

# Chapter 8

## Mechanistic Aspect of NO–NH<sub>3</sub>–O<sub>2</sub> Reacting System

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### 8.1 Introduction

This chapter delineates the mechanistic aspects of the NO–NH<sub>3</sub>–O<sub>2</sub> reacting system, also known as the *standard SCR* reaction. The standard SCR technology was first developed in the 1970s, and thus has a long history in the research area of catalyst development as well as the associated reaction mechanisms. Nevertheless, the reaction mechanisms do not always coincide even among the most popular systems such as the Cu or Fe ion-exchanged zeolites and vanadium-based catalysts. However, such extensive research activities conducted might be reaching a substantial agreement on several mechanistic details.

In this chapter, the reaction mechanisms of the standard SCR reaction are discussed from various perspectives including steady-state kinetics, the relations with NH<sub>3</sub>/NO oxidation ability and acid site amount, the effect of coexisting gases, and transient reaction behavior. Through these comprehensive analyses, some similarities and differences of the reaction mechanism among the conventional SCR catalysts could be extracted. Also, new perspectives on standard SCR mechanism could be suggested.

### 8.2 Steady-State Reaction Analysis

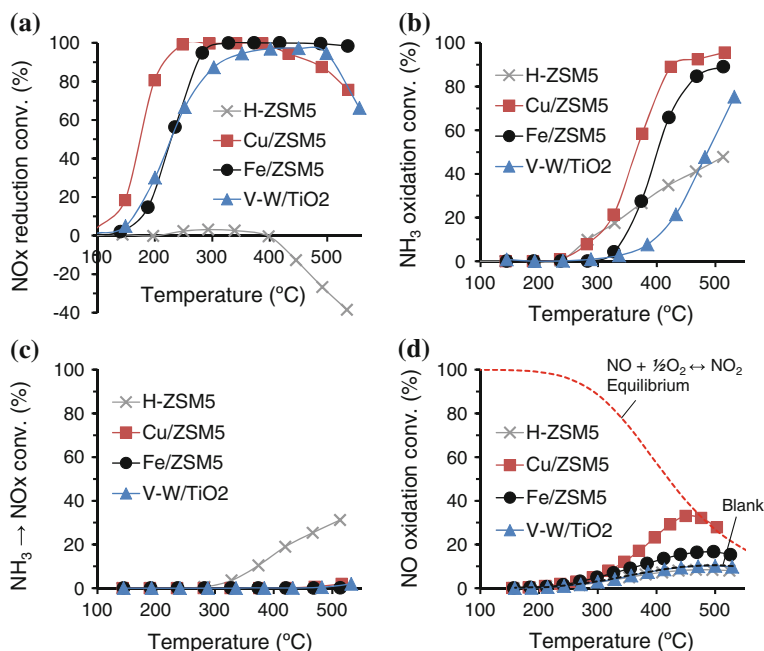
#### 8.2.1 NH<sub>3</sub>/NO/O<sub>2</sub>, NH<sub>3</sub>/O<sub>2</sub>, and NO/O<sub>2</sub> Reactions

To have a grasp of basic reaction behaviors, standard SCR as well as NH<sub>3</sub>/NO oxidation reactions were investigated under steady-state condition. For the samples, three conventional SCR catalysts, V–W/TiO<sub>2</sub>, Fe/ZSM-5, and Cu/ZSM-5,

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**Fig. 8.1** **a** NO<sub>x</sub> conversion under standard SCR reaction, **b** total NH<sub>3</sub> conversion and **c** NH<sub>3</sub> → NO<sub>x</sub> conversion under NH<sub>3</sub> oxidation reaction, **d** NO → NO<sub>2</sub> conversion under NO oxidation reaction. **a**: 0.05 % NO, 0.06 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, 8 % H<sub>2</sub>O with N<sub>2</sub>, **b**, **c**: 0.1 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, 8 % H<sub>2</sub>O with N<sub>2</sub>, **d**: 0.1 % NO, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, 8 % H<sub>2</sub>O with N<sub>2</sub>

were tested. Additionally, H-ZSM-5 was also tested as a reference. Figure 8.1a–d shows the catalytic activity of standard SCR, NH<sub>3</sub> oxidation, and NO oxidation reactions. The compositions of the feed gas were as follows: 0.05 % NO, 0.06 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, 8 % H<sub>2</sub>O with N<sub>2</sub> for standard SCR; 0.1 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, 8 % H<sub>2</sub>O with N<sub>2</sub> for NH<sub>3</sub> oxidation; 0.1 % NO, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, 8 % H<sub>2</sub>O with N<sub>2</sub> for NO oxidation.

For standard SCR reaction (NH<sub>3</sub>/NO/O<sub>2</sub> system) in Fig. 8.1a, Cu/ZSM-5 showed the highest activity in low temperature region (<300 °C), while Fe/ZSM-5 was the highest above 400 °C. On the other hand, H-ZSM-5 has little activity, and also negative conversions were seen over 400 °C due to NH<sub>3</sub> oxidation to NO<sub>x</sub>. The conversion of V-W/TiO<sub>2</sub> was nearly equal to that of Fe/ZSM-5 around 250 °C, though their temperature profiles differed slightly; V-W/TiO<sub>2</sub> was more active in the lower temperature (<200 °C), while the situation was the opposite in the higher temperature (>300 °C), which is also verified by Arrhenius plots in the Sect. 8.2.2. Since N<sub>2</sub>O was not detected for all the conditions, only the standard SCR reaction ( $2\text{NO} + \frac{1}{2}\text{O}_2 + 2\text{NH}_3 \rightarrow 2\text{N}_2 + 3\text{H}_2\text{O}$ ) progresses except for unselective NH<sub>3</sub> oxidation which was initiated at the higher temperature region (>400 °C).

From Fig. 8.1b, NH<sub>3</sub> oxidation without inlet NO started above 300 °C for all the catalysts, which is much higher onset temperature than the SCR reaction. As by-products, N<sub>2</sub>O was not detected for all the catalysts, and NO<sub>x</sub> was produced only for H–ZSM-5 above 300 °C (Fig. 8.1c). It indicates that NH<sub>3</sub> oxidation reaction to N<sub>2</sub> ( $2\text{NH}_3 + \frac{3}{2}\text{O}_2 \rightarrow \text{N}_2 + 3\text{H}_2\text{O}$ ) mainly proceeds for the three SCR catalysts. As for H–ZSM-5, on the other hand, a large amount of NO<sub>x</sub> was produced from NH<sub>3</sub>, probably because the rate of NH<sub>3</sub> oxidation to NO<sub>x</sub> should be much faster than that of SCR reaction between produced NO<sub>x</sub> and residual NH<sub>3</sub>.

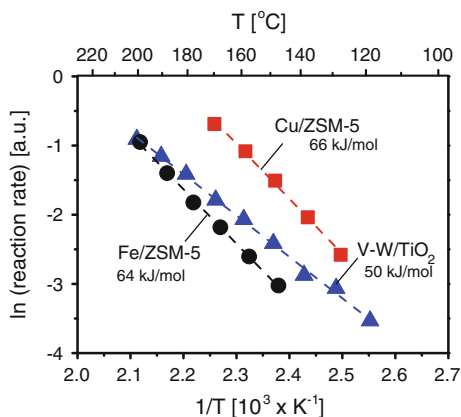
Figure 8.1d shows the NO oxidation conversion to NO<sub>2</sub> under the NH<sub>3</sub> absent condition. For all the samples, the NO oxidation conversion was much lower than SCR and NH<sub>3</sub> oxidation conversions, suggesting that NO is hard to be oxidized. Also, the NO oxidation ability (Cu–ZSM-5 > Fe–ZSM-5 > V–W/TiO<sub>2</sub> ≈ H–ZSM-5 ≈ Blank) does not necessarily coincide with the trend of SCR conversion (Cu–ZSM-5 > Fe–ZSM-5 ≈ V–W/TiO<sub>2</sub> ≫ H–ZSM-5). However, NO oxidation is believed to be a very important step in the SCR process, and thus it is discussed in more detail in another section.

## 8.2.2 Apparent Activation Energy

The apparent activation energies of the Fe/ZSM-5, Cu/ZSM-5, and V–W/TiO<sub>2</sub> catalysts were determined from the Arrhenius plots of the logarithm of the apparent rate versus 1/T as shown in Fig. 8.2. The reaction rates were measured with maintaining pseudo-differential condition. The composition of the gas was kept as 0.05 % NO, 0.05 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 8 % CO<sub>2</sub>, 10 % H<sub>2</sub>O with the remainder N<sub>2</sub>. The temperature range was varied from 120 to 200 °C because in the higher temperature region, other contributions such as diffusion limitation and/or NH<sub>3</sub> oxidation might be affected [1, 2]. The apparent activation energies of the Fe/ZSM-5 and Cu/ZSM-5 catalysts were estimated to be 64 and 66 kJ/mol which is roughly equivalent. On the other hand, the V–W/TiO<sub>2</sub> catalyst showed a more gradual slope than the zeolites and the activation energy was estimated to be 50 kJ/mol. This difference would be a main reason for the different temperature profiles between Fe/ZSM-5 and V–W/TiO<sub>2</sub> in Fig. 8.1a.

Efstathiou and Fliatoura [3] investigated the apparent activation energy of a V/TiO<sub>2</sub> catalyst while varying the NO and NH<sub>3</sub> concentration (0.05–0.2 %) at 150–190 °C. They reported that the change of the activation energy with the NO and NH<sub>3</sub> concentration was small and obtained a value of 48.5 kJ/mol (11.6 kcal/mol) under 0.1 % NO and 0.05 % NH<sub>3</sub> [3], which agrees well with the values estimated from Fig. 8.2.

**Fig. 8.2** Arrhenius plots of the logarithm of apparent SCR rate versus the inverse of temperature. Apparent activation energies are compared. Gas composition = 0.05 % NO, 0.05 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 8 % CO<sub>2</sub>, 10 % H<sub>2</sub>O with the remainder N<sub>2</sub>



### 8.2.3 Apparent Reaction Orders

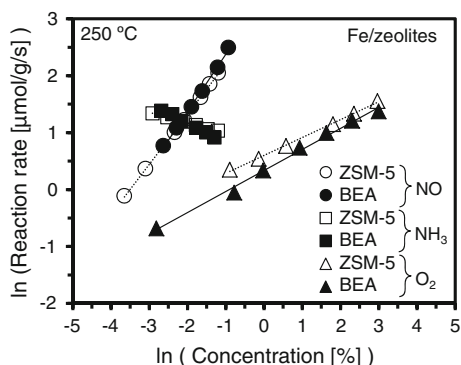
Reaction orders contain important information for predicting the rate-determining step as well as the reaction mechanism. Apparent reaction orders can be estimated by measuring the reaction rates with varying gas concentration (partial pressure) under pseudo-differential condition. Figure 8.3 shows the dependence of the standard SCR rate on the NO, O<sub>2</sub>, and NH<sub>3</sub> concentrations over Fe/ZSM-5 and Fe/BEA. Although the balance gas compositions were different for the two samples, i.e., 10 % CO<sub>2</sub>, 5 % H<sub>2</sub>O, and N<sub>2</sub> for Fe/ZSM-5 versus only N<sub>2</sub> for Fe/BEA, both showed identical dependence. The SCR rates increased with NO and O<sub>2</sub> concentrations but slightly decreased with NH<sub>3</sub> concentration. This indicates that the standard SCR reaction is promoted by NO and O<sub>2</sub> but is inhibited by NH<sub>3</sub>. Since all the data gave linear relationships under the log–log plots, the reaction rate can be simply expressed using the power law

$$r_s = k_{\text{app}}[\text{NO}]^\alpha[\text{O}_2]^\beta[\text{NH}_3]^\gamma$$

where  $r_s$  is the standard SCR rate,  $k_{\text{app}}$  is the apparent rate constant, and  $\alpha$ ,  $\beta$ , and  $\gamma$  are the apparent reaction orders for NO, O<sub>2</sub>, and NH<sub>3</sub>, respectively. Thus, the apparent reaction orders can be estimated from the slopes in Fig. 8.3, and are summarized in Table 8.1 along with the reported literature data [4–10]. As seen from Table 8.1, the reaction orders obtained here are comparable for the reported values for Fe/zeolites [6–8]; the NO orders are slightly lower than first order, the O<sub>2</sub> orders are slightly lower than half, while the NH<sub>3</sub> orders are negative.

Meanwhile, H-ZSM-5 shows approximately first order for O<sub>2</sub> [9, 10]. The reason for the difference in the O<sub>2</sub> orders between H-type zeolites and Fe/Cu zeolites could be due to the contribution of different forms of O<sub>2</sub> toward the rate-determining step; for instance, undissociated molecular O<sub>2</sub> or dissociated atomic O might participate in the elementary reaction.

**Fig. 8.3** Log–log plots of apparent SCR rate versus NO, O<sub>2</sub>, and NH<sub>3</sub> concentrations for Fe/ZSM-5 and Fe/BEA. Balance gas is 10 % CO<sub>2</sub>, 5 % H<sub>2</sub>O, and N<sub>2</sub> for Fe/ZSM-5, and only N<sub>2</sub> for Fe/BEA. Apparent activation orders are listed in Table 8.1



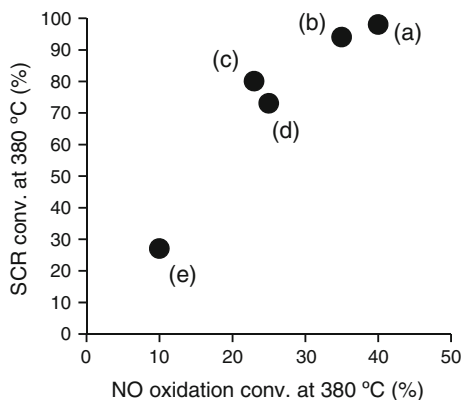
If one assumes that the rate-determining step in the standard SCR is the oxidation of NO, the reaction order for the NO oxidation should have a similar value with that for the SCR reaction. To confirm this presumption, the dependence of the NO oxidation rate on the NO and O<sub>2</sub> concentrations were investigated by using Fe/ZSM-5 and Fe/BEA. The estimated apparent orders are listed in Table 8.1 along with the relevant literature data [11]. The apparent reaction orders for the two Fe/zeolites showed similar values despite different structure and coexisting gases. Also, the reaction orders are nearly in accordance with the literature data reported by Metkar et al. [11]. They measured the NO and O<sub>2</sub> orders in the presence of NO<sub>2</sub> feed as an inlet gas, and found that the reaction orders for NO and O<sub>2</sub> did not change when the inlet NO<sub>2</sub> concentration was changed. By comparing the NO and O<sub>2</sub> orders between the NO oxidation and the SCR reaction (Table 8.1), one can find a similarity which is nearly first order for NO and nearly half order for O<sub>2</sub>. Thus, the rate-determining step in the standard SCR might be the NO oxidation step. The same holds true when the activation energies are compared; Metkar et al. [11] reported that the activation energy for the NO oxidation (39 kJ/mol) is nearly equal to the activation energy for the standard SCR reaction (42 kJ/mol) over Fe/ZSM-5.

However, there is a crucial difference between the two reactions, which is NO<sub>2</sub> order for the two reactions; the order is positive for the SCR reaction [4], whereas it is negative for the NO oxidation [11]. In fact, Iwasaki et al. [4] investigated the NO<sub>2</sub> order during NO/NO<sub>2</sub>/NH<sub>3</sub> reaction system (the so-called fast SCR condition) and found that the NO<sub>2</sub> order is positive for Fe/ZSM-5. Also, Metkar et al. [11] investigated the NO<sub>2</sub> order during the NO oxidation and estimated to be  $-0.42$  to  $-0.49$  for Fe/ZSM-5 and  $-0.89$  to  $-1.00$  for Cu/CHA. These differences would result from the different behavior of NO<sub>2</sub> on the surface; the NO<sub>2</sub> produced is consumed immediately by NH<sub>3</sub> during the SCR reaction, whereas the NO<sub>2</sub> and nitrate products are strongly adsorbed on the surface during the NO oxidation reaction, which is verified by in situ FT-IR in other chapter.

**Table 8.1** Apparent reaction orders of standard SCR and NO oxidation reactions using zeolite catalysts

Reaction	Catalyst	NO order	O <sub>2</sub> order	NH <sub>3</sub> order	Temperature (°C)	Coexisting gas	Ref
Standard SCR	Fe/BEA	1.00	0.37	-0.34	250	N <sub>2</sub>	U.D. <sup>a</sup>
Standard SCR	Fe/ZSM-5	0.81-0.90	0.29-0.34	-0.11 to -0.21	200-300	10 % CO <sub>2</sub> , 5 % H <sub>2</sub> O, N <sub>2</sub>	[4]
Standard SCR	Fe/ZSM-5	0.55-0.94	0.36-0.41	-0.11 to -0.15	260-300	He	[6]
Standard SCR	Fe/ZSM-5	0.90-1.02	0.33-0.39	-0.28 to -0.49	210-350	5 % H <sub>2</sub> O, N <sub>2</sub>	[7]
Standard SCR	Fe/ZSM-5	0.97-1.09	0.52-0.59	-0.27 to -0.32	200-300	Ar	[8]
Standard SCR	Cu/ZSM-5	1	0.60	0	300	He	[5]
Standard SCR	H-ZSM-5	1.00	0.77	-0.45	500	He	[9]
Standard SCR	H-ZSM-5	0.73	1.06	-0.61	340-440	0-20 % H <sub>2</sub> O, N <sub>2</sub>	[10]
NO oxidation	Fe/BEA	0.81	0.56	-	250	N <sub>2</sub>	U.D. <sup>a</sup>
NO oxidation	Fe/ZSM-5	0.90	0.67	-	280	10 % CO <sub>2</sub> , 5 % H <sub>2</sub> O, N <sub>2</sub>	U.D. <sup>a</sup>
NO oxidation	Fe/ZSM-5	0.9-1.0	0.55-0.59	-0.42 to -0.49 <sup>b</sup>	200-290	330 ppm NO <sub>2</sub> + Ar	[11]
NO oxidation	Cu/CHA	0.85-1.0	0.47-0.51	-0.89 to -1.00 <sup>b</sup>	200-290	330 ppm NO <sub>2</sub> + Ar	[11]

<sup>a</sup> U.D.: Unpublished data<sup>b</sup> NO<sub>2</sub> order



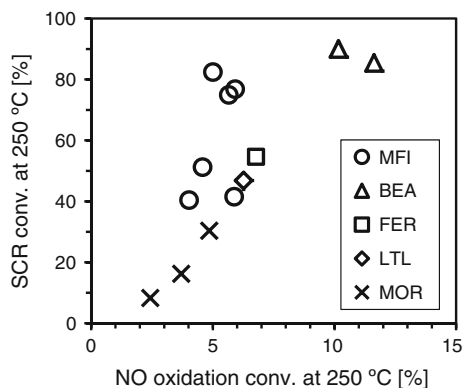
**Fig. 8.4** SCR conversion versus NO oxidation conversion for Fe/zeolites prepared by different Fe loading methods and amounts of Fe. The data is used from Ref [13]. Gas composition = 0.2 % NO, 0 or 0.2 % NH<sub>3</sub>, and 2 % O<sub>2</sub> with remainder He. The specification of the samples is described by “preparation method\_Fe/Al ratio”: **a** sublimation with FeCl<sub>3</sub>\_0.83, **b** sublimation with FeCl<sub>3</sub>\_0.49, **c** ion-exchange with Fe(acac)<sub>3</sub> followed by evaporation\_0.96, **d** ion-exchange by Fe(acac)<sub>3</sub> followed by washing\_0.21, **e** ion-exchange by Fe(NO<sub>3</sub>)<sub>3</sub> followed by precipitation\_0.35

### 8.2.4 Relationship with NO Oxidation Activity

As mentioned in Sect. 8.2.3, the oxidation of NO would be a crucial step in the standard SCR reaction. In fact, there are many reports in the literature which suggest that the SCR activity is correlated with the NO oxidation conversion when the same type of active metal is compared [12–17]. On the other hand, some literature indicates that there is no correlation between them especially when comparing different active species, such as Fe and Cu [11, 18–20]. In this section, the reason for this inconsistency has been discussed.

Figure 8.4 shows the relationship between the standard SCR conversion and NO oxidation reaction conversion using Fe/zeolites prepared by different Fe loading methods and Fe loading amounts. The data which is used from Ref. [13] by Delahay et al. demonstrates a positive correlation between them, implying that the active sites for NO reduction are identical with the NO oxidation sites. Figure 8.5 shows the relationship between standard SCR conversion and NO oxidation reaction conversion when several Fe/zeolites with different pore structures and Si/Al<sub>2</sub> ratios were used [16]. As can be seen from the figure, the SCR conversion in this case correlates well with the NO oxidation conversion. Thus, the activity relationship is preserved even when different types of zeolites are used.

However, when the comparison is made between different kinds of active metals, the SCR conversion does not always correlate with the extent of NO oxidation. For instance, Metkar et al. [11, 19]. have reported that Fe/ZSM-5 showed a higher NO oxidation conversion than Cu/CHA, while Cu/CHA



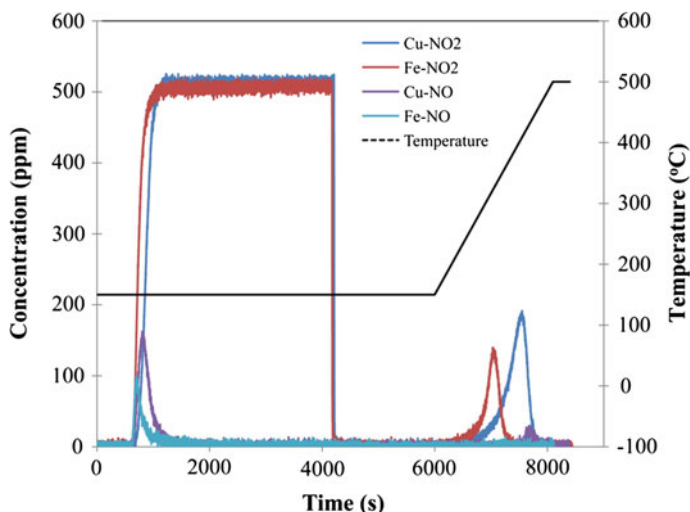
**Fig. 8.5** SCR conversion versus NO oxidation conversion of Fe/zeolites with different structure and Si/Al<sub>2</sub> ratio [16]. Gas composition = 0.1 % NO, 0 or 0.12 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, and 8 % H<sub>2</sub>O with remainder N<sub>2</sub>

possessed a greater SCR activity than Fe/ZSM-5. Thus, it seems that the SCR activity is not dependent on the NO oxidation under the comparison between Fe and Cu. The key to solve this discrepancy is that the determining factors for the two reactions would be different. Delahay et al. [13] discussed that the difference in activity between SCR and NO oxidation can only be explained if the NO oxidation reaction is controlled by the desorption of NO<sub>2</sub>. In fact, the desorption energy of NO<sub>2</sub> from Fe/ZSM-5 is very high (138 kJ/mol) [21], and the same goes for Cu/zeolites. Furthermore, the adsorption strength of NO<sub>2</sub> is dependent on the metal species; for example, Fig. 8.6 shows the NO<sub>2</sub>-TPD experiment reported by Metkar et al. [11]. The NO<sub>2</sub>-TPD spectra indicate that NO<sub>2</sub> is more strongly bound to Cu/zeolite compared to Fe/zeolite [11]. The same result has been obtained by Tronconi et al. [22]. These NO<sub>2</sub>-TPD results are in line with the reaction order results that Cu/zeolite has larger negative NO<sub>2</sub> order than Fe/zeolite as is stated in the Sect. 8.2.3 and Table 8.1 [11].

Taking the above results into consideration, we can conclude that the oxidation of NO in the absence of NH<sub>3</sub> is strongly affected by the NO<sub>2</sub> adsorption strength which depends on the type of active metal used. In other words, the rate-determining step of the NO oxidation under NH<sub>3</sub> absent condition would be the NO<sub>2</sub> desorption process. Figure 8.7 shows NO oxidation scheme over metal ion-exchanged zeolite by assuming that NO oxidation proceeds with the redox cycle of the metal ions. As the states of the metal ions, both mononuclear and binuclear states were considered. In this figure, the desorption step of the adsorbed NO<sub>2</sub>, that is the reduction step of the metal ions from M<sup>n+</sup> to M<sup>(n-1)+</sup>, would probably be the slowest process, which should be determined by the type of metal.

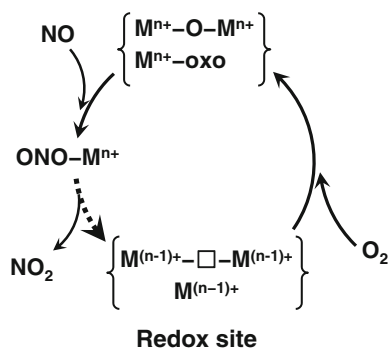
Regarding standard SCR reaction, on the other hand, the NO<sub>2</sub> desorption does not seem to be the rate-determining step because produced NO<sub>2</sub> should react with NH<sub>3</sub> immediately, which is elucidated and discussed in more detail in the other sections. Therefore, it is difficult to make a correlation between SCR activity and





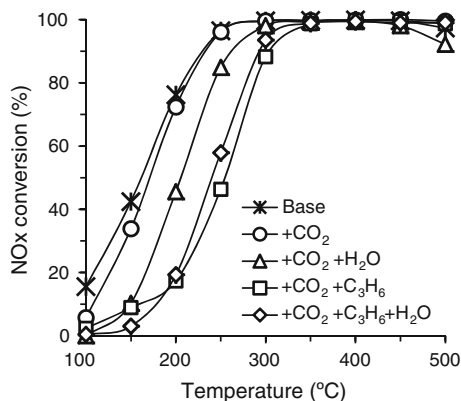
**Fig. 8.6** NO<sub>2</sub>-TPD experiments carried out on Fe- and Cu-zeolite catalysts. NO<sub>2</sub> adsorption = 150 °C; temperature ramp = 10 °C/min. Reprinted with permission from [11]

**Fig. 8.7** Schematic representation of catalytic cycle for NO oxidation reaction over metal-exchanged zeolite catalysts. Redox sites are associated with oxo-metal (isolated or binuclear) ion-exchanged sites



NO oxidation when different active metals are compared. Nevertheless, the author believes that the SCR activity is correlated with NO oxidation ability “in the presence of NH<sub>3</sub>”, simply because the fast SCR (NO/NO<sub>2</sub>/NH<sub>3</sub> system) rate is extremely faster than the standard SCR rate. The point is that NO oxidation conversion (NO<sub>2</sub> formation rate) under “NH<sub>3</sub> absent condition” does not necessarily correspond to NO oxidation ability under “NH<sub>3</sub> present condition,” i.e., standard SCR condition. Thus, the author presumes that although NO<sub>2</sub> is hard to be desorbed from Cu sites, Cu would have a greater potential to oxidize NO to NO<sub>2</sub> under NH<sub>3</sub> present condition. However, quantifying this ability is very difficult because the production rate of NO<sub>2</sub> adspecies can hardly be measured in the presence of NH<sub>3</sub>. Thus, an advanced technique which makes it possible to verify the assumption is desired.

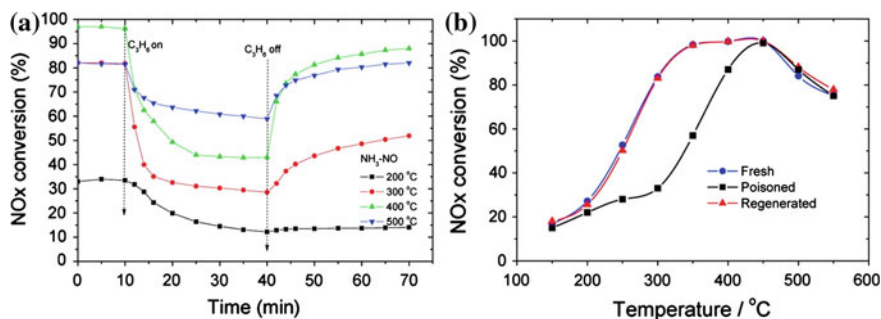
**Fig. 8.8** SCR conversion of Fe/BEA in the presence of 10 % CO<sub>2</sub>, 8 % H<sub>2</sub>O, and/or 333 ppm C<sub>3</sub>H<sub>6</sub>. Base gas composition: 0.1 % NO, 0.12 % NH<sub>3</sub>, and 8 % O<sub>2</sub> with the remainder N<sub>2</sub>



### 8.2.5 Effect of Coexisting Gases and Poisoning

Considering the practical use of SCR catalysts for diesel engines, we have to take into account the possible effects due to the presence of other compounds such as CO, CO<sub>2</sub>, H<sub>2</sub>O, HC, and the poisoning effect from SO<sub>2</sub> which are all present during the combustion of fuel. Figure 8.8 shows the standard SCR conversion of Fe/BEA in the presence of CO<sub>2</sub>, H<sub>2</sub>O, and C<sub>3</sub>H<sub>6</sub>. The base gas was 0.1 % NO, 0.12 % NH<sub>3</sub>, and 8 % O<sub>2</sub> with the remainder N<sub>2</sub>. When 10 % CO<sub>2</sub> was added to the base gas, the NO<sub>x</sub> conversion slightly declined, which indicates that CO<sub>2</sub> has a little inhibitory effect on the SCR reaction. Next, the addition of 8 % H<sub>2</sub>O and/or 333 ppm C<sub>3</sub>H<sub>6</sub> to the base + CO<sub>2</sub> feed further lowered the NO<sub>x</sub> conversion. Here, the addition of 333 ppm C<sub>3</sub>H<sub>6</sub> decreased the activity much more than 8 % H<sub>2</sub>O did, despite the low HC concentration. Additionally, the NO<sub>x</sub> conversion under the presence of both 333 ppm C<sub>3</sub>H<sub>6</sub> and 8 % H<sub>2</sub>O was higher than that in presence of 333 ppm C<sub>3</sub>H<sub>6</sub> only, suggesting that H<sub>2</sub>O suppresses the strong inhibition by C<sub>3</sub>H<sub>6</sub>. Thus, the degree of inhibitory effect on the SCR reaction follows the order: C<sub>3</sub>H<sub>6</sub> > H<sub>2</sub>O > CO<sub>2</sub>.

Li et al. [23] and He et al. [24] have investigated the effect of the regeneration temperature on the Fe/ZSM-5 and Fe/BEA catalysts, respectively, after C<sub>3</sub>H<sub>6</sub> poisoning. Figure 8.9a shows the change in the NO<sub>x</sub> conversions in response to the presence (on) and absence (off) of C<sub>3</sub>H<sub>6</sub> at several temperatures over Fe/ZSM-5 [23]. When 0.1 % C<sub>3</sub>H<sub>6</sub> was added to the feed (10 min), all the conversions decreased, but the extent of decrease differed with the temperature. Then, after the removal of C<sub>3</sub>H<sub>6</sub> from the feed (40 min), all the conversions except at 200 °C recovered. However, the extent of recovery depended on the temperature; with no improvement observed at 200 °C, while the conversions recovered to some extent at 300 and 400 °C. At 500 °C, the NO<sub>x</sub> conversion completely recovered to the initial conversion level before the addition of C<sub>3</sub>H<sub>6</sub>. Figure 8.8b shows the comparison of SCR activities of fresh, poisoned, and regenerated samples [23]. The term “poisoned” means that the catalyst was pretreated with C<sub>3</sub>H<sub>6</sub> containing gas



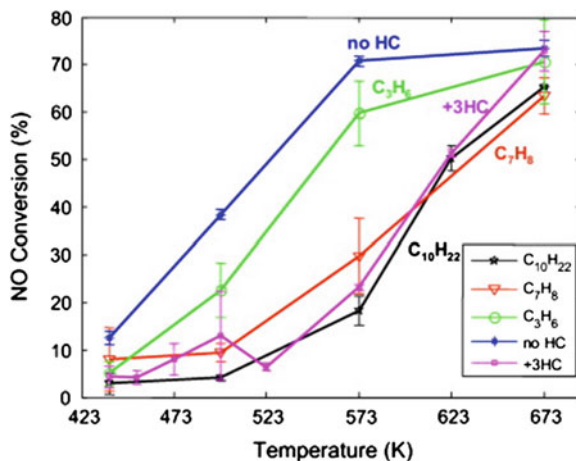
**Fig. 8.9** **a** The change in NO<sub>x</sub> conversions with response to the C<sub>3</sub>H<sub>6</sub> on and off at 200–500 °C for Fe/ZSM-5. **b** NO<sub>x</sub> conversions of fresh, C<sub>3</sub>H<sub>6</sub> poisoned (at 200 °C), and regenerated (in 10 % O<sub>2</sub> at 550 °C for 30 min) samples. Gas composition = 0.1 % NO, 0.1 % NH<sub>3</sub>, 0.1 % C<sub>3</sub>H<sub>6</sub> (when used), 5 % O<sub>2</sub>, and 2 % H<sub>2</sub>O with remainder He. Reprinted with permission from [23]

at 200 °C, while “regenerated” means that the poisoned catalyst was treated at 550 °C in presence of 10 % O<sub>2</sub>. It can be seen that the NO<sub>x</sub> conversion of the poisoned sample clearly decreased at 200–400 °C. However, the regenerated sample showed almost similar activity to the fresh one, indicating that the catalyst can be completely regenerated by the 550 °C treatment. In addition, an FT-IR study suggested that the hydrocarbon oxygenates such as formate-, acetate-, and nitrogen-containing organic compounds were created on the surface [23]. Thus, they concluded that the major cause for the deactivation was the carbonaceous deposition onto Fe<sup>3+</sup> sites which are responsible for the oxidation of NO to NO<sub>2</sub>. In fact, they have also confirmed that the NO oxidation activity was significantly inhibited by the C<sub>3</sub>H<sub>6</sub> poisoning [23].

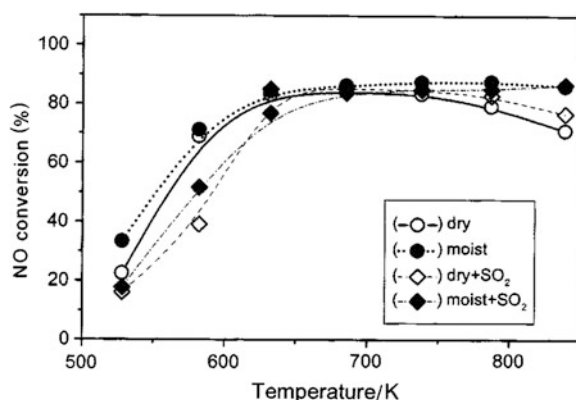
Malpartida et al. [25] have reported the effect of HC types on the SCR reactivity using Fe/ZSM-5. Figure 8.10 shows NO conversion when different types of HCs (C<sub>3</sub>H<sub>6</sub>, C<sub>7</sub>H<sub>8</sub>, C<sub>10</sub>H<sub>22</sub>) coexisted [25]. The addition of any type of HC led to a decrease in the NO conversion, but its effect was different for different HCs; the rate of decline was limited in the case of C<sub>3</sub>H<sub>6</sub> but was more significant in the presence of toluene (C<sub>7</sub>H<sub>8</sub>) and decane (C<sub>10</sub>H<sub>22</sub>). In situ FT-IR observed the deposition of C-species, and its quantity was dependent on the HCs; C<sub>10</sub>H<sub>22</sub> > C<sub>7</sub>H<sub>8</sub> > C<sub>3</sub>H<sub>6</sub>, which is in the reverse order with respect to the NO conversion [25]. Thus, they concluded that the most important effect from HC poisoning at low temperature is the competitive adsorption between the hydrocarbon molecules and NH<sub>3</sub> onto the active Fe sites [25].

Next, the effect of SO<sub>2</sub> poisoning and regeneration is presented. Figure 8.11 shows the influence of H<sub>2</sub>O and SO<sub>2</sub> on the SCR conversion over Fe/ZSM-5 [26]. It is evident that SO<sub>2</sub> exerts a poisoning influence at low temperature both in case of dry as well as moist feed. Remarkably, this effect is reversed at a high temperature, i.e., above 450 °C (723 K), the NO conversion is the highest even in the presence of SO<sub>2</sub>.

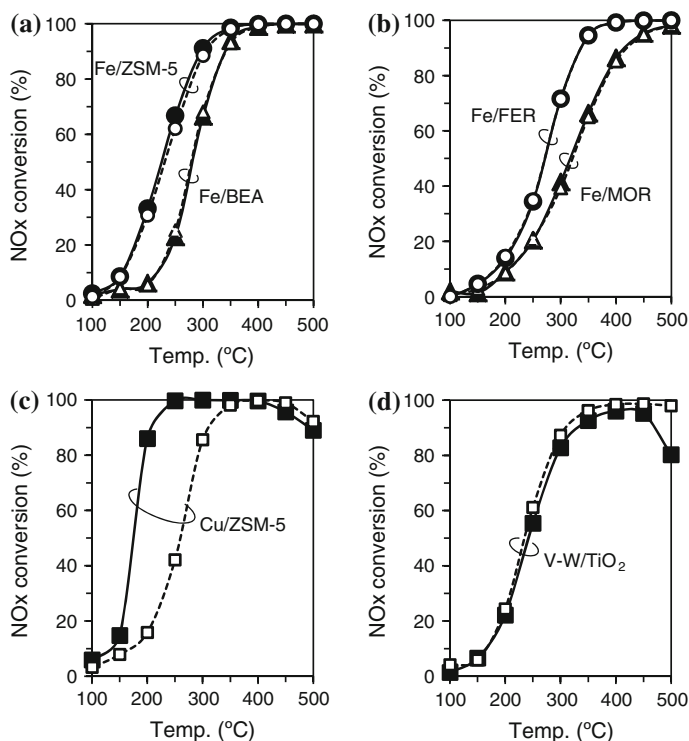
**Fig. 8.10** SCR conversion of Fe/ZSM-5 as a function of the temperature for different HC composition: without HC, 85 ppm  $C_3H_6$ , 85 ppm  $C_7H_8$ , 85 ppm  $C_{10}H_{22}$ , and 85 ppm mixed HCs (17 ppm  $C_3H_6$ , 25 ppm  $C_7H_8$  and 43 ppm  $C_{10}H_{22}$ ). Base gas composition: 150 ppm NO, 150 ppm  $NH_3$ , 300 ppm CO, 14 %  $O_2$ , 4 %  $CO_2$ , and 1 %  $H_2O$  with remainder Ar. Reprinted with permission from [25]



**Fig. 8.11** Influence of  $H_2O$  and  $SO_2$  on the NO conversion over Fe/ZSM-5. Dry condition: 0.1 % NO, 0.1 %  $NH_3$ , and 2 %  $O_2$  with the remainder He. Moist condition: as dry, with 2.5 %  $H_2O$  added, '+ $SO_2$ ', with 200 ppm  $SO_2$  added. Reprinted with permission from [26]



Finally, the effect of regeneration on the  $SO_2$ -poisoned catalysts is presented [27]. First, hydrothermally aged samples (700 °C for 5 h) were poisoned by a feed containing 30 ppm  $SO_2$  until the adsorption saturated at 300 °C, and was then regenerated under standard SCR condition by maintaining at 550 °C for 10 min. Figure 8.12 shows the  $NO_x$  conversions before the  $SO_2$  poisoning and after the  $SO_2$  regeneration for Fe/zeolites, Cu/ZSM-5, and V-W/TiO<sub>2</sub>. Obviously, all the regenerated Fe/zeolites maintained equivalent activity with those free from  $SO_2$ . Meanwhile, the Cu/ZSM-5 catalyst greatly deteriorated even after the regeneration. This suggests that the major cause of the deterioration is not the zeolite structure but the type of ion-exchanged metal. Therefore, Fe/zeolites possess a higher endurance for  $SO_2$  poisoning than Cu/zeolites in this case. In addition,



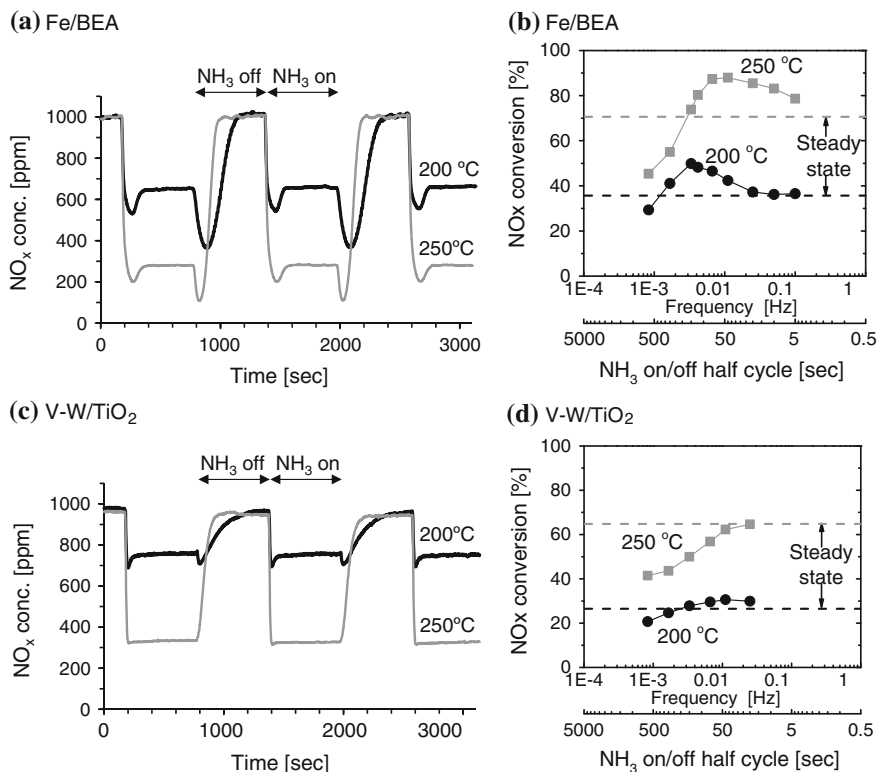
**Fig. 8.12** NO<sub>x</sub> conversions of hydrothermally aged (700 °C for 5 h) Fe/zeolites with different structures (a, b), Cu/ZSM-5 (c), and V–W/TiO<sub>2</sub> (d) before SO<sub>2</sub> poisoning (filled symbols) and after SO<sub>2</sub> poisoning and regeneration (open symbols). SCR feed: 0.1 % NO, 0.12 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, and 8 % H<sub>2</sub>O with remainder N<sub>2</sub>. SO<sub>2</sub> poisoning and regeneration: poisoning under 30 ppm SO<sub>2</sub> + SCR feed at 300 °C for 20 min, followed by regenerating under SCR feed at 550 °C for 10 min

V–W/TiO<sub>2</sub> shows also high endurance for SO<sub>2</sub>. Interestingly, regenerated V–W/TiO<sub>2</sub> has greater activity than SO<sub>2</sub> free one at 500 °C. This is probably because the SO<sub>2</sub> poisoning inactivates aggregated V species which provoke NH<sub>3</sub> unselective oxidation at high temperature.

## 8.3 Transient Reaction Analysis

### 8.3.1 Periodic NH<sub>3</sub> Supply

As the composition and the concentration of diesel exhaust gases vary significantly depending on the engine operation, it is quite important to understand the transient behavior of NO<sub>x</sub> reduction following NH<sub>3</sub> supply and shutoff. In this section, the effect of the periodical supply of NH<sub>3</sub> on the NO<sub>x</sub> reduction behavior is presented.



**Fig. 8.13** NO<sub>x</sub> concentration (a, c) and average NO<sub>x</sub> conversion (b, d) under periodic supply of NH<sub>3</sub> with Fe/BEA (a, b) and V-W/TiO<sub>2</sub> (c, d) catalysts. Gas composition = 0.1 % NO, 0.2 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, and 8 % H<sub>2</sub>O with the remainder N<sub>2</sub>; catalyst weight = 1 g; flow rate = 3.5 l/min

As a first test, symmetrical NH<sub>3</sub> on/off cycles were conducted by changing the switching time from 5/5 to 600/600 s/s at 200 and 250 °C. Figure 8.13a shows the outlet NO<sub>x</sub> concentration with the Fe/BEA zeolite catalyst under 600/600 s switching condition. The feed gas was a mixture having the composition: 0.1 % NO, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, 8 % H<sub>2</sub>O, and the remainder N<sub>2</sub> with a periodical supply of 0.2 % NH<sub>3</sub>. When NH<sub>3</sub> was added to the feed, the NO<sub>x</sub> concentration quickly decreased due to the SCR reaction, went through a minimum, and then slowly approached a steady-state level. When NH<sub>3</sub> was removed from the feed, the NO<sub>x</sub> concentration was reduced to a greater degree than the steady-state level, went through a minimum and then reached the inlet NO<sub>x</sub> value. Similar results have been reported by many researchers [4, 5, 18, 28–30]. This indicates that the SCR reaction using adsorbed NH<sub>3</sub> continues even after the NH<sub>3</sub> feed is shutoff, and furthermore, the reaction is accelerated in the absence of gaseous NH<sub>3</sub>. In other words, SCR is inhibited by the presence of gaseous NH<sub>3</sub> and/or by a high coverage of adsorbed NH<sub>3</sub>. In Fig. 8.13a, one can see that the degree of transient NO<sub>x</sub>

reduction is pronounced at a lower temperature. This can be due to the following two factors: First, the amount of adsorbed NH<sub>3</sub> available for the SCR reaction increases with decrease in the temperature [4, 28, 30, 31] and second, the inhibiting effect of gaseous NH<sub>3</sub> and/or high NH<sub>3</sub> coverage is intensified at a lower temperature [4].

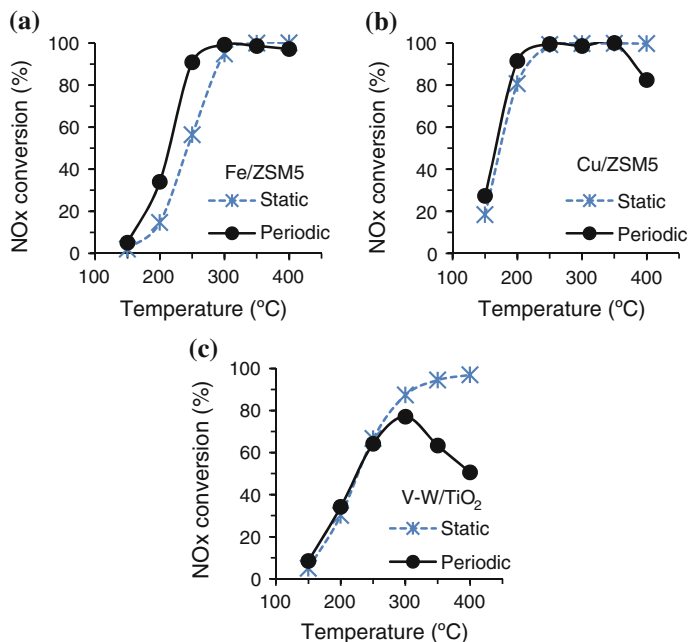
Figure 8.13b shows the average NO<sub>x</sub> conversion with change in the NH<sub>3</sub> on/off cycle time. Interestingly, under certain conditions the average NO<sub>x</sub> conversion exceeded the steady-state conversion. It suggests that an intermittent supply of NH<sub>3</sub> is more effective than a continuous supply. Additionally, because of the difference in the NH<sub>3</sub> adsorption capacity, the maximum conversion at 200 °C is shifted to longer cycle time (smaller frequency) as compared to that at 250 °C. Thus, depending on the temperature there is an optimum NH<sub>3</sub> on/off condition. The optimum condition would be varied with several factors such as NH<sub>3</sub> storage capacity and W/F. Recently, the contributions of these parameters have also been elucidated by fitting procedure of simulation studies [30, 32, 33].

Figure 8.13c shows the NO<sub>x</sub> profile with a commercial V–W/TiO<sub>2</sub> catalyst. In this case, the NO<sub>x</sub> concentration monotonically decreased and increased in response to the NH<sub>3</sub> on/off switching. The transient NO<sub>x</sub> removal behavior was hardly observed in this case. This is probably due to the low NH<sub>3</sub> adsorption capacity of the V-based catalyst, which has been verified later. Figure 8.13d shows the average NO<sub>x</sub> conversions with the V–W/TiO<sub>2</sub> catalyst versus the NH<sub>3</sub> on/off cycle time. The average conversions were mostly less than the steady-state level.

Next, asymmetric NH<sub>3</sub> on/off switching (on/off = 60/120 s) with variation of the temperature (150–400 °C) were conducted. Figure 8.14a–c shows the average NO<sub>x</sub> conversions for the Fe/ZSM-5, Cu/ZSM-5, and V–W/TiO<sub>2</sub> catalysts. In case of the Fe/ZSM-5 catalyst (Fig. 8.14a), the NO<sub>x</sub> conversions under the periodic condition were higher than those under the steady-state condition below 300 °C, which is in conformity with the result depicted in Fig. 8.13b. Similar enhancement in the NO<sub>x</sub> reduction in the low temperature region was observed over H–ZSM-5 by Wallin et al. [28]. They have reported that NO<sub>x</sub> reduction was enhanced by up to five times as compared to a continuous supply of NH<sub>3</sub> by changing the NH<sub>3</sub> pulse condition at 200–300 °C [28].

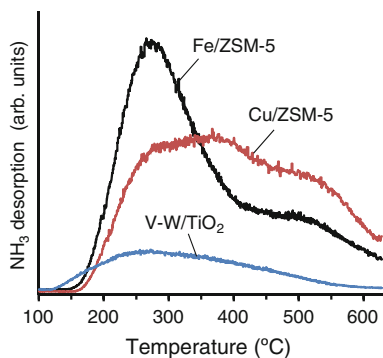
The same observation holds true for the Cu/ZSM-5 catalyst (Fig. 8.14b) below 250 °C. However, at 400 °C the periodic conversion is less than the steady-state one. The reason for this lower activity for the periodic condition is probably due to the decrease of the reaction selectivity between NO and NH<sub>3</sub> [34, 35]. As shown in Fig. 8.1b, Cu/ZSM-5 exhibits higher activity for NH<sub>3</sub> oxidation than Fe/ZSM-5 and V–W/TiO<sub>2</sub>. Thus, it can be assumed that a part of the adsorbed NH<sub>3</sub> is consumed by O<sub>2</sub> under NH<sub>3</sub> off condition, leading to the lower activity for the periodic measurement.

Meanwhile, the periodic conversions with V–W/TiO<sub>2</sub> were roughly in accordance with the steady-state conversions at the low temperatures ( $\leq 250$  °C). However, in the high temperature region ( $\geq 300$  °C), the periodic conversions greatly decreased despite the fact that the steady-state conversions monotonically increased with the temperature. This is because the NH<sub>3</sub> adsorption capacity



**Fig. 8.14** Average NO<sub>x</sub> conversion for **a** Fe/ZSM-5, **b** Cu/ZSM-5, and **c** V-W/TiO<sub>2</sub> under periodic and static supply of NH<sub>3</sub>. Catalyst weight = 1 g; flow rate = 3.5 l/min. Periodic: NH<sub>3</sub> on/off = 60/120 s/s; 0.02 % NO, 0.073 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, and 8 % H<sub>2</sub>O with the remainder N<sub>2</sub>. Static: 0.05 % NO, 0.06 % NH<sub>3</sub>, 8 % O<sub>2</sub>, 10 % CO<sub>2</sub>, and 8 % H<sub>2</sub>O with the remainder N<sub>2</sub>

**Fig. 8.15** NH<sub>3</sub>-TPD spectra for Fe/ZSM-5, Cu/ZSM-5 and V-W/TiO<sub>2</sub> catalysts. NH<sub>3</sub> adsorption = 150 °C; temperature ramp = 20 °C/min; W/F = 3.3 g min/l

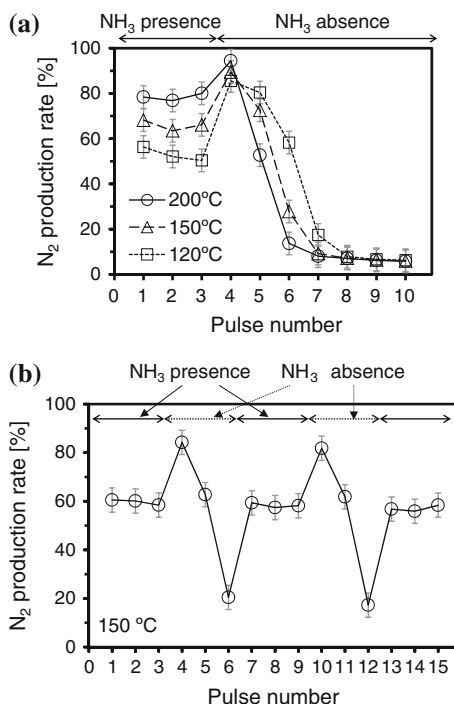


available for the transient SCR reaction in case of the V-W/TiO<sub>2</sub> catalyst is low, especially at the high temperature. To confirm this, NH<sub>3</sub>-TPD spectra are presented in Fig. 8.15. In fact, the amount of desorbed NH<sub>3</sub> from the V-W/TiO<sub>2</sub> catalyst is very little compared to the zeolite-based catalysts.



**Fig. 8.16** N<sub>2</sub> production rate by NO pulse reaction in the presence and absence of NH<sub>3</sub> feed over Fe/ZSM-5.

Continuous gas flow = 0.1 l/min, either 0 or 0.04 % NH<sub>3</sub>, and 10 % O<sub>2</sub> with remainder He; NO pulse = 0.34 ml; catalyst weight = 0.25 g. Reprinted with permission from [4]

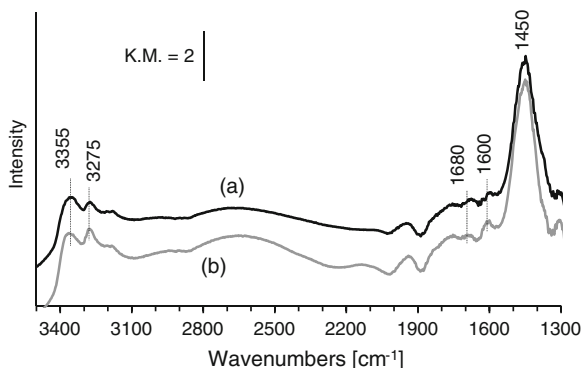


### 8.3.2 NO Pulse Reaction

To investigate the catalytic effect of Fe/ZSM-5 on the transient NO<sub>x</sub> reduction in more detail, the NO pulse reaction test was conducted with monitoring of the N<sub>2</sub> production [4]; NO pulses were introduced to a continuous gas flow consisting of either 0 or 400 ppm NH<sub>3</sub>, 10 % O<sub>2</sub>, with the remainder He. Figure 8.16a shows the N<sub>2</sub> production rates in the presence and absence of the NH<sub>3</sub> feed. In the presence of NH<sub>3</sub> (pulses 1–3), the N<sub>2</sub> production rates were almost constant and increased with increasing temperature. When NH<sub>3</sub> was removed from the feed, the amount of N<sub>2</sub> increased (pulse 4) and then decreased (pulses 5–10), suggesting that the SCR reaction between the adsorbed NH<sub>3</sub> and pulsed NO is promoted in the absence of NH<sub>3</sub>. The total amount of N<sub>2</sub> produced in the absence of NH<sub>3</sub> (pulses 4–10) which corresponds to the amount of NH<sub>3</sub> adsorbed is larger at lower temperatures [4, 31].

Figure 8.16b shows the N<sub>2</sub> production rates when the presence and absence of NH<sub>3</sub> is repeated at the interval of three pulses. The N<sub>2</sub> production rates in the first NH<sub>3</sub> absent region (pulses 4 and 10) were higher than those in the NH<sub>3</sub> present regions; this suggests that the promotional effect of the absence of NH<sub>3</sub> is repeatable. This is in conformity with the behavior observed during the periodical NH<sub>3</sub> supply test as shown in Fig. 8.13a.

**Fig. 8.17** Difference FT-IR spectra over Fe/BEA in presence of 730 ppm NH<sub>3</sub> flowing at 150 °C (a), and after the purge with 10 % O<sub>2</sub> at 150 °C (b)



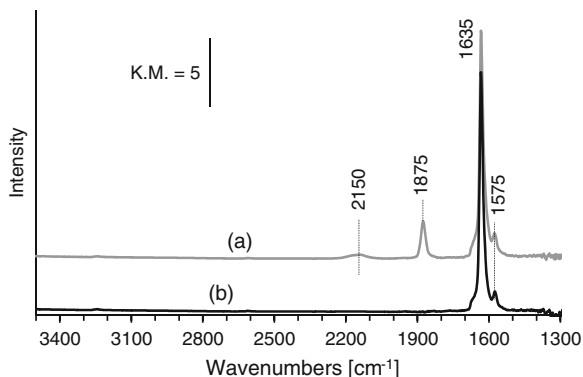
### 8.3.3 *In Situ FT-IR Analysis*

To trace the surface-adsorbed species during the transient NO<sub>x</sub> reduction, *in situ* FT-IR analysis was applied. Analyzing the transient change of these adsorbates would help in understanding the SCR mechanism and identifying the rate-determining step.

Before the transient reaction analysis, the steady-state adsorption species formed when NH<sub>3</sub>/N<sub>2</sub> or NO + O<sub>2</sub>/N<sub>2</sub> was passed over the Fe/BEA catalyst have been presented. Figure 8.17a shows the difference spectra before and after 730 ppm NH<sub>3</sub> flow at 150 °C. Prior to the NH<sub>3</sub> adsorption, the sample was pre-treated with 10 % O<sub>2</sub> for 30 min at 550 °C followed by cooling it down to 150 °C. A strong band at 1,450 cm<sup>-1</sup> and a weak band at 1,680 cm<sup>-1</sup> can be assigned to the symmetric and asymmetric bending vibrations respectively, of chemisorbed NH<sub>4</sub><sup>+</sup> on the Brønsted acidic sites [12, 36, 37]. Meanwhile, weaker bands at 1,300 and 1,600 cm<sup>-1</sup> can be assigned to the symmetric and asymmetric bending vibrations respectively, of coordinately linked NH<sub>3</sub> to Lewis acidic sites [12, 36, 37]. The bands at 3,275 and 3,355 cm<sup>-1</sup> can be assigned to the N–H stretching vibration of NH<sub>4</sub><sup>+</sup> ions with the three hydrogen atoms bonded to the three oxygen ions of the AlO<sub>4</sub> tetrahedra (3H structure) [12, 36, 38]. The broad band between 2,600 and 2,900 cm<sup>-1</sup> can be attributed to the N–H stretching vibration of physisorbed NH<sub>3</sub> [12, 36, 37]. Figure 8.17b shows the NH<sub>3</sub>-adsorbed spectra after purging with 10 % O<sub>2</sub>/N<sub>2</sub> at 150 °C. There is no change after the O<sub>2</sub> purge, suggesting that neither oxidation nor desorption of adsorbed NH<sub>3</sub> occurred at this temperature.

Figure 8.18a shows the difference spectra before and after NO + O<sub>2</sub> flow. After pretreatment with 10 % O<sub>2</sub> at 550 °C, the sample was treated with a flow of 1,000 ppm NO, 10 % O<sub>2</sub> at 150 °C. A strong sharp band was observed at 1,635 cm<sup>-1</sup> which can be assigned to nitro (NO<sub>2</sub>) group on the ion-exchanged Fe sites [36, 39–41]. Thus, NO was oxidized to NO<sub>2</sub> over the Fe sites and adsorbed

**Fig. 8.18** Difference FT-IR spectra over Fe/BEA in presence of 1,000 ppm NO and 10 % O<sub>2</sub> flowing at 150 °C (a), and after the purge with 10 % O<sub>2</sub> at 150 °C (b)

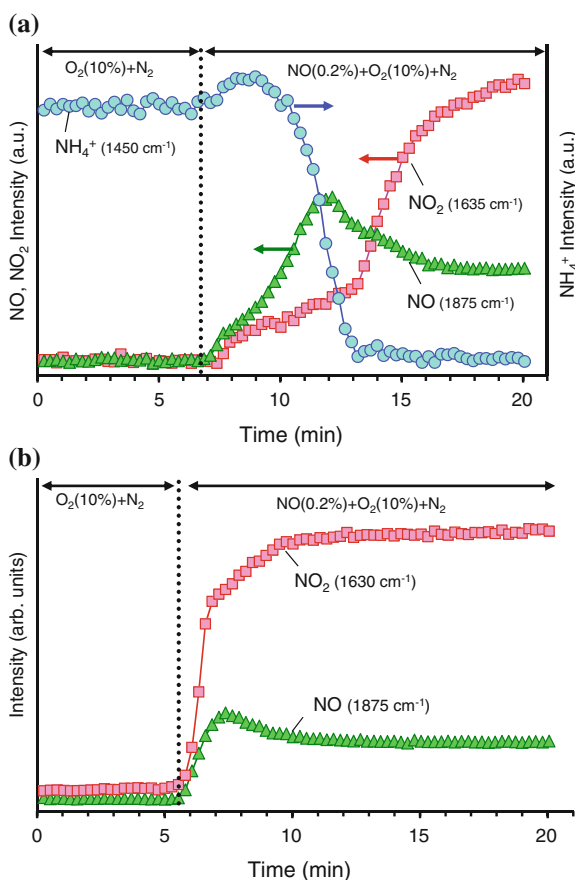


there. Small bands at 1,575 and 1,875  $\text{cm}^{-1}$  can be assigned to nitrate and NO species, respectively, on the Fe sites [36, 39–41]. Additionally, a very weak broad band at 2,150  $\text{cm}^{-1}$  could be assigned to  $\text{NO}^+$  species adsorbed on the Brønsted acidic sites [36, 39–41]. Figure 8.18b shows the  $\text{NO}_x$ -adsorbed spectra after purging with 10 % O<sub>2</sub> at 150 °C. The bands at 2,150 and 1,875  $\text{cm}^{-1}$  disappeared, and only the  $\text{NO}_2$  and nitrate bands remained.

Next, a transient reaction test was carried out by introducing NO + O<sub>2</sub> onto NH<sub>3</sub> preadsorbed on the Fe/BEA catalyst at 150 °C. Figure 8.19a shows the peak intensity profiles of the three main bands; 1,450  $\text{cm}^{-1}$  (NH<sub>4</sub><sup>+</sup>), 1,635  $\text{cm}^{-1}$  (NO<sub>2</sub>), and 1,875  $\text{cm}^{-1}$  (NO). When 0.2 % NO was added to 10 % O<sub>2</sub> + N<sub>2</sub> feed (7 min), the NH<sub>4</sub><sup>+</sup> band slightly increased and then decreased with increase in the NO and NO<sub>2</sub> bands. After the disappearance of the NH<sub>4</sub><sup>+</sup> band (13 min), the NO and NO<sub>2</sub> bands reached a steady-state level (20 min). Interestingly, the NO band went through a maximum at around 12 min, whereas the NO<sub>2</sub> band increased sharply after the NH<sub>4</sub><sup>+</sup> band vanished ( $\geq 13$  min). Thus, the NO<sub>2</sub> band was lower than the NO band in the presence of the NH<sub>4</sub><sup>+</sup> band, but it exceeded after the disappearance of the NH<sub>4</sub><sup>+</sup> band. In other words, the band intensities between NO and NO<sub>2</sub> reversed before and after the disappearance of the NH<sub>4</sub><sup>+</sup> band.

Figure 8.19b shows the intensity profiles of the NO and NO<sub>2</sub> bands in the absence of preadsorbed NH<sub>3</sub>. In this case, the NO<sub>2</sub> band intensity remained constantly higher than the NO band, which is consistent with the steady-state result observed in Fig. 8.18a. Comparing Fig. 8.19a and b we can make the following hypotheses: While the SCR reaction with using adsorbed NH<sub>3</sub> was occurring, (a) NO<sub>2</sub> formation from the oxidation of NO is inhibited by adsorbed NH<sub>4</sub><sup>+</sup>, and/or (b) the NO<sub>2</sub> produced is immediately consumed via the reaction with the adsorbed NH<sub>4</sub><sup>+</sup>. In any case, it could be said from this result that the rate-determining step of the surface SCR reaction would be the formation of NO<sub>2</sub> adspecies by NO oxidation over the active Fe sites.

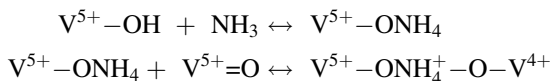
**Fig. 8.19** IR peak intensity profiles of NO, NO<sub>2</sub>, and NH<sub>4</sub><sup>+</sup> bands at 150 °C. 0.2 % NO was added to 10 % O<sub>2</sub> feed in the presence of preadsorbed NH<sub>3</sub> (a), or in the absence of preadsorbed NH<sub>3</sub> (b)



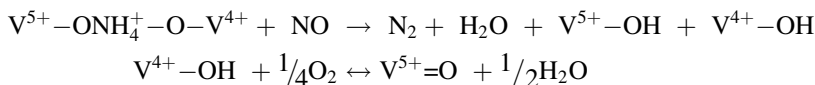
## 8.4 Reaction Mechanisms

### 8.4.1 Vanadium-Based Catalysts

In this section, some mechanistic implications of the SCR reaction over vanadium catalysts have been discussed based on the previous literature. The standard SCR reaction over V-based catalysts is generally considered to occur between the strongly adsorbed NH<sub>3</sub> and gaseous or weakly adsorbed NO [42–49]. The proposed reaction mechanisms often involve two adjacent vanadium species, namely the terminal oxygen species, i.e., V = O (redox sites), and the hydroxyl group, i.e., V–OH (Brønsted acidic sites). Topsøe et al. [44–46] suggested that the reaction scheme involves the adsorption of NH<sub>3</sub> on the Brønsted acidic sites (V<sup>5+</sup>–OH) followed by activation of adsorbed NH<sub>3</sub> via reaction at the redox sites (V<sup>5+</sup> = O):



This activated form of NH<sub>3</sub> reacts with gaseous or weakly adsorbed NO, producing N<sub>2</sub> and H<sub>2</sub>O, and leading to partially reduced state (V<sup>4+</sup>–OH). This reduced species could be reoxidized by oxygen to the V<sup>5+</sup>=O species.

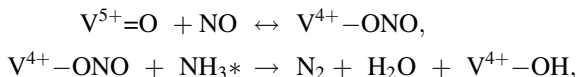


Topsøe et al. [44–46] reported that under high O<sub>2</sub> concentration condition (>1 %), the NH<sub>3</sub> activation step is fast and equilibrated, and thus the rate-limiting step is the reaction of NO with activated NH<sub>4</sub><sup>+</sup>.

Kamata et al. [48] estimated the ratio of the redox sites (V<sup>5+</sup>=O) to the Brønsted acidic sites (V<sup>5+</sup>–OH) by steady-state kinetic analysis. The relative amount of V<sup>5+</sup>=O sites varied from ~0.1 to ~0.4 with the partial pressure of O<sub>2</sub>, indicating that the number of V<sup>5+</sup>=O sites are less than the number of V<sup>5+</sup>–OH sites.

Roduit et al. [1] proposed a global kinetic model for the standard SCR reaction based on V-based catalysts. The kinetic model accounts for three different reactions and intraparticle diffusion. The three reactions are Langmuir–Hinshelwood; LH-type SCR, Eley–Rideal; ER-type SCR, and direct NH<sub>3</sub> oxidation. The main SCR pathway proceeds via the ER-type mechanism, but in the low temperature region ( $T \leq 200$  °C), LH-type reaction occurs. Furthermore, at high temperatures ( $T \geq 300$  °C), NH<sub>3</sub> oxidation and intraparticle mass transfer also takes place [1].

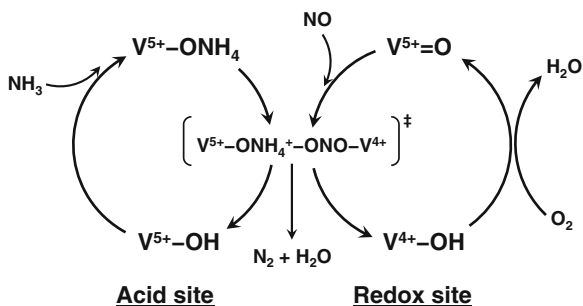
Tronconi et al. [50, 51] observed a transient improvement of SCR activity just after NH<sub>3</sub> shut off at low temperature. From this result, they pointed that the inhibitory effect of NH<sub>3</sub> cannot be accommodated by a simple ER kinetics assuming the reaction between adsorbed NH<sub>3</sub> and gaseous NO. They, then proposed that NO is oxidized by the V catalyst to a nitrite species, but the equilibrium is highly unfavorable and shifts to the right only in the presence of NH<sub>3</sub> [52]. The NH<sub>3</sub> which adsorbs on nearby acidic sites react with the nitrites to give N<sub>2</sub> and H<sub>2</sub>O via decomposition of unstable ammonium nitrite intermediates, for example, according to



where NH<sub>3</sub><sup>\*</sup> represents adsorbed ammonia on the acidic sites. In this case, the inhibitory effect of NH<sub>3</sub> could be more easily explained by either a competitive adsorption of NH<sub>3</sub> onto the V sites involved in NO activation or an adverse electronic interaction of the adsorbed NH<sub>3</sub> with the vanadium oxidizing centers [52].

Taking into account the above contributions, the SCR schemes at low temperature condition can be generalized as in Fig. 8.20. The catalytic cycle could be divided into two parts which takes place on; (a) acidic sites meant for NH<sub>3</sub>

**Fig. 8.20** Schematic representation of catalytic cycle for standard SCR reaction over vanadium-based catalyst. Acidic site and redox site are associated with  $V^{5+}-OH$  and  $V^{5+}=O$ , respectively



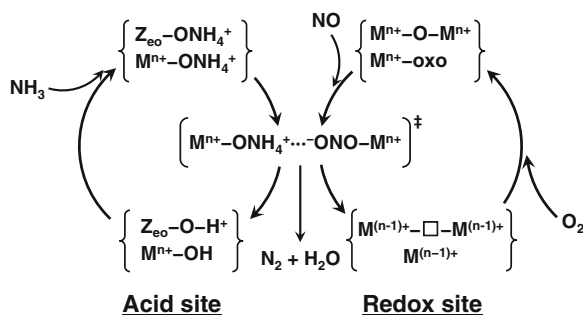
adsorption/activation and (b) redox sites meant for adsorbed  $NH_3$  activation and  $NO$  adsorption/activation. This reaction mechanism suggests the requirement of two types of surface vanadium atoms. Many papers have suggested that the  $NO_x$  conversion is correlated with the amount of  $V=O$  sites, and concluded that the redox site is indispensable to induce the SCR reaction [42, 44, 48, 49]. However, assuming the usage of transient SCR with preadsorbed  $NH_3$ , the amount of acidic sites would also play a key role, because very little  $NH_3$  can be adsorbed and available for the transient SCR reaction.

#### 8.4.2 Fe- or Cu-Exchanged Zeolite Catalysts

Numerous studies have been conducted to reveal the SCR reaction mechanism [4, 8, 18, 30, 35–37, 53–57] as well as active species [7, 58–66] for metal-exchanged zeolites. Recently, spectroscopic studies including EXAFS analysis revealed that a binuclear structure ( $M-O-M$ ) is created on the ion-exchanged sites [60–63]. Also, it has been commonly accepted that such binuclear species play an important role as active sites for several reactions such as  $N_2O/NO$  decomposition [67–70] and  $C_6H_6/CH_4$  oxidation by  $N_2O$  [71–74]. Komatsu et al. [5] hypothesized that paired  $Cu^{2+}$  is the active copper species in view of the relationship between the SCR activity and the copper concentration. Similarly, Chen and Sachtler [58], and Mauvezin et al. [59] assumed that an oxygen-bridged binuclear iron complex acts as the active site for the SCR reaction because  $CO$  consumption in  $CO$ -TPR was nearly half of the amount of  $Fe$ . Schwidder et al. [29, 64] and Brandenberger et al. [7, 65] suggested that not only mononuclear  $Fe$  but also the binuclear species contribute to the SCR reaction.

For the SCR mechanism, Delahay et al. [13, 75] proposed a  $Fe^{2+}/Fe^{3+}$  (or  $Cu^+/Cu^{2+}$ ) redox cycle as a part of the SCR scheme; the extra-framework oxygen on  $Fe^{3+}$  ( $Cu^{2+}$ ) oxo/hydroxo species reacts with  $NO$  to form a surface nitrogen oxide intermediate ( $Fe^{3+}-N_xO_y$  or  $Cu^{2+}-N_xO_y$ ). Then, this species reacts with  $NH_3$  to form  $N_2$  and  $H_2O$  with concomitant reduction of  $Fe^{3+}$  ( $Cu^{2+}$ ) to  $Fe^{2+}$  ( $Cu^+$ ) species. The  $Fe^{2+}$  ( $Cu^+$ ) species is reoxidized back to  $Fe^{3+}$  ( $Cu^{2+}$ ) oxo/hydroxo species by  $O_2$  [13, 75].

**Fig. 8.21** Schematic representation of catalytic cycle for standard SCR reaction over metal-exchanged zeolite catalysts. Acid sites are associated with Lewis or Brønsted sites at ion-exchanged metal or free proton sites. Redox sites are associated with oxo-metal (isolated or binuclear) ion-exchanged sites



Considering these previous reports, one can assume the following general SCR mechanism (Fig. 8.21): First, the reaction sites would be composed of acidic sites and redox sites similar to the V catalyst. However, in some cases, there is a possibility that one site can possess both the properties. For the acidic sites, the ion-exchanged metal sites (Brønsted or Lewis type) or residual free proton sites (Brønsted type) can be expected. Strong  $NH_3$  adsorption on such acidic sites during the SCR reaction has been reported in the literature [36, 37, 54]. Regarding the redox sites, the ion-exchanged metal cations (mononuclear and/or binuclear oxo species) can be expected. From TPR study, these sites are known to be easily reduced compared to extra-framework bulk metal oxides [63, 73, 76–78]. Also, Nobukawa et al. [73, 74] reported that very reactive oxygen atoms can be created over the binuclear Fe sites after  $N_2O$  treatment, and that it can desorb easily during a TPD run. This reactive oxygen atom in the nascent state is able to oxidize  $CH_4$  to  $CO/CO_2$  which is one of the difficult reactions to occur [73, 74].

By comparing the SCR scheme (Fig. 8.21) with  $NO$  oxidation scheme (Fig. 8.7), one can find similarities and differences. First of all, both reactions seem to progress via similar redox cycles of the active metal. However, judging from the reaction kinetic analysis discussed in Sects. 8.2.3 and 8.2.4, the rate-determining step of  $NO$  oxidation would be  $NO_2$  desorption process. As for the SCR reaction, on the other hand, the process prior to the formation of  $NO_2$  related adspecies (e.g., nitrite or nitrate intermediate) would be the rate-determining step, as is discussed in Sect. 8.3.3. Therefore, the slowest step in the redox cycles would be different in the two reactions.

For the SCR reaction,  $NO$  activation to form  $NO_2$  species would be the key step. For a deeper understanding of the SCR mechanism, further reaction kinetic analysis combined with tracing the reversible valence change of active metal is necessary. However, it can be said from the result of Sects. 8.3.1 and 8.3.2 that gaseous and/or high coverage  $NH_3$  inhibits the rate-determining step, and thus reaction rate can be

promoted by improving the reaction conditions such as adapting the periodic operation. Additionally, the acid site amount is also an important factor affecting the SCR activity especially for the periodic operation condition.

## 8.5 Conclusions

In this chapter, the mechanistic aspects of the NO–NH<sub>3</sub>–O<sub>2</sub> reacting system were addressed by using three conventional SCR catalysts, Cu or Fe ion-exchanged zeolites and V–W/TiO<sub>2</sub>. There had been several differences among the catalysts. For instance, the temperature profiles of SCR activity were different between the zeolite-based catalysts and V–W/TiO<sub>2</sub>. Regarding the tolerance for SO<sub>2</sub> poisoning, Fe/zeolite and V–W/TiO<sub>2</sub> showed high durability, while Cu/zeolite greatly deteriorated in the low temperature activity due to the different affinity between the active metals and sulfur.

Also, the periodic operation (NH<sub>3</sub> on/off cycling) had positive effect on the low temperature activity for Fe- and Cu-exchanged zeolites, because of strong inhibition by gaseous NH<sub>3</sub> and/or high NH<sub>3</sub> coverage. For V–W/TiO<sub>2</sub>, on the other hand, the periodic operation had not positive effect but negative especially under high temperature condition due to its lower NH<sub>3</sub> storage capacity.

However, the reaction mechanism could be depicted as common schemes which would be composed of (a) acidic sites meant for NH<sub>3</sub> adsorption/desorption, and (b) redox sites meant for NO oxidation and forming NO<sub>x</sub>–NH<sub>y</sub> intermediate species. Although the SCR activities of the three catalysts were not always correlated with NH<sub>3</sub>/NO oxidation abilities as well as acid site amount, each property plays an important role for explaining the reaction behaviors under high temperature and/or periodic conditions, as well as determining the reaction mechanisms. In situ FT-IR analysis of the SCR reaction between NO + O<sub>2</sub> and preadsorbed NH<sub>3</sub> over Fe/zeolite suggested that the rate-determining step of the surface SCR would be the formation of NO<sub>2</sub> adspecies by NO oxidation over Fe sites, which is an important insight to clarify the detailed SCR mechanism.

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