



# Dispersion-Engineered SiN-Coated TeO<sub>2</sub> Hybrid Waveguide for Nonlinear Applications

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## Abstract

On-chip light generation in the mid-infrared (mid-IR) region of the electromagnetic spectrum is gaining considerable attention due to its various potential applications in free-space communication, mid-IR spectroscopy, sensing, and thermal imaging. In this work, we have designed a dispersion-engineered silicon nitride (SiN)-coated tellurium oxide (TeO<sub>2</sub>) hybrid waveguide on silica (SiO<sub>2</sub>) substrate with barium fluoride (BaF<sub>2</sub>) as cladding for nonlinear applications. Strong modal confinement, broad dispersion characteristic, and high nonlinearity were achieved in the proposed hybrid waveguide design, which are important features for obtaining desired nonlinear applications. Through numerical simulations, we found that the dispersion curve is nearly flat within the dispersion range of  $-40.60$  ps/nm/km to  $33.15$  ps/nm/km for a spectral bandwidth of  $1.55$ – $4.25$   $\mu\text{m}$  with a zero-dispersion wavelength (ZDW) around  $1.80$   $\mu\text{m}$ , which is suitable for generating nonlinear effects such as four-wave mixing, self-phase modulation, and Raman scattering. Such types of on-chip hybrid waveguide devices can be pumped using a commercially available fiber laser operating at a wavelength of  $2$   $\mu\text{m}$ . The design of the hybrid waveguide was optimized to achieve very low modal confinement loss ranging from  $0.1 \times 10^{-4}$  to  $35$  dB/cm, with a spectral bandwidth of  $1.5$ – $4$   $\mu\text{m}$ . Additionally, a high nonlinear coefficient value of  $1372$   $\text{W}^{-1} \text{km}^{-1}$  was achieved at a pumping wavelength of  $1.5$   $\mu\text{m}$  in hybrid waveguide. The results of such hybrid waveguides can be helpful to experimentalists working in this field for developing nonlinear hybrid waveguide devices. These nonlinear hybrid waveguide devices have potential nonlinear applications, including four-wave mixing, Raman scattering, and supercontinuum spectrum spanning the near-IR to mid-IR. Further, the on-chip hybrid waveguide structure can be significantly help to expand the functionality of future photonics integrated circuits.

**Keywords** Hybrid waveguide · dispersion · zero-dispersion wavelength · Nonlinearity

## Introduction

In recent years, there has been an emphasis on understanding the physics underlying the intricate subject of nonlinear optical physics (intensity-dependent optical properties of material).<sup>1</sup> Some of the nonlinear phenomena are self-phase modulation (SPM), cross-phase modulation (XPM), stimulated Raman scattering (SRS), four-wave mixing (FWM), and many others.<sup>2</sup> SPM generates new frequency components and broadens the spectrum due to phase modulation

caused by changes in light intensity in the pulse itself.<sup>2,3</sup> SRS is a process of interaction between incident photons and molecular vibrations, causing them to generate new frequency components towards the lower-frequency domain.<sup>2,4</sup> FWM generates new frequencies on the lower side and the higher side of the input pulse spectrum under phase matching conditions.<sup>2,5</sup> There are various noteworthy uses of nonlinear optical phenomena across many domains, such as frequency conversion, optical parametric oscillators (OPO), optical switching and modulation, nonlinear optical microscopy, quantum nonlinear optics, and supercontinuum generation, which have fascinated many researchers in this field.<sup>1,2</sup> One of the astonishing nonlinear phenomena is supercontinuum (SC) generation (the ultra-broadening of a short intense laser pulse after passing through a highly nonlinear media),<sup>6</sup> which has become an intense focus of

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research because of its various dramatic applications such as broadband laser sources, gas sensing, military purposes, and various clinical analyses such as optical coherence tomography and other areas.<sup>6–9</sup> SC spectra are coherent laser sources generated through nonlinear processes such as SPM, FWM, SRS, and dispersion characteristics of a nonlinear material.

To achieve stable, smooth, un-depletable, coherent, and wide SC spectra, the pumping wavelength of the input fiber laser source is around a zero-dispersion wavelength (ZDW) of nonlinear material, and this material should have a flat and low dispersion profile that falls in the anomalous dispersion region.<sup>6,7</sup> A wide range of advantages can be obtained from the generation of SC spectra in the anomalous dispersion region, including the production of extremely broadband spectra that span from the visible to the near-infrared or even mid-infrared regions. SC spectra can also be tuned by varying parameters like pump power, pulse duration, and the properties of the nonlinear medium, and they offer high optical power density across broad spectra. However, the pumping in the anomalous dispersion regime, the broadening mechanism of the SC spectrum, is due to the modulation instability or soliton fission on the anomalous side of the dispersion profile together with the emission of dispersive waves in the normal dispersion region. The SC spectrum generated by the soliton dynamics is susceptible to the laser shot noise, and the output pulse shows a complex temporal structure which makes recompression difficult.<sup>6,10</sup> The generation of on-chip light sources in the mid-infrared (mid-IR) region spanning wavelengths from 2  $\mu\text{m}$  to 25  $\mu\text{m}$  has attracted considerable research attention due to its fascinating applications in fluorescence microscopy, imaging,<sup>11</sup> and free space communication,<sup>12</sup> as a transparency window of earth atmosphere lies between 2  $\mu\text{m}$  and 5  $\mu\text{m}$  and 8–13  $\mu\text{m}$ . This region is also known as the molecular fingerprinting region because it contains most of the vibrational transitions that occur in molecules. These features can be used in various fields such as medicine and security.<sup>7,13,14</sup> Most previous numerical and experimental studies for the generation of mid-IR light sources were conducted using silica (SiO<sub>2</sub>), bismuth, chalcogenide, and tellurite fibers, integrated waveguides, or photonic crystal fibers (PCF).<sup>15–19</sup> Silica PCF geometry has high modal confinement but it has weak nonlinearity, and a high-power pumping source is required; also, its transparency is below 2.4  $\mu\text{m}$ , so it cannot be used for mid-IR light generation. Chalcogenide, tellurite, and fluoride materials have high nonlinearity, and their transparency lies in the mid-IR region. However, the ZDW of these highly nonlinear materials lies in the mid-IR region, and there is a lack of available fiber laser sources operating at these large wavelengths. High nonlinearity and pumping around the ZDW reduce the power requirement of the input laser source. Researchers are looking for new designs and ways to modify the properties of

materials to achieve the desired ZDW of nonlinear material, and to obtain flat and wide dispersion characteristics to produce broad, stable, non-depletable light sources in the mid-IR domain.<sup>20–27</sup>

During the previous decade, Choi et al. showed that Ge–Sb–S chalcogenide glasses were the subject of much research due to their nonlinear optical characteristics. It was demonstrated that with its huge refractive index and wide transparency range, this waveguide has a nonlinear parameter of 7 W<sup>-1</sup>/m at 1.5  $\mu\text{m}$  and generates SC spectra between 1280 nm and 2120 nm, which makes this ridge waveguide a promising platform for future nonlinear applications in the infrared domain.<sup>28</sup> Saini et al. designed and numerically analyzed an on-chip rib Ga–Sb–S chalcogenide waveguide structure for mid-IR SC generation. Numerical investigations showed that the waveguide has two ZDWs at 2050 nm and 2800 nm with nonlinear coefficients of 24,100 W<sup>-1</sup> km<sup>-1</sup> and 14,000 W<sup>-1</sup> km<sup>-1</sup>, respectively. When driven by 97-fs laser pulses with a peak strength of 1 kW at 2050 nm, the waveguide structure produces a mid-IR SC spectrum ranging from 1000 nm to 7800 nm.<sup>29</sup> Further, SC spectra ranging from 1.2  $\mu\text{m}$  to 7.2  $\mu\text{m}$  are generated in an As<sub>2</sub>Se<sub>3</sub> chalcogenide glass on-chip rib waveguide structure when pumped with an input laser pulse of 200 fs at 2.8- $\mu\text{m}$  wavelength with peak power of 2.5 kW.<sup>30</sup> Medjouri et al. numerically investigated an As<sub>2</sub>S<sub>3</sub> chalcogenide glass ridge waveguide structure. This waveguide structure exhibits a ZDW around 2  $\mu\text{m}$  and generates ultra-broad, flat, stable SC spectra spanning from 700 nm to 5200 nm driven by 25 kW power 100-fs laser source operating at a wavelength of 2050 nm. It has been used for sensing, military purposes, and other applications.<sup>31</sup> Sinobad et al. reported a highly coherent octave-spanning mid-IR on-chip broad laser source in an air-clad Si–Ge/Si waveguide.<sup>32</sup> Terro et al. reported a low-loss germanium-on-silicon photonic integrated device generating a broad bandwidth mid-IR spectra of 3.39–6.02  $\mu\text{m}$  at a pumping wavelength of 4.6  $\mu\text{m}$  using a 200-fs optical parametric amplifier (OPA) laser source.<sup>33</sup> Gyger et al. investigated simulated Brillouin zone scattering for the first time in silicon nitride (SiN) completely coated with silica cladding.<sup>34</sup> Furthermore, Saini and Supradeepa reported the design and analysis of a tellurium oxide (TeO<sub>2</sub>)-coated SiN hybrid waveguide on a sapphire substrate that extends SC spectra from 0.88  $\mu\text{m}$  to 5.22  $\mu\text{m}$  or 0.95  $\mu\text{m}$  to 5.50  $\mu\text{m}$  at pumping wavelengths of 1.55  $\mu\text{m}$  and 2  $\mu\text{m}$ , respectively, using a pump peak power of 10 kW. By using sapphire as substrate instead of silica, the transparency window increases up to 7  $\mu\text{m}$ .<sup>35</sup> Zhang et al. numerically studied single-layer double-core Si<sub>3</sub>N<sub>4</sub> coupled waveguides having four ZDWs. This on-chip waveguide design generated a 750–3001-nm broad spectrum using an input hyperbolic secant pulse of 50 fs, in the anomalous region.<sup>36</sup> Sheikmolae et al. proposed a GAP-Se tapered

hybrid chalcogenide planar rib waveguide that has two ZDWs at 2.81  $\mu\text{m}$  and 4.91  $\mu\text{m}$  for nonlinear application.<sup>37</sup> Botter et al., for the first time, observed a stimulated Brillouin scattering third-order nonlinear effect in a  $\text{TeO}_2$ -coated SiN waveguide.<sup>38</sup> Mbonde et al. recently reported that complementary metal–oxide–semiconductor (CMOS)-compatible thin  $\text{Si}_3\text{N}_4$  coated with  $\text{TeO}_2$  on  $\text{SiO}_2$  substrate enhances nonlinearity 2.5 times, making the perfect element for nonlinear applications on integrated photonics devices.<sup>39</sup>

Furthermore,  $\text{TeO}_2$  is a highly promising oxide glass that has high linear and nonlinear optical properties. It can be investigated as optical fibers, integrated photonics circuits for four-wave mixing, broadband Raman amplification, rare-earth-metal-doped amplifiers, laser sources, and SC generation.<sup>39–42</sup> It has a high-value linear and nonlinear refractive index, 20 times more than silica fiber.<sup>35</sup> It has transparency in visible to mid-IR regions with low loss and low dispersion value with a high Raman gain coefficient.<sup>43–45</sup> CMOS-compatible SiN is transparent in the visible to infrared domain.<sup>46,47</sup> Its high performance, transparency, compactness, low loss, and cost-effectiveness make it perfect for photonic integrated devices, and it has various applications in gas sensing, clinical investigation, amplifiers, and laser sources.<sup>48,49</sup> Like  $\text{TeO}_2$ , SiN also has a high linear and nonlinear refractive index, providing a good platform for nonlinear optical properties. Considering  $\text{BaF}_2$  as the upper layer rather than considering no cover layer has provided advantages.  $\text{BaF}_2$  is a versatile optical window material with low dispersion and a broad transparency range from the ultraviolet to the far-infrared.<sup>50,51</sup> Using  $\text{BaF}_2$  as covering in comparison to no covering layer or air as the covering layer results in a low dispersion value. A low dispersion profile is crucial for maximizing SC generation in fibers by reducing temporal walk-off during spectral broadening. Also, there is little variation in confinement loss using  $\text{BaF}_2$  in the spectral range of 1.5–4  $\mu\text{m}$ .

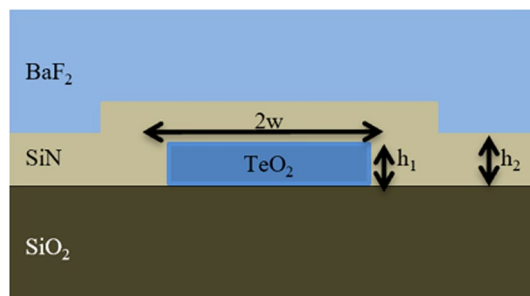
Recently, a high-quality  $\text{TeO}_2$  waveguide integrated on a low-loss SiN wafer-scale platform was fabricated for the application of compact linear, nonlinear, and active devices operating in visible to mid-IR regions.<sup>44</sup> However, through numerical simulations, we found a deep-normal (deep-negative) dispersion profile of the fabricated  $\text{TeO}_2$  integrated waveguide on the SiN platform.<sup>44</sup> Also, another  $\text{TeO}_2$ -coated SiN hybrid waveguide was reported for near- to mid-IR SC generation.<sup>35</sup> This hybrid waveguide also has a dispersion profile in the normal dispersion region, and the ZDW lies around 3.5  $\mu\text{m}$ , which is not suitable for nonlinear applications such as four-wave mixing and SC spectrum generation using conventional laser pumping at 1.55  $\mu\text{m}$  and 2.0  $\mu\text{m}$ .

In this work, we have designed and analyzed a dispersion-engineered SiN-coated  $\text{TeO}_2$  hybrid waveguide on  $\text{SiO}_2$  substrate with  $\text{BaF}_2$  as cladding for nonlinear applications.

Dispersion characteristics, modal confinement loss, and nonlinearity are important features to achieve the desired results. By simulating this hybrid waveguide design, we have obtained a broad and low-value dispersion curve lying in the anomalous region, low confinement loss, and high nonlinearity for the wavelength spanning from 1.55  $\mu\text{m}$  to 4.25  $\mu\text{m}$ . The designed hybrid waveguide structure is highly applicable for future on-chip photonic integrated circuits. A designed hybrid SiN-coated  $\text{TeO}_2$  waveguide device can be a significant choice to expand its functionality towards nonlinear applications using commercially available laser pulses operating at 2  $\mu\text{m}$ .

## Design and Proposed Fabrication Method for the Hybrid Waveguide Structure

The schematic transverse cross-sectional view of the designed SiN-coated  $\text{TeO}_2$  hybrid waveguide on silica substrate with  $\text{BaF}_2$  as cladding is illustrated in Fig. 1, where  $w$  is the width of the  $\text{TeO}_2$  strip,  $h_1$  represents the thickness of the  $\text{TeO}_2$  strip, and  $h_2$  indicates the thickness of the SiN layer coated over the  $\text{TeO}_2$  strip. Seventy percent of the thickness of the SiN layer is considered on both sides of the  $\text{TeO}_2$  strip. From a fabrication point of view, the  $\text{TeO}_2$  film can be deposited on a 2- $\mu\text{m}$ -thick  $\text{SiO}_2$  substrate. This type of waveguide structure can be obtained by employing radio-frequency (RF) reactive sputtering or liquid-phase chemical vapor deposition (LPCVD) techniques.<sup>35</sup> Following the RF sputtering technique, coating of SiN layer over  $\text{TeO}_2$  strip can be obtained. The pattern of a hybrid waveguide device can be fabricated using electron beam lithography and reactive ion etching (RIE) techniques.<sup>43</sup> Additionally, a 2- $\mu\text{m}$ -thick cladding layer of  $\text{BaF}_2$  is deposited using the spin-coating method. Finally, a hybrid waveguide structure is obtained. The optimized geometrical parameters of hybrid waveguide are illustrated in Table I. The core region of the designed hybrid waveguide shows several modes. To avoid inter-modal coupling between these modes, mode-coupling



**Fig. 1** A transverse cross-sectional view of a SiN-coated  $\text{TeO}_2$  hybrid waveguide.

suppression conditions are satisfied by the effective indices of the modes.<sup>52</sup> Only the fundamental transverse electric (TE) mode is considered during the whole numerical simulation, since higher-order modes have larger confinement losses. Figure 2a–d shows the distribution of electric fields for confined fundamental TE modes at pumping wavelengths of 1.5  $\mu\text{m}$ , 2  $\mu\text{m}$ , 3  $\mu\text{m}$ , and 5  $\mu\text{m}$ .

**Table I** Optimized geometrical parameters of the hybrid waveguide design

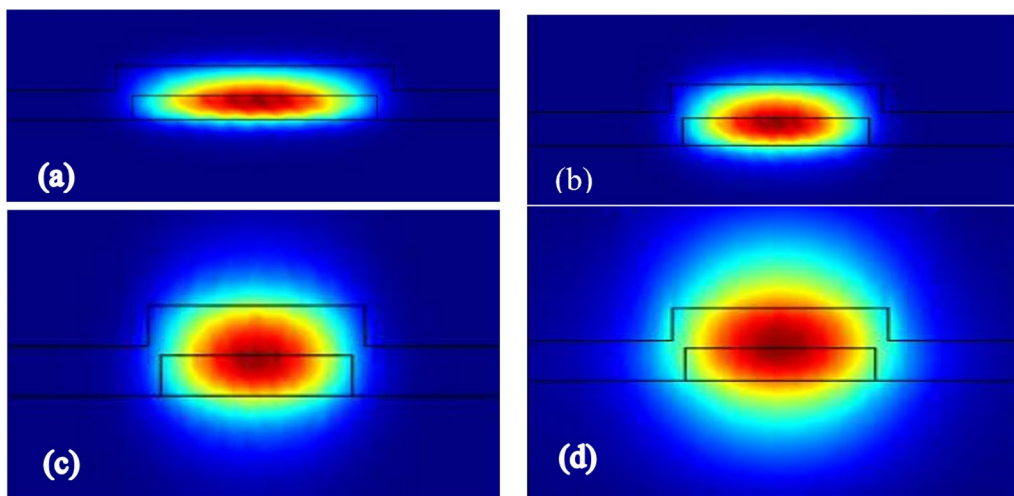
Parameters	Value
$h_1$ (thickness of TeO <sub>2</sub> layer)	470 nm
$h_2$ (thickness of SiN strip)	580 nm
$w$ (width of TeO <sub>2</sub> layer)	3 $\mu\text{m}$

## Numerical Method Analysis

To explore the design of a SiN-coated TeO<sub>2</sub> hybrid waveguide, the TE modes passing through this hybrid waveguide were simulated and their effective mode indices were calculated using the full-vectorial finite element method (FEM). COMSOL Multiphysics (an adaptable simulation tool) supports FEM for solving problems in the previously mentioned investigations. With the variation in the wavelength of the input laser pulse, changes in the refractive index of the material are observed. This variation in the refractive index of TeO<sub>2</sub>, SiN, SiO<sub>2</sub>, and BaF<sub>2</sub> materials is calculated using the Sellmeier equation (Eq. 1) and Sellmeier coefficients of these materials as shown in Table II.<sup>35</sup>

$$n^2 = A_0 + \sum_{n=1}^n \frac{A_n \lambda^2}{\lambda^2 - a_n^2} \quad (1)$$

Understanding and controlling nonlinear optical properties is greatly aided by group velocity dispersion (GVD), especially when it comes to optical fibers and other



**Fig. 2** Electrical field distribution of fundamental TE modes confined in the core region of the hybrid waveguide at pumping wavelengths of (a) 1.55  $\mu\text{m}$ , (b) 2  $\mu\text{m}$ , (c) 3  $\mu\text{m}$ , and (d) 5  $\mu\text{m}$ .

**Table II** Sellmeier coefficients for TeO<sub>2</sub>, SiN, BaF<sub>2</sub>, and SiO<sub>2</sub><sup>35,51</sup>

Sellmeier coefficient	TeO <sub>2</sub> ( $\lambda$ in $\mu\text{m}$ )	SiN ( $\lambda$ in nm)	BaF <sub>2</sub> ( $\lambda$ in $\mu\text{m}$ )	SiO <sub>2</sub> ( $\lambda$ in $\mu\text{m}$ )
$A_0$	3.5483034	1	1.3397	1
$A_1$	0.9783726	3.0249	0.8107	0.6961663
$A_2$	6.6510879	40314	0.19652	0.4079426
$A_3$	–	–	4.52469	0.8974794
$a_1$	0.287522973	135.3406	0.10065	0.0684043
$a_2$	15	1239842	29.87	0.1162414
$a_3$	–	–	53.82	9.896161

waveguides. Various components of input laser pulses may disperse over time as they pass through the fibers due to GVD, leading to pulse broadening. High-intensity light can induce new frequency components. Differences in group velocity of these new frequency components can affect the features and effectiveness of nonlinear processes. In the anomalous dispersion domain, nonlinear phenomena may occasionally counteract GVD and solitons may develop. For optimization of optical nonlinear systems, dispersion needs to be considered, and the dispersion profile of the hybrid waveguide can be simulated using Eq. 2.<sup>35</sup>

$$D = -\frac{\lambda}{c} \frac{\partial^2 \text{Re}(n_{\text{eff}})}{\partial \lambda^2} \quad (2)$$

where  $c$  represents the speed of light, and  $\text{Re}(n_{\text{eff}})$  is the real part of the effective mode indices. The effective area of a mode traveling through a hybrid waveguide and its nonlinear coefficient is given by Eqs. 3 and 4, respectively.<sup>35</sup>

$$A_{\text{eff}} = \frac{\left( \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} |E|^2 dx dy \right)^2}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} |E|^4 dx dy} \quad (3)$$

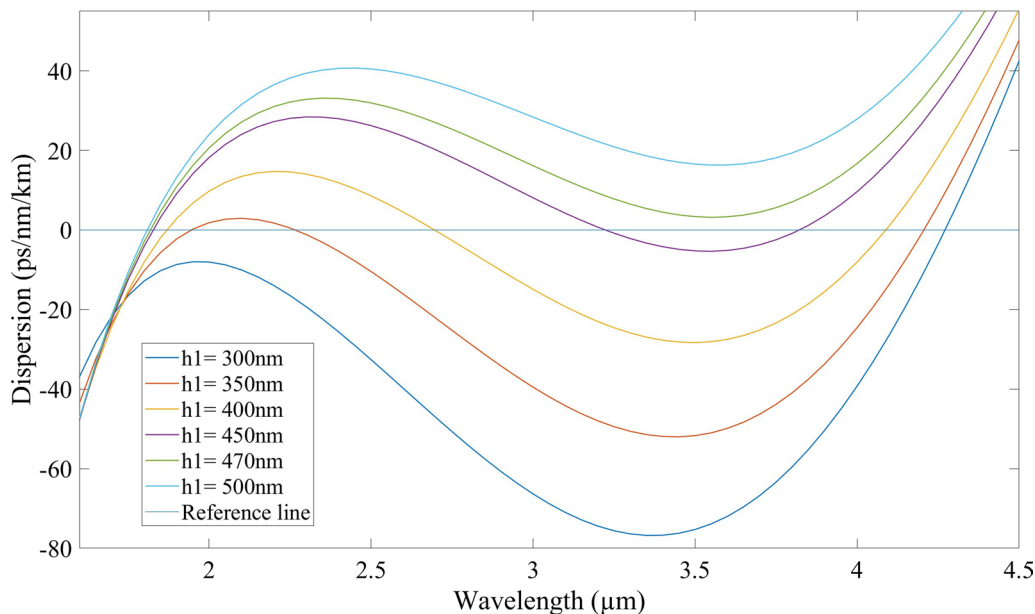
$$\gamma = \frac{2\pi n_2}{\lambda A_{\text{eff}}} \quad (4)$$

where  $E$  denotes the amplitude of the electric field intensity,  $n_2$  is the nonlinear refractive index for  $\text{TeO}_2$ , and  $n_2 = 1.3 \times 10^{-18} \text{ m}^2/\text{W}$ .<sup>35</sup> We consider only the  $\text{TeO}_2$  nonlinear refractive index when calculating the effective nonlinearity because at shorter wavelengths of  $1.55 \mu\text{m}$  and  $2 \mu\text{m}$ , most of the light of the fundamental mode is confined in the  $\text{TeO}_2$  core region rather than in the SiN strip region. Light starts to be confined in a SiN strip at higher wavelengths, as shown in Fig. 2. Also, confinement loss is very large beyond  $4.5 \mu\text{m}$ . This hybrid waveguide can be advantageous for nonlinear applications within the wavelength range up to  $4.5 \mu\text{m}$ .

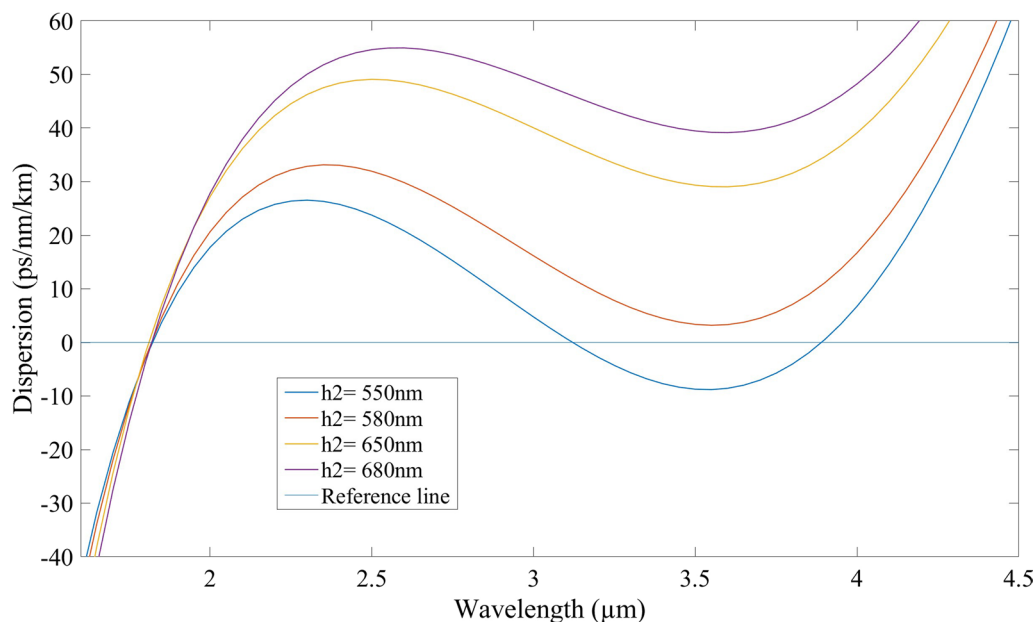
## Result and Discussion

Dispersion and nonlinearity play a major role in understanding and managing nonlinear optical characteristics of photonic-integrated devices. Proper dispersion engineering allows us to employ conventional laser sources for the characterization of such devices. We have designed our hybrid waveguide structure for obtaining its ZDW near  $2 \mu\text{m}$ . The dispersion characteristics of a reported hybrid waveguide are shown in Figs. 3, 4, 5, and 6.

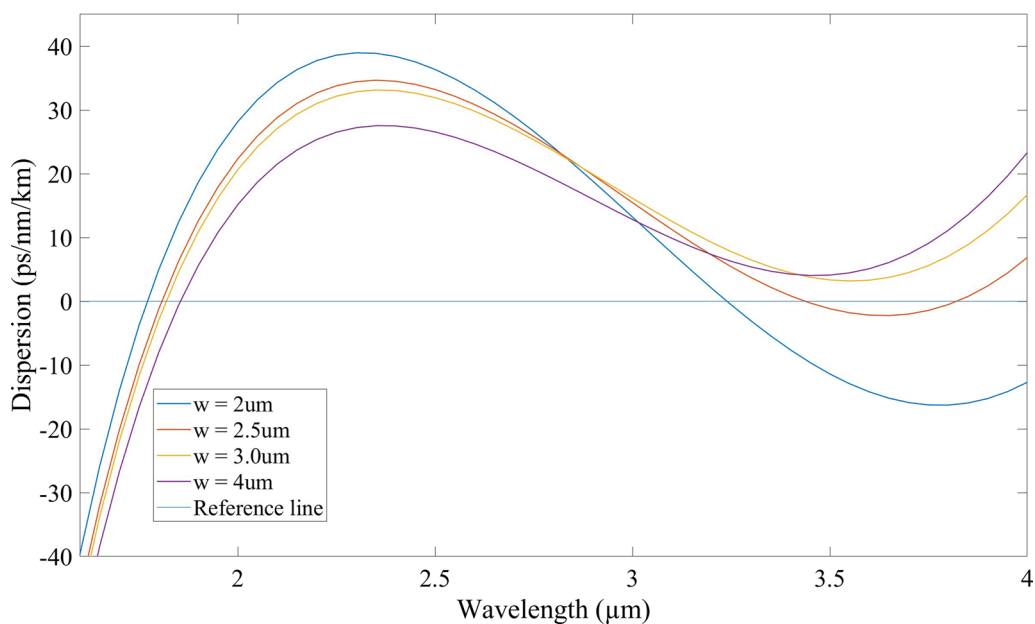
Figure 3 shows the change in dispersion characteristics with a change in thickness ( $h_1$ ) of the  $\text{TeO}_2$  strip at  $h_2 = 580 \text{ nm}$  and  $w = 3 \mu\text{m}$ . It can be seen that with an increase in the thickness of  $\text{TeO}_2$  strip, the dispersion curve shifts from a normal dispersion domain to an anomalous dispersion domain, and the value of the ZDW shifts towards the lower-wavelength region. Further, the dispersion curve becomes progressively flatter on increasing  $h_1$ .



**Fig. 3** Dispersion profiles of a SiN-coated  $\text{TeO}_2$  hybrid waveguide with variation in thickness ( $h_1$ ) of the  $\text{TeO}_2$  core at  $w = 3 \mu\text{m}$  and  $h_2 = 580 \text{ nm}$ .



**Fig. 4** Dispersion profiles of a SiN-coated TeO<sub>2</sub> hybrid waveguide with variation in thickness ( $h_2$ ) of SiN at  $h_1 = 470$  nm and  $w = 3$   $\mu\text{m}$ .

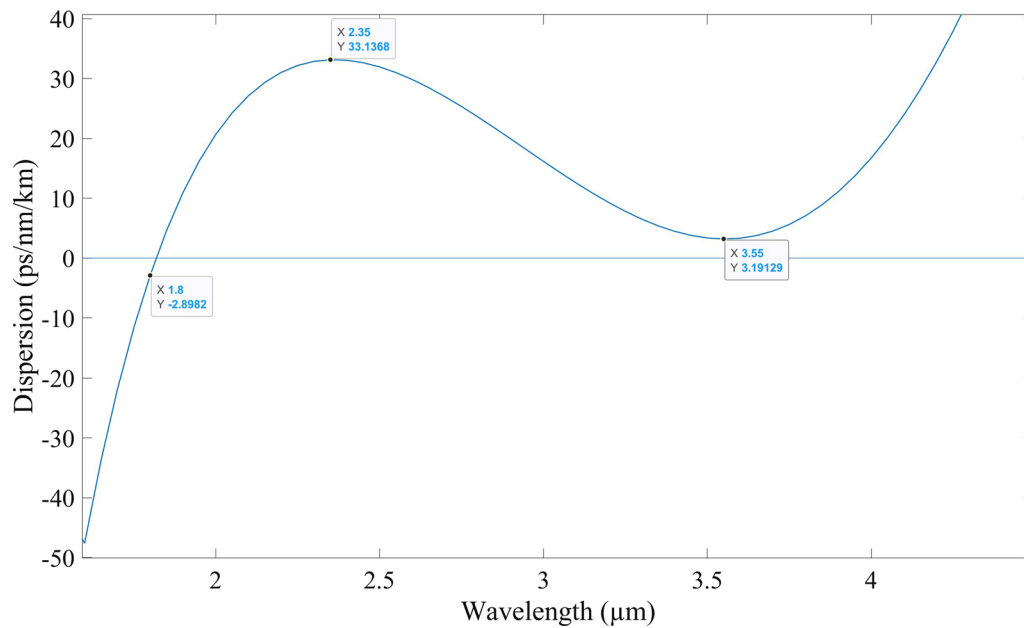


**Fig. 5** Dispersion profiles of a SiN-coated TeO<sub>2</sub> hybrid waveguide with variation in the width ( $w$ ) of TeO<sub>2</sub> at  $h_1 = 470$  nm and  $h_2 = 580$  nm.

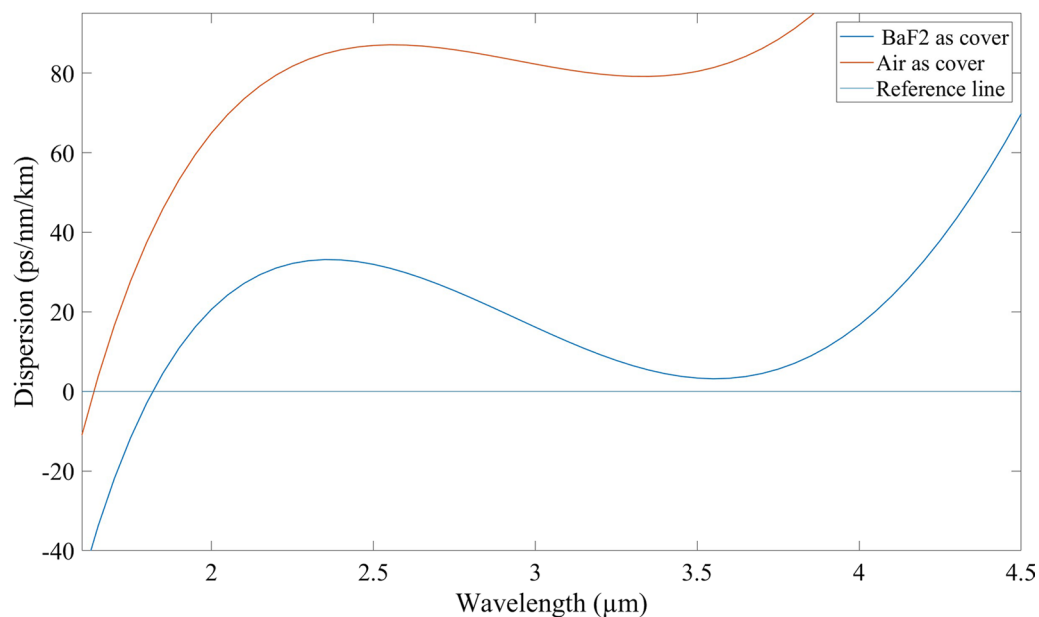
Figure 4 presents the variation in dispersion characteristics with an increase in thickness ( $h_2$ ) of coated SiN layer at  $h_1 = 470$  nm and  $w = 3$   $\mu\text{m}$ . It can be observed that with an increase in the thickness of the SiN layer, the dispersion curve shifts towards a higher dispersion value.

Figure 5 presents the change in dispersion characteristics with an increase in the width ( $w$ ) of the TeO<sub>2</sub> strip at  $h_1 = 470$  nm and  $h_2 = 580$  nm. It is observed that the dispersion curve shifts to a lower dispersion value and the ZDW

shifts towards a higher wavelength with an increase in the width of the TeO<sub>2</sub> strip. Modal dispersion and a ZDW in a waveguide are affected by the thickness and width of the core due to its effect on the mode distribution, effective refractive index, and mode confinement. Thicker cores provide optical modes more room to spread out in the transverse direction. This is why it is expected that as the thickness of the core increases, there is an increase in the dispersion



**Fig. 6** Dispersion profile of the proposed hybrid waveguide structure with optimized geometrical parameters  $h_1=470$  nm,  $h_2=580$  nm, and  $w=3$   $\mu\text{m}$ .

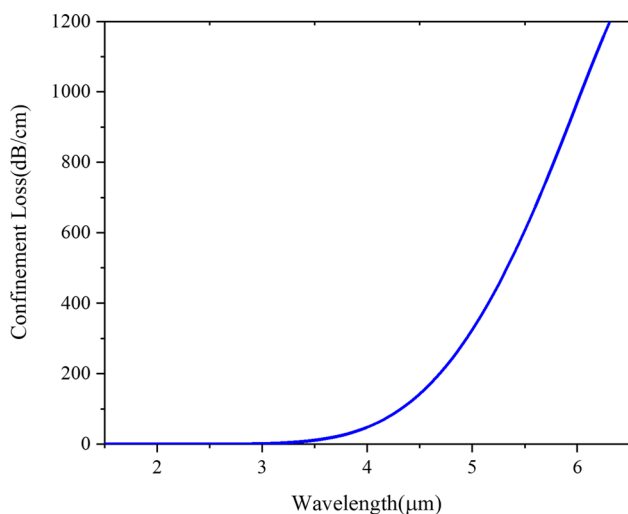


**Fig. 7** Comparison between dispersion profiles of the SiN-coated  $\text{TeO}_2$  hybrid waveguide with  $\text{BaF}_2$  and air as cladding.

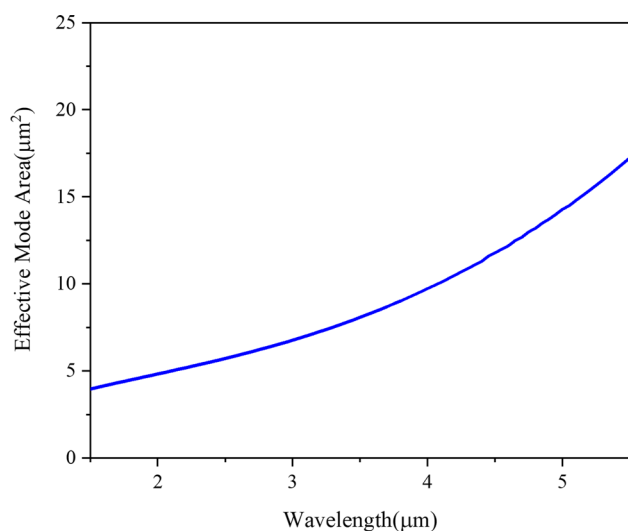
value, and the ZDW shifts towards a lower wavelength value, which was observed by numerical simulation.

Figure 6 shows the dispersion profile with optimized geometrical parameters of the hybrid waveguide, namely  $h_1=470$  nm,  $h_2=580$  nm, and  $w=3$   $\mu\text{m}$ . With these optimized parameters, the dispersion curve varies from 40.60 ps/nm/km to 33.15 ps/nm/km within the spectral range of 1.55–4.25  $\mu\text{m}$ , and the value of the ZDW is around 1.80 ps/nm/km. The dispersion curve lies in the anomalous domain

upon optimized geometrical parameters. At pumping wavelengths 1.55  $\mu\text{m}$ , 2  $\mu\text{m}$ , 3  $\mu\text{m}$ , and 4  $\mu\text{m}$  observed dispersion values are  $-40.60$  ps/nm/km, 20.64 ps/nm/km, 16.15 ps/nm/km, and 16.70 ps/nm/km, respectively. By using  $\text{BaF}_2$  as covering, the low dispersion value varies from 3.192 ps/nm/km to 33.1368 ps/nm/km in the spectral range from 1.85  $\mu\text{m}$  to 4.0  $\mu\text{m}$  in comparison to no covering layer or air, as the covering layer dispersion varies from 89.1122 ps/nm/km to 79.18 ps/nm/km in the same spectral range. A low dispersion



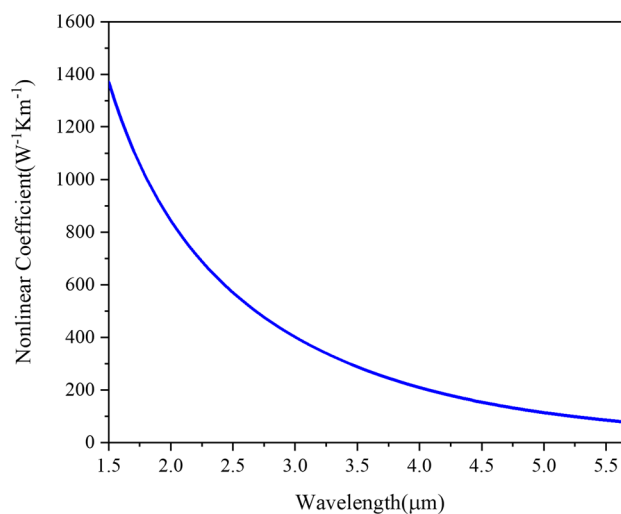
**Fig. 8** Confinement loss of a SiN-coated TeO<sub>2</sub> hybrid waveguide with varied input laser pulse wavelengths.



**Fig. 9** Spectral variation in the effective mode area of an on-chip hybrid waveguide.

profile is crucial for maximizing SC spectral broadening. A comparison in dispersion characteristics of BaF<sub>2</sub> cover and air as cover is shown in the Fig. 7.

To benefit from TeO<sub>2</sub> material features such as high nonlinearity and light emission in rare-earth-doped films, large optical confinement inside the core is ideal. Figure 8 shows the modal confinement loss as a function of the wavelength of an input laser pulse. It can be seen that the value of confinement loss is in the range from  $0.1 \times 10^{-4}$  dB/cm to 35 dB/cm with spectral bandwidth of 1.5 to 4 μm. Confinement loss in a given hybrid waveguide structure increases sharply after 4.5 μm. Tellurite glasses are transparent in the spectral range



**Fig. 10** Spectral variation in nonlinear coefficient of an on-chip hybrid waveguide.

below 5 μm. These materials exhibit significant material loss for longer wavelengths in the IR region. Saini et al., Feng et al., and Jha et al. independently studied the optical losses of tellurium oxide.<sup>43,53,54</sup> Their research shows large material and propagation loss beyond 5 μm in tellurite-based optical fibers, which sets the long-wavelength limit of mode confinement at 4.5 μm. This hybrid waveguide can be advantageous for nonlinear applications within the wavelength range up to 4.5 μm.

Spectral variations in the effective area of the fundamental TE mode which travels through this numerically simulated hybrid waveguide are presented in Fig. 9. It is noted that at pumping wavelengths of 1.55 μm, 1.80 μm, and 2 μm, the values of effective mode area are 4.06 μm<sup>2</sup>, 4.5 μm<sup>2</sup>, and 4.8 μm<sup>2</sup>, respectively. For various nonlinear applications, the nonlinearity of the material must be high. The variation in the nonlinearity of a hybrid waveguide with the variation in the wavelength of the input laser pulse is presented in Fig. 10. It can be seen that the values of the nonlinear coefficient are 1297 W<sup>-1</sup> km<sup>-1</sup>, 1008 W<sup>-1</sup> km<sup>-1</sup>, and 843 W<sup>-1</sup> km<sup>-1</sup> at the pumping wavelengths 1.55 μm, 1.80 μm, and 2 μm, respectively.

## Conclusion

We have designed and analyzed a SiN-coated TeO<sub>2</sub> on-chip hybrid waveguide for nonlinear applications. After the parameters of the hybrid waveguide are optimized, the dispersion characteristics are nearly flat and broad within the dispersion range of  $-40.60$  ps/nm/km to 33.15 ps/nm/km for the spectral bandwidth of 1.50–4.25 μm, and the ZWD measures around 1.80 μm. To generate nonlinear effects in such types of on-chip waveguide devices, a commercially accessible fiber laser operating at 2.0 μm can



be employed. Pumping around the ZDW lowers the input power requirement and maximum transfer of energy to the output spectra. Results indicate that this design exhibits a low modal confinement loss for a wavelength range of 1.5–4  $\mu\text{m}$  and very high nonlinear coefficient of 1297  $\text{W}^{-1}\text{km}^{-1}$  and 843  $\text{W}^{-1}\text{km}^{-1}$  at 1.55  $\mu\text{m}$  and 2  $\mu\text{m}$  operating wavelengths, respectively. The designed hybrid waveguide structure can be employed for future on-chip integrated devices. Results of numerical simulation confirm that this hybrid SiN-coated  $\text{TeO}_2$  waveguide device can significantly aid in expanding its functionality for nonlinear optical applications across numerous domains, including on-chip light sources, frequency conversion, clinical investigations, four-wave mixing, Raman amplification, mid-IR imaging, and generation of mid-IR supercontinuum spectra, among many other domains.

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