic dilation [100, 101], or development of cerebrovascular aneurysms [102-104]. WSS can be estimated from 4D flow MRI data by multiplying the deformation tensor $\dot{\varepsilon}$ that contains the velocity gradients in all directions at the wall, with the viscosity of blood. As schematically illustrated in Fig. 16.7 (top), initial studies have employed 4D flow MRI to quantify regional time-resolved WSS based on 2D analysis planes [105]. The variation of WSS direction over the cardiac cycle can be used to calculate the oscillatory shear index (OSI) [106]. More recently, methods have been

1. Time-resolved 3D segmental WSS on 2D plane



Fig. 16.7 (1) 3D segmental WSS in 2D planes. (**a**) Planes are placed perpendicularly to the aorta measured with 4D flow MRI, (**b**) contours are manually drawn to delineate the vessel wall and to define the segments for WSS calculation, (**c**) B-spline fits through the v_x and v_y velocities are created to derive the gradients at the wall that after multiplication with blood viscosity, (**d**) yield the WSS vectors in the plane. When repeated for all time frames, OSI can be calculated. (2) 3D WSS on the entire aorta surface. (**e**) At each point along the vessel wall, the *z*-axis is aligned with the inward normal vector, and with the assumption that there is no velocity through the wall, the deformation tensor is reduced from nine components to two (**f**). Spline fits along the *x* and *y* velocities along the normal vector yield the v_x and v_y derivatives. After multiplication with viscosity and rotation back to the original axes system, the local WSS vector is obtained

developed to compute volumetric 3D WSS along the 3D surface of the entire aorta, carotid or intracranial vasculature, or aneurysms (Fig. 16.7, bottom) [74, 107–109]. For the aorta, a method for the quantification of turbulent WSS variation was recently developed [110].

Although 3D WSS mapping allows for compact visualization of hemodynamic parameters (see Fig. 16.7, (2)), it does not detect where "abnormal" values are present. In addition, aortic WSS undergoes significant changes during healthy aging which underlines the importance of age-matched control cohorts in clinical studies to identify patients with altered WSS [111]. To address this limitation, a "WSS heatmap concept" was recently developed which offers the opportunity to quantify the extent of altered WSS [112]. The method is based on aortic 4D flow MRI data of a healthy control population to create an aortic "WSS atlas." As shown in Fig. 16.8, the aortic



Fig. 16.8 Patient-specific WSS heatmaps. (**a**) A 3D cohort-averaged WSS map of a control cohort ("WSS atlas") is used as reference to provide mean, median, and normal confidence intervals ($CI = \pm 2$ standard deviations, SD) of the normal physiologic aortic WSS distribution. (**b**) After delineating the regions of abnormal WSS for an individual patient, defined as values outside the CI, heatmaps of abnormally elevated or decreased WSS are created

atlas establishes regional confidence intervals for normal physiologic WSS throughout the aorta. Patient-specific WSS is then co-registered to the healthy control atlas to calculate heatmaps which represent regions of abnormally low or high WSS (i.e., outside of the 95% confidence interval provided by the control WSS atlas).

It should be noted that the discrete nature of the 4D flow MRI measured velocity field will result in a systematic underestimation of WSS. This is a common limitation of the technique. While absolute accuracy when assessing WSS in vivo is challenging, the relative pattern of expression (and magnitude) can reliably be inferred, especially if scan parameters and the procedure for WSS estimation are consistent between study populations [113, 114].

4D Flow MRI in Vessel Wall Disease: From Head to Toe

Head

In clinical practice, transcranial Doppler ultrasound is routinely used for cerebrovascular flow measurements. However, the technique is operator-dependent and limited by the acoustic windows of the head. 2D PC-MRI can provide reliable flow measurements in large intracranial arteries and veins, not limited by location. However, challenges for using 2D PC-MRI for flow measurement include small and tortuous vessels [115], complex vascular anatomy, and need for the manual placement of 2D imaging planes in multiple vessel segments. As an alternative, 4D flow MRI is increasingly used to assess cerebrovascular 3D blood flow [116, 117]. Emerging applications include the hemodynamic evaluation of intracranial aneurysms, arteriovenous malformations (AVM), and intracranial atherosclerotic disease (ICAD). Several groups have reported the successful measurement and evaluation of flow and WSS in intracranial aneurysms in patient feasibility studies [107, 118–121], indicating the potential of flow MRI to assist in the classification of individual aneurysms pre-intervention.

Arteriovenous Malformations (AVMs)

In patients with cerebral AVMs, flow information is potentially valuable for a better understanding of the impact of a focal AVM on the flow redistribution in the brain and/or in treatment planning by attempting to identify the feeding arteries with highest flow (see Fig. 16.9), enabling efficient and targeted embolization treatment. Recent reports include the quantification of flow and WSS in patients using a highly optimized radial 4D flow technique [108, 122]. Additional studies demonstrated the potential of 4D flow MRI for the evaluation of global and regional AVM flow



Fig. 16.9 Intracranial 4D flow MRI (left) and time-of-flight (TOF) 3D angiogram (right) in a 62-year-old male patient with a large cerebral AVM (Spetzler-Martin grade = 3). The dense AVM vascular network and high flow velocity in a main AVM feeding artery (arrow) can clearly be appreciated

characteristics [123, 124]. The findings showed that 4D flow MRI can assess treatment-induced changes in cerebrovascular flow distribution and was able to demonstrate significant associations between 4D flow metrics, cerebral perfusion indices, and AVM risk factors such as the Spetzler-Martin grade [124].

Intracranial Atherosclerotic Disease (ICAD)

Intracranial atherosclerotic plaques can alter local and global hemodynamics (particularly proximal or distal to stenosed vessels). Currently, intracranial hemodynamic disturbance in patients with ICAD is primarily assessed using transcranial Doppler ultrasound. Few studies have been performed to characterize the 3D blood flow disturbance and flow redistribution across the major cerebral arteries in patients with ICAD. An early study by Hope et al. reported that TOF MRA overestimated the degree of stenosis and that 4D flow MRI velocity measurements could improve accuracy of diagnosis, when compared to catheter angiography [119]. It should be noted that current flow imaging techniques (2D and 4D) are limited by insufficient spatial resolution for the characterization of blood flow at sites of critical or severe stenosis. Instead, post-stenotic flow is typically used to represent the regional flow in the stenotic artery. Higher magnetic field (7 Tesla) with increased spatial resolution may be required for improved flow assessment in the smaller vessels [125].

Intracranial Aneurysm

A large number of studies investigating flow patterns in intracranial aneurysms were based on computational fluid dynamics (CFD) techniques in conjunction with subject-specific geometries extracted from medical images [126–129]. Findings from these studies revealed a wide variety of complex intra-aneurysmal flow patterns that were strongly dependent on patient-specific vascular geometry. In addition, a number of studies showed that changes in WSS along the wall of intracranial aneurysms may be associated with risk of aneurysm growths or rupture [73, 107, 121]. However, CFD has limitations such as assumptions concerning blood properties, boundary conditions, and vessel properties [129–131]. As an alternative, 4D flow MRI is increasingly used to assess intra-aneurysmal 3D hemodynamics in vivo. Several groups have reported the successful measurement and evaluation of intra-aneurysmal flow and WSS in patient feasibility studies [73, 116, 119, 132–137], indicating the potential of flow MRI to assist in the classification of individual aneurysms pre-intervention.

Neck

Carotid artery stenosis is a leading cause of ischemic stroke, and detailed insights into the causes for the development of atherosclerosis at this site are of interest. Among other risk factors, it is assumed that the development of atherosclerosis in the naturally bulbic ICA is related to local hemodynamic conditions such as flow deceleration or recirculation associated with reduced and oscillating WSS [138]. Particularly, low absolute WSS and high OSI are hypothesized to determine the composition of atherosclerotic lesions and the development of high-risk plaques [99, 102]. Since blood flow through the carotid bifurcation is complex with non-symmetric flow profiles, the full three-directional velocity information by 4D flow MRI can be useful for a complete in vivo assessment of the segmental distribution of WSS.

4D flow studies analyzing WSS in the normal carotid bifurcation confirmed that potentially atherogenic wall (e.g., low WSS) parameters were predominantly concentrated at the posterior wall of the proximal ICA [139, 140]. Cibis et al. found lower WSS in regions of higher wall thickness in the carotid bifurcation [141, 142]. An example of a cohort-averaged map showing low WSS at locations of high wall thickness is displayed in Fig. 16.10. The wall thickness map is in concordance with the tendency of carotid atherosclerosis to affect the outer walls of arterial bifurcations and to mostly develop in the proximal part of the ICA bulb [143, 144]. Moreover, a significant relationship between the size of regions exposed to altered wall parameters and the individual bifurcation geometry was demonstrated, similar to carotid bifurcation study using CFD [138]. In patients with ICA stenosis, markedly altered filling and helix formation in the ICA bulb were observed, while revascularization partly restored normal filling and helix formation [145]. Furthermore, a direct comparison of mean and absolute flow velocities in the common carotid artery (CCA) between 4D flow MRI and Doppler ultrasound showed good agreement despite general underestimation of peak velocities by MRI [146].

4D flow MRI-derived WSS quantification could thus be a valuable technique to assess the individual risk of flow-mediated atherosclerosis and carotid plaque progression.



Fig. 16.10 Three-dimensional (a) wall shear stress and (b) wall thickness carotid bifurcation maps averaged over 20 subjects with plaques. In (c) the correlation between WSS and WT is shown with color-coding for the density of the points

The assessment of PWV in the carotid arteries as a measure of vessel stiffness (and thus atherosclerotic burden) is challenging due its small size that necessitates high spatial and temporal resolution [147]. It is thus challenging to derive PWV using 4D flow MRI in the carotid arteries. For the determination of local PWV in the carotid arteries, the temporal resolution of through-plane 2D CINE PC-MRI was recently drastically improved by compressed sensing acceleration [148]. These novel acquisition strategies hold promise for future applications of either 2D or 4D flow MRI-derived PWV.

Thorax

Cardiothoracic 4D flow imaging is typically performed as part of a standard-of-care aortic/pulmonary imaging protocol, which includes additional MRI techniques for the assessment of cardiac function and wall motion (CINE imaging), aortic and pulmonary dimensions and geometry (MR angiography), as well as aortic and pulmonary valve morphology and dynamics (CINE imaging). The combination with 4D flow MRI provides a comprehensive assessment of aortic/pulmonary structure and function. These data have contributed to the understanding of the development of vessel wall abnormalities (atherosclerosis, aortic dilation, aneurysm) as a consequence of thoracic vascular diseases such as aortic valve diseases (stenosis, insufficiency, congenital bicuspid aortic valve (BAV)), aortic coarctation, or Marfan syndrome.

Aortic Valve Disease and Aortopathy

The presence of aortic valve disease significantly alters the hemodynamic environment in the thoracic aorta. Several studies have shown promise of 4D flow MRIbased blood flow visualization for the investigation of valve-related abnormal flow patterns (e.g., aberrant vortex or helix flow) as shown in Fig. 16.11. However, the visual evaluation of changes in aortic flow patterns (e.g., grading of vortex of helix flow) can be limited by lack of standardization, observer bias, and thus reproducibility. A more effective and representative assessment is provided by the calculation of 4D flow-derived measures that quantify the impact of altered flow characteristics on the vessel wall, such as flow displacement and WSS.

Flow displacement is an easy to obtain quantitative marker that represents outflow asymmetry (i.e., deviation for a symmetric flow profile). Studies have shown that flow displacement can detect altered systolic outflow patterns in patients with different types and severity of aortic valve disease [149–153] or in patients with aortic dilation [154]. For example, recent studies showed that different aortic valve fusion phenotypes in patients with BAV resulted in distinctly altered eccentric aortic outflow jet patterns [101, 155]. Differences in aortic dilation type were associated



Fig. 16.11 Velocity and WSS in two patients with a stenosed bicuspid aortic valve. (**a**, **d**) Peak systolic velocity path lines showing right-handed helical flow (top) and left-handed helical flow (bottom). Vortex flow can be seen as well (white arrows). (**b**, **e**) Stenotic flow leads to high wall shear stress on the right-anterior aortic wall (top) and left-posterior wall (bottom) which can be concisely visualized by elevated WSS heatmaps (**c**, **f**)

with altered flow displacement in the ascending aorta, suggesting a physiologic mechanism by which valve morphology can influence aortic wall remodeling.

Patient studies have demonstrated the potential of WSS to quantify the impact of deranged flow on the aortic wall. Initial 4D flow studies were based on 2D-based planar quantification of WSS changes in patients with aortic dilation [156], aortic atherosclerosis [157], or aortic valve abnormalities such BAV disease [101, 158–160]. Bieging et al. were the first to create a 3D segmentation of the aorta for the purpose of regional WSS estimation in patients with ascending aortic aneurysms [74]. More recently, Potters et al. used a modified algorithm to estimate 3D WSS on the entire aorta surface [109].

Interestingly, several 4D flow MRI studies have shown that the presence of aortic valve disease has a very different effect on aortic hemodynamics as compared to aortic dilation or aneurysm alone. Aortic dilation with an otherwise normal aortic valve generally leads to slow helix-type flow with significantly reduced WSS in the ascending aorta. In contrast, BAV or aortic valve stenosis will result in significantly elevated flow velocities, high-velocity transvalvular outflow jets, and eccentrically elevated WSS. These findings have been confirmed by a series of studies by Bissel et al., Mahadevia et al., Shan et al., and Rodríguez-Palomares et al. in larger cohorts (65–142 subjects, respectively) [100, 101, 155, 161]. A recent large cohort 4D flow MRI study in patients with aortic valve disease (>500 subjects) confirmed these findings. As shown in Fig. 16.12, aortic 4D flow MRI can be used to show the incidence of elevated WSS for specific groups of patients and healthy controls. Results clearly showed that aortic valve stenosis resulted in a marked increase in regional WSS compared to patients with aortic dilation but normal tricuspid aortic valve



Fig. 16.12 (a) Registration and interpolation techniques are used to project regions of elevated WSS onto a shared aortic geometry. Summing elevated WSS regions yields a map of the regional incidence of elevated WSS. Group-specific 3D maps of abnormally elevated WSS for (b) tricuspid aortic valve (TAV) with dilation with no aortic valve stenosis (AS), mild AS and moderate and severe AS, and (c) BAV patients with right non-valve function morphology (RN-BAV) with no AS, mild AS, and moderate and severe AS

[162]. In addition, the WSS heatmap concept can be employed to highlight regions with abnormally elevated WSS in individual patients (see Fig. 16.12) [163].

A recent study utilized the WSS heatmap concept to assess the correlation between abnormal in vivo 3D WSS and regional aortic tissue remodeling in BAV patients with AS [164]. BAV patients undergoing ascending aortic resection received preoperative 4D flow MRI to regionally map 3D WSS and correlate these findings with histologic examination of surgically resected tissue samples. Paired aortic wall samples (i.e., regions of both elevated and normal WSS within the same patient) were collected and compared for medial elastin degeneration by histology. Regions of increased WSS showed greater medial elastin degradation compared to adjacent areas with normal WSS. Another study confirmed these results and showed that in the presence of aortic stenosis, the correlation between WSS and elastin fiber thickness was stronger than without AS [165]. These data suggest that regional valvemediated hemodynamics could serve as potential prognostic biomarkers of aortic disease.

Marfan Syndrome

Marfan syndrome is an inherited autosomal dominant connective tissue disease, mostly related to mutations in the fibrillin-1 (FBN1) gene. Many organ systems can be involved, but most life-threatening complications are related to the cardiovascular system and include aortic wall abnormalities leading to dissection and aortic rupture. Although the entire aorta may dilate in Marfan syndrome, the aortic root and the proximal descending aorta are prone for progressive dilation and dissection [166–168]. Few studies have investigated aortic WSS in MFS disease cohorts [169–171]. Altered WSS was most pronounced in the proximal ascending aorta and the proximal descending aorta, which corresponds to locations where aortic dissection and rupture are most likely to occur. A recent longitudinal study in Marfan patient with baseline and mean follow-up 4D flow MRI (mean duration of 3.5 ± 1.2 years) confirmed these findings [169]. MFS patients had lower segmental WSS in the inner proximal DAo segment which correlated with increased localized aberrant vortex/helix flow patterns and an enlarged diameter. Aortic hemodynamics were stable over multi-year follow-up, but subtle localized flow changes in the descending aorta were already present at young age and tended to be more pronounced in the course of time. This is an important and intriguing finding, as the proximal descending aorta is a known initiation region for type B aortic dissections.

4D flow MRI was also used to calculate PWV as a measure for aortic stiffness in the aorta of BAV patients compared to controls and Marfan patients [172, 173]. Marfan patients had markedly higher aortic PWV and thus stiffer aortas compared to controls and BAV patients. The increased aortic stiffness may lead to further deterioration of aortic and LV function and may thus constitute important parameter for longitudinal monitoring of risk for progressive aortic dilation in these patients.

Aortic Coarctation

Aortic coarctation accounts for 6% of congenital cardiac malformations, is associated with hypertension and peripheral vascular disease, and often requires surgical repair [174]. This disease is characterized by a congenital narrowing of the aorta, usually at the level of the distal arch or proximal descending aorta. To provide insight into the degree of stenosis and impact on distal flow as a result of the coarctation, traditional assessment includes aorta diameter measurements and post-coarctation flow velocity assessment. Using 4D flow MRI to assess this cohort of patients has proven to provide useful characteristics about the impact of coarctation and coarctation repair on flow features throughout the aorta. Recent studies have shown that 4D flow MRI can measure and visualize alterations in 3D aortic hemodynamics in coarctation patients such as elevated helix and vortex flow throughout the entire aorta, including the region of repair [175–178]. Patients with aortic coarctation tend to have flow jet eccentricity following the coarctation resulting in jet impingement and elevated WSS along the descending aorta [179, 180].

Aortic Atherosclerosis

Stiffening of the aorta is frequently observed with increasing age and disease (e.g., hypertension, diabetes) due to an increase in the collagen-elastin ratio. Increased stiffness results in greater hemodynamic loading conditions on the aortic endothe-lium leading to the development of atherosclerosis [84, 181].

The most commonly measured and best surrogate for arterial stiffness is pulse wave velocity (PWV) [85, 182, 183]. In 2 studies with 37 and 98 subjects, respectively, the reliability of 4D flow-based estimation of global aortic PWV was demonstrated in volunteers and patients with aortic atherosclerotic disease with a good observer dependence and excellent test-retest reliability [82, 184]. Both studies demonstrated significant correlations of aortic stiffness with age. In addition, in patients with atherosclerosis, the PWV was significantly increased compared with controls demonstrating the sensitivity of the technique to detect elevated aortic stiffness. In a recent study, 4D flow MRI-derived PWV parameters correlated significantly with echocardiographic stiffness parameters and intima-media thickness in the descending aorta of stroke patients [185]. Harloff et al. showed an increase in aortic PWV in older subjects that had more aortic plaque [186].

Peripheral Arteries

Peripheral arterial occlusive disease (PAOD) is commonly explored with basic clinical tests such as the ankle-brachial-index, constant load treadmill test, and Doppler ultrasound due to its excellent temporal and spatial resolution. A number of studies have reported the use of 2D PC MRI for the quantitative assessment of PAOD severity [187–190]. Similar to Doppler ultrasound, the waveforms derived in locations superior or inferior to stenoses were being used to characterize the severity of PAOD [191, 192]. In a similar fashion, 4D flow MRI can be applied to the peripheral arteries, but only few studies have been reported to date. Application of this technique in the lower extremities has been limited to a single study which evaluated the iliac and proximal femoral at 3T [193]. Limitations of 4D flow in the extremities include the large anatomical coverage needed for vessel assessment, small vessel size (specially in distal vessels), and thus long scan times to achieve sufficient spatial resolution and SNR. Future research is warranted to extend previously published feasibility results to longitudinal and comparative studies investigating the potential impact of 4D flow MRI in PAOD.

Future Directions and Conclusions

Recent developments related to highly accelerated 4D flow MRI have resulted in increased flexibility for the application of 4D flow MRI with reduced scan times and/or increased spatiotemporal resolutions. These developments have led to more widespread applications of 4D flow MRI, but further improvements in spatial resolution for the reliable quantification of vascular hemodynamics near the vessel wall or in small arteries affected are needed. 4D flow MRI acquisition at higher field strengths, e.g., 7T, and the associated increase in signal-to-noise ratio is promising in this regard. Studies have demonstrated that 7T 4D flow MRI allows for more detailed visualization of 3D velocity fields compared to 3T in the brain [125, 194]

and the aorta [195, 196]. However, 7T scanners are expensive and need tailor-made equipment and specialized operator expertise, which can hamper its clinical application. As an alternative, 4D flow image quality and velocity dynamic range can be improved by dual- or multi-VENC flow encoding. By combining a low-VENC acquisition with phase unwrapping guided by a simultaneous high-VENC acquisition, aliasing-free images can be acquired with high velocity-to-noise ratio [197]. By interleaving the high- and low-VENC acquisitions in combination with imaging acceleration techniques, dual-VENC 4D flow MRI has shown promise for detailed velocity measurements for neurovascular and aortic applications [198, 199]. Alternatively, additional velocity encoding steps further improved velocity-to-noise ratio, and velocity unwrapping can be added to standard acquisitions at the cost of extra scan time [27, 200, 201]. These methods showed improved aortic and neuro-vascular blood flow velocity visualization [202, 203].

PWV and WSS quantification are promising markers of vessel wall abnormalities but require laborious and time-consuming manual placement of analysis planes or segmentation of the 3D vessel lumen. To make 4D flow MRI data analysis more time-efficient, several groups have developed methods to automate these processing steps. For example, Bustamante et al. used advanced atlas-based methods for timeresolved aortic segmentation and plane placement [204]. The centerline of a 3D aortic segmentation can subsequently be used for automatic plane placement [151]. For 3D segmentation of the intracranial vasculature, highly automated algorithms were developed [205].

In conclusion, 4D flow MRI is a highly versatile technique which can be employed to derive important clinical parameters such as pulse wave velocity and wall shear stress in a large range of vessel wall diseases. Many studies have shown the additional value of 4D flow MRI in a clinical setting, but the methodology is still limitedly used for diagnosis or treatment planning in cardiovascular disease worldwide. Current and future efforts in the field are dedicated to the acceleration of the acquisition and the automated processing of the data, with the ultimate goal of developing 4D flow MRI in a widespread, easy-to-use clinical tool for vessel wall disease assessment.

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