RESEARCH ARTICLE

Accelerated degradation of orange G over a wide pH range in the presence of $FeVO₄$

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HIGHLIGHTS

- The applicability of $FeVO₄$ extended the optimum pH range for heterogeneous Fenton process towards neutral conditions.
- The datas for the removal of OG in FeVO₄ systems conform to the Langmuir – Hinshelwood model.
- The irradiation of FeVO₄ by visible light significantly increases the degradation rate of OG due to the enhanced rates of the iron and vanadium cycles.

GRAPHIC ABSTRACT

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ABSTRACT

In this study, FeVO₄ was prepared and used as Fenton-like catalyst to degrade orange G (OG) dye. The removal of OG in an aqueous solution containing 0.5 $g \cdot L^{-1}$ FeVO₄ and 15 mmol L^{-1} hydrogen peroxide at pH 7.0 reached 93.2%. Similar rates were achieved at pH 5.7 $(k = 0.0471 \text{ min}^{-1})$, pH 7.0 $(k = 0.0471 \text{ min}^{-1})$ $= 0.0438$ min⁻¹), and pH 7.7 ($k = 0.0434$ min⁻¹). The FeVO₄ catalyst successfully overcomes the problem faced in the heterogeneous Fenton process, i.e., the narrow working pH range. The data for the removal of OG in FeVO₄ systems containing H_2O_2 conform to the Langmuir–Hinshelwood model $(R^2 = 0.9988)$, indicating that adsorption and surface reaction are the two basic mechanisms for OG removal in the FeVO₄–H₂O₂ system. Furthermore, the irradiation of FeVO₄ by visible light significantly increases the degradation rate of OG, which is attributed to the enhanced rates of the iron cycles and vanadium cycles.

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1 Introduction

Advanced oxidation processes (AOPs) have become the focus of increasing research over the past two decades due

to their ability to destroy toxic and biologically refractory organic contaminants in aqueous solutions [[1\]](#page-5-0). Otherwise known as Fenton system, such technologies generate reactive oxygen species, primarily in the form of the highly reactive and nonselective hydroxyl radical \bullet OH), which can oxidize organic pollutants. Aqueous mixtures of ferrous iron (Fe^{II}) and hydrogen peroxide (H₂O₂) are common present-day AOPs [[2](#page-5-0),[3\]](#page-5-0). However, the inherent setbacks of the homogeneous Fenton process, such as the difficulty in catalyst recovery, high sensitivity to pH, and

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formation of ferric sludge, have limited the development of heterogeneous catalysts [[4](#page-5-0)–[7](#page-5-0)]. In particular, the optimum pH value for Fenton oxidations is usually reported in the acidic range near pH 3 and the necessity to acidify the reaction medium limits the applicability of the Fenton process in environmental technology [[8\]](#page-5-0).

Owing to the limitations of the homogeneous Fenton method when used to treat municipal wastewater, heterogeneous Fenton and Fenton-like catalysts, such as α-Fe₂O₃, α- and γ-FeOOH [[9](#page-5-0)–[11](#page-5-0)], Fe₃O₄ [\[12,13\]](#page-5-0), and FeVO₄ [\[14\]](#page-5-0), have been studied extensively. when used to treat municipal wastewater, hetero-
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The reaction mechanism between iron-containing materials and H_2O_2 is described by the following reactions [[15](#page-5-0)]. α - and γ -FeOOH [9–11], Fe₃O₄ [12,13], and
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eaction mechanism between iron-containing mate-
 H_2O_2 is described by the following reactions [15].
 $\equiv \text{Fe}^{\text{III}} + \text{H}_2\text{O}_2 \rightarrow$

$$
\equiv \text{Fe}^{\text{III}} + \text{H}_2\text{O}_2 \rightarrow \equiv \text{Fe}^{\text{II}} + \bullet \text{OOH} + \text{H}^+ \tag{1}
$$

$$
\equiv Fe^{II} + H_2O_2 \rightarrow \equiv Fe^{III} + \bullet OH + OH^- \qquad (2)
$$

Furthermore, there are anions that combine with iron cation (e.g., V) to form heterogeneous Fenton-like catalysts [\[14\]](#page-5-0). Moreover, hydroxyl radicals are produced by catalytic reactions that involve V and H_2O_2 [[16,17](#page-5-0)]. These reactions are summarized below. The $\begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{pmatrix}$ and the area anions that combine with iron e.g., V) to form heterogeneous Fenton-like [14]. Moreover, hydroxyl radicals are produced vitic reactions that involve V and H₂O₂ [16,17]. e.g., V) to form heterogeneous Fenton-like
[14]. Moreover, hydroxyl radicals are produced
price reactions that involve V and H_2O_2 [16,17].
actions are summarized below.
 $\equiv V^V + H_2O_2 \rightarrow \equiv V^V + \bullet OOH + H^+$ (3)
 $\equiv V^W + H_2O_2$

$$
\equiv V^{V} + H_2O_2 \rightarrow \equiv V^{IV} + \bullet OOH + H^{+}
$$
 (3)

$$
\equiv V^{IV} + H_2O_2 \rightarrow \equiv V^{V} + \bullet OH + OH^{-}
$$
 (4)

In recent years, because of the mass production and wide use of dyes, the treatment of dye wastewater has attracted attention. This study highlights the degradation efficiency of azo dyes, particularly orange G (OG), which is widely used in the textile, pulp, and paper industries [\[18\]](#page-6-0). Although there are data on the degradation of azo dyes, little data exists on the kinetics and operation factors of degradation systems. In this study, the detailed investigation of the degradation of OG in the presence of $FeVO₄$ is discussed with the aim of extending the pH range of Fenton-like process toward neutral conditions. The reaction rates are determined under various operating conditions and the kinetic parameters are expressed in terms of a pseudo-first-order equation. In addition, the role of visible light is investigated.

2 Materials and methods

2.1 Materials

Analytical-grade ammonium metavandate, ferric nitrate 9 hydrate, and hydrogen peroxide (30%) were obtained from Sigma-Aldrich. Orange G was purchased from Hengrun Dyestuff Chemical Co. Ltd. (Guangzhou, China) and used without purification. All other reagents were from Sigma-Aldrich. The aqueous solutions used in the degradation reactions were prepared with deionized water obtained from a Millipore Milli-Q system. The stock solution of OG $(200 \text{ mg} \cdot \text{L}^{-1})$ was prepared with distilled water. The H_2O_2 solution (100 mmol· L^{-1}) was prepared fresh.

2.2 Catalyst preparation

FeVO4 was prepared following Ref [\[19](#page-6-0)]. Briefly, a 0.26 M iron nitrate solution was quickly mixed with a 4.27 mmol \cdot L⁻¹ ammonium metavanadate solution under continuous stirring and the mixture was maintained at 75°C for 1 h in a temperature-controlled water bath. The yellow precipitate was then washed with deionized water until the pH of the supernate turned neutral. Then, the precipitate was washed by acetone several times. Finally, the precipitate was air-dried and homogenized.

2.3 Experimental procedure

The batch degradation experiments were performed in a 250 mL beaker. Reaction mixtures were obtained by taking an appropriate amount of the OG stock solution and FeVO4, and were magnetically stirred for 30 min to complete the adsorption of OG on FeVO4. The final volume of the reaction mixture was 100 mL. The reaction was initiated when H_2O_2 was added to the solution. HCI and NaOH $(1 \text{ mol} \cdot \text{L}^{-1})$ were used to adjust the initial pH value of solution before adding FeVO₄. Continuous mixing was maintained throughout the experiments. At intermittent reaction times, a portion of the reacted solution was withdrawn and filtered for analysis. In all the experiments, the temperature of the solution was maintained at 25.0° C \pm 0.5°C. For the irradiation experiments, a solar simulator (CHF-XM35-500W) equipped with a 500 W Xe arc lamp (OSRAM, Germany) and an ultraviolet (UV)-cut filter was used as the visible light source. The reaction solutions were kept well mixed with a magnetic stirrer.

The samples for the total organic carbon (TOC) analysis were mixed with excess sodium azide to quench the radicals.

2.4 Determination of OG and TOC

The OG concentrations were determined using a UV–vis spectrophotometer (PerkinElmer, Lambda 20) with maximum absorption wavelength at 495 nm, and the TOC was measured using a TOC analyzer (Shimadzu TOC-5000A).

The analyses were repeated three times and the averages were then considered.

3 Results and discussion

3.1 Effect of $FeVO₄$ on the degradation of OG

In the absence of FeVO4, OG was stable in solution containing H_2O_2 . Then, OG was rapidly degraded at pH of

7.0 \pm 0.1 by the presence of both FeVO₄ and H₂O₂. Figure $1(a)$ shows the OG degradation vs the FeVO₄ concentration from 0.1 g \cdot L⁻¹ to 2.0 g \cdot L⁻¹ at pH 7.0 \pm 0.1 and initial concentrations of 20 mg·L⁻¹ OG and 15 mmol·L⁻¹ H₂O₂. The degradation of OG can be approximately modeled by pseudo-first-order kinetics. The curves $ln(C_0/C) = kt$, fitted to the data by linear regression, are showed in the inset of Fig. 1(a). In the equation, k is the rate constant, t is time, and C_0 and C are the concentrations of OG at 0 min or t min, respectively. It can be seen from Fig. 1(a) that with increasing FeVO₄ concentration, the decolorization rate of OG increased and reached a plateau at FeVO₄ concentration of 1.0 $g \cdot L^{-1}$. The corresponding pseudo-first-order rate constants (k) are 0.0094, 0.0222, 0.0438, 0.0695, and 0.0611 min–¹ , respectively. As expected, when the amount of catalyst increases, the OG removal rate increases, which is attributed to the increased number of active sites for H_2O_2 decomposition and adsorption of organic compounds [[20](#page-6-0)]. When catalyst loading exceeds a certain amount, many of the originally generated radicals are deactivated because of collisions, and the excess ground state $FeVO₄$ may cause scavenger effects [\[21,22\]](#page-6-0). Thus, the degradation rate of OG did not increase when the FeVO₄ concentration increased from 1.0 $g \cdot L^{-1}$ to 2.0 $g \cdot L^{-1}$. Although the optimal FeVO₄ concentration is $1.0 \text{ g} \cdot \text{L}^{-1}$, experiments were also conducted at a concentration of $0.5 \text{ g} \cdot \text{L}^{-1}$.

To evaluate the mineralization during the catalytic oxidation of OG, the TOC was monitored, as shown in Fig. 1(b). In terms of the TOC removal, as with the OG decolorization, a better performance is reached when the FeVO₄ concentration is 1.0 $g \cdot L^{-1}$. In addition, after reaction for 1 h, more than 90% of OG and less than 50% TOC were removed when the concentration of $FeVO₄$ exceeded $0.5 \text{ g} \cdot \text{L}^{-1}$ (Fig. 1(b)). Moreover, after reaction for 2 and 3 h with the solution containing $0.5 \text{ g} \cdot L^{-1}$ FeVO₄, the TOC removal was 57.4% and 64.0% (data not shown),

respectively, indicating that the OG intermediates were long-lived and the mineralization rate was slow.

3.2 Effect of H_2O_2 concentration on the degradation of OG

The effect of H_2O_2 concentration on the OG degradation in the FeVO₄–H₂O₂ system at pH 7.0 \pm 0.1 is shown in Fig. 2(a). The degradation rate of OG in solutions containing $0.5 \text{ g} \cdot L^{-1}$ FeVO₄ increases with increasing $H₂O₂$ concentration. For reaction time of 1 h, $H₂O₂$ concentrations of 5 mmol $\cdot L^{-1}$, 10 mmol $\cdot L^{-1}$, 15 mmol $\cdot L^{-1}$, 25 mmol·L⁻¹, and 40 mmol·L⁻¹ correspond to 75.4%, 81.0%, 93.2%, 99.3%, and 99.3% OG removal, respectively. As seen from reactions (1) – (4) , H_2O_2 can react with both iron species (≡Fe^{III}/Fe^{II}) and vanadate species (≡V^V/ V^{IV}) to generate \bullet OOH and \bullet OH. Increasing H₂O₂ concentration would benefit for increasing the rate of OH formation through the above two pathways or more. Consequently, above 90% OG was degraded after adding 15 mmol·L⁻¹ H₂O₂. However, \bullet OH is consumed by the excess H_2O_2 (reaction (5)). In this study, the optimum initial concentration of H_2O_2 is 15 mmol·L⁻¹. would benefit for i
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H₂O₂ + \bullet OH→HO⁴₂

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H_2O_2 + \bullet OH \rightarrow HO_2^{\bullet} + H_2O \tag{5}
$$

The 1 h treatment of OG by $FeVO_4-H_2O_2$ systems removes 44.0%, 46.4%, and 47.8% TOC from neutral wastewater at a concentration of 15 mmol· L^{-1} , 25 mmol·L⁻¹, and 40 mmol·L⁻¹ H_2O_2 , respectively (Fig. 2(b)). The mineralization of OG continued to occur by prolonging the reaction time. At the irradiation time of 3 h, TOC reduction of 70.8% was achieved in a neutral solution with 40 mmol \cdot L⁻¹ H₂O₂ and 0.5 g \cdot L⁻¹ FeVO₄.

3.3 Effect of initial OG concentration

A set of Fenton-like experiments at pH 7.0 ± 0.1 was performed in an aqueous suspension with 0.5 g·L⁻¹

Fig. 1 (a) Orange G (OG) removal vs time (b) total organic carbon (TOC) removal vs FeVO₄ concentration after 1 h reaction. [OG]₀ = 20 mg·L⁻¹, $[H_2O_2]_0 = 15$ mmol·L⁻¹, and pH = 7.0 \pm 0.1

Fig. 2 (a) OG removal vs time and (b) TOC removal vs H_2O_2 concentration after reaction for 1 h, 2h and 3h. [OG]₀ = 20 mg·L⁻¹, $[FeVO₄]_0 = 0.5 \text{ g} \cdot \text{L}^{-1}$, and pH = 7.0 \pm 0.1

FeVO₄, 15 mmol·L⁻¹ H₂O₂ and different initial OG concentrations, i.e., 5, 10, 20, 35, and 50 mg·L⁻¹. Figure 3 (a) shows that the degradation rate constant decreases with increasing initial concentration. At high initial concentration, two factors restrict the degradation of OG. First, the increased amount of OG may occupy many FeVO₄ active sites, which suppresses the generation of the oxidants and lowers the degradation rate. Second, the high OG concentration means more intermediate products would react with the radicals instead of OG. Hence, the degradation of OG decreases with increasing initial OG concentration.

The kinetics of the catalytic oxidation of organic compounds can be successfully modeled using the Langmuir–Hinshelwood (L–H) equation to describe the correlation between the degradation rate constants and initial concentrations [[21](#page-6-0),[23](#page-6-0),[24](#page-6-0)],

$$
k = k_{\text{ini}} \frac{K_{OG}}{1 + K_{OG} C_0},\tag{6}
$$

where

$$
\frac{1}{k} = \frac{1}{k_{ini}C_0} + \frac{1}{k_{ini}K_{OG}},\tag{7}
$$

and k is the pseudo-first-order rate constant (min^{-1}) , k_{ini} is the intrinsic reaction rate constant $(mg \cdot L^{-1} \cdot min^{-1})$, and K_{OG} is the L–H adsorption constant of OG over the FeVO₄ surface $(mg^{-1} L)$ in aqueous solutions. The plot of $1/k$ vs [OG]₀ gives the slope $(1/k_{\text{ini}})$ and intercept $(1/k_{\text{ini}}K_{\text{OG}})$ (Fig. 3(b)). A good linear correlation ($R^2 = 0.9988$) between $1/k$ and $[OG]_0$ was obtained, indicating that despite the poor adsorption of OG on the $FeVO₄$ surface, the reaction of OG with the surface OH radicals are important [\[25\]](#page-6-0). From the intercept and slope, the k_{ini} and

Fig. 3 The effect of initial OG concentrations: (a) Pseudo-first-order kinetics; (b) reciprocal of the pseudo-first-order rate constant vs the initial concentration of OG. [FeVO4]₀ = 0.5 g·L⁻¹, [H₂O₂] ₀ = 15 mmol·L⁻¹, and pH = 7.0 \pm 0.1

 K_{OG} values for OG are calculated at 1.614 mg·L⁻¹·min⁻¹ and $0.0605 \text{ mg}^{-1} \cdot L$, respectively.

3.4 Effect of pH on the degradation of OG

pH is an important parameter that affects Fenton-like reactions. To observe the effect of pH on the degradation of OG, several experiments were conducted in the same solution but at different pH of 4.2–11.0 and the results are shown in Fig. 4(a). The corresponding pseudo-first-order rate constants (k) are shown in Fig. 4(b). The degradation of OG depends on pH, and with increasing pH, k decreases gradually. Fenton-like systems have excellent degradation rates of wastewater with acidic pH; however, at circumneutral pH, the precipitation of $Fe₂O₃·nH₂O$ inhibits the recycling of Fe^{III}/Fe^{II} [[8](#page-5-0)].

As shown in Fig. 4(b), the degradation of OG by $FeVO₄/$ H_2O_2 systems at pH 5.7 ($k = 0.0471$ min⁻¹) and pH 7.7 ($k =$ 0.0434 min⁻¹) is similar to that of the original system (pH 7.0, $k = 0.0438$ min⁻¹) without pH adjustment, suggesting that the pH range was extended by the $FeVO₄$ catalyst. This is also supported by the k values of 0.0373 min⁻¹, 0.0284 min^{-1} , and 0.0259 min^{-1} for systems with pH 8.7, 9.2, and 9.8, respectively. This is attributed to V^{5+} in $FeVO₄$ being a Lewis acid that adsorbs OH⁻ in solution [\[26\]](#page-6-0). For better understanding the change of solution pH, the determination of pH value were carried out before and after the addition of FeVO4. As expected, the pH of the system decreased after adding FeVO4. For example, pH decreased from 7.0, 7.7, and 8.7 to 4.3, 5.2, and 5.4, respectively, after stirring the $FeVO₄$ solutions for 30 min. Undoubtedly, the decrease in the solution pH favors the degradation of pollutants in Fenton-like systems. On the other hand, the isoelectric point of $FeVO₄$ is reported at 4.15 [[14](#page-5-0)], which is lower than that of α -Fe₂O₃ (5.2–8.6), FeOOH (6.7 ± 0.2) and Fe₃O₄ (6.5 ± 0.2) [[27](#page-6-0)]. Thus, compared with other iron oxides, $FeVO₄$ has a low isoelectric point, which means the adsorption of negatively

charge on $FeVO₄$ surface would occur over pH 4.15. Therefore, the pH application range of $FeVO₄$ was wide from 4.0 to 9.0 (Fig. 4(b)). The enhanced reactivity in neutral solution displayed by $FeVO₄$ may allow it to be the better candidate for heterogeneous Fenton catalysts than other iron catalysts such as α -Fe₂O₃, FeOOH and Fe₃O₄.

3.5 Visible light irradiation and the degradation of OG

It has been reported the band gap of $FeVO₄$ was between 2.05 and 2.7 eV $[28-30]$ $[28-30]$ $[28-30]$ $[28-30]$ which means FeVO₄ can be a visible light photocatalyst. To evaluate the photocatalytic activity of FeVO4, the photodegradation of OG under visible light with and without $FeVO₄$ was investigated. Figure 5 shows the OG removal as a function of irradiation time. No significant change after 1 h irradiation was observed in the OG solution either with or without H_2O_2 , suggesting that the loss of OG owing to the visible light irradiation without catalyst can be ignored. By adding 0.5 g $\cdot L^{-1}$ FeVO₄, obvious photodegradation was observed with 97.8% OG removal after irradiation for 30 min. For comparison, in an identical experiment in the dark, only 75.2% OG was removed. These results suggest that visible light enhances the photocatalytic activity of $FeVO₄$ in the presence of H_2O_2 .

The recycling of $\equiv Fe^{III}$ from $\equiv Fe^{II}$ by reaction (2) and \equiv V^V from \equiv V^{IV} by reaction (4) are several orders of magnitude slower that reaction (1) and reaction (3), respectively. Reaction (2) and reaction (4) are considered as the rate-limiting steps of the iron cycling and vanadium cycling, respectively. The presence of visible light increases the rates of reactions (2) and (4) [[31](#page-6-0)–[33\]](#page-6-0) and simultaneously accelerates the regeneration of Fe^{II} and V^{IV} . As a result, the Fe^{III}/Fe^{II} and V^{V}/V^{IV} cycles are well maintained in the FeVO₄–H₂O₂ system and \bullet OH are produced faster, which meaning that the role of incident light increases significantly the H_2O_2 efficiency in producing \bullet OH according to reactions (1)–(4). Conse-

Fig. 4 Effect of pH on the degradation of OG (a) and k vs pH (b). [FeVO₄]₀ = 0.5 g·L⁻¹, [H₂O₂]₀ = 15 mmol·L⁻¹, and [OG]₀ = 20 mg·L⁻¹

Fig. 5 Effect of visible light irradiation on the degradation of OG. $[OG]_0 = 20$ mg $\cdot L^{-1}$, $[FeVO_4]_0 = 0.5$ g $\cdot L^{-1}$, and $[H_2O_2]_0 = 15$ $mmol·L^{-1}$

quently, the oxidative capacity of the $FeVO_4-H_2O_2$ system greatly improves, and the decolorization rate of OG increases owing to the irradiation with visible light.

4 Conclusions

The degradation of OG in neutral solutions was investigated considering the $FeVO₄$ and $H₂O₂$ concentrations, and initial concentration of OG solutions. In the $FeVO₄$ H_2O_2 system, \bullet OH is the most important reactive species for the degradation of OG. The OG degradation in the $FeVO₄–H₂O₂$ system follows first-order reaction kinetics and conforms to the Langmuir–Hinshelwood model (R^2 = 0.9988). FeVO₄ was successfully applied to the treatment of wastewater at circumneutral pH. The irradiation with visible light greatly enhanced the rate of oxidation of OG in the FeVO₄–H₂O₂ system at pH 7.0, which is attributed to the enhanced rates of the iron and vanadium cycles as $FeVO₄$ absorbed light.

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