RESEARCH PAPER

Numerical simulations on the dynamics of a particle pair in a viscoelastic fuid in a microchannel: efect of rheology, particle shape, and confnement

Gaetano D'Avino1 · Pier Luca Mafettone1

Received: 13 February 2019 / Accepted: 25 April 2019 / Published online: 16 May 2019 © Springer-Verlag GmbH Germany, part of Springer Nature 2019

Abstract

The dynamics of two particles suspended in a viscoelastic fuid and aligned on the centerline of a microfuidic channel is investigated by direct numerical simulations. The shear-thinning elastic fuid is modeled by the Giesekus constitutive equation. The relative particle velocity is studied by varying the interparticle distance, the Deborah number, fuid shear thinning, confnement ratio, and particle shape. Concerning the latter aspect, spherical and spheroidal particles with diferent aspect ratios are considered. The regimes of particle attraction and repulsion as well as the equilibrium confgurations are identifed and correlated with the fuid rheological properties and particle shape. The observed dynamics is related to the distribution of the viscoelastic normal stresses in the fuid between the particles. The results reported here provide useful insights into design efficient microfluidics devices to achieve particle ordering, i.e., the formation of equally spaced particle structures.

Keywords Particle pair · Viscoelasticity · Focusing · Ordering · Numerical simulations · Microfuidics

1 Introduction

The focusing of particles at the centerline of a microfuidic channel induced by fuid viscoelasticity has been of great interest over the last years (D'Avino et al. [2017](#page-12-0); Lu et al. [2017](#page-13-0)). As compared to other similar techniques (Xuan et al. [2010](#page-13-1)), particle alignment in a viscoelastic medium can be achieved in a simple straight microchannel avoiding extra components and/or complex designs of the device. Several theoretical, experimental and numerical works have elucidated the mechanism behind the focusing phenomenon as well as the role of fuid rheology, fow intensity, and geometry (shape of the channel cross section and confnement ratio, i.e., the ratio between the particle size and the characteristic dimension of the channel) on the alignment

This article is part of the topical collection "Particle motion in non-Newtonian microfuidics" guest edited by Xiangchun Xuan and Gaetano D'Avino.

 \boxtimes Gaetano D'Avino gaetano.davino@unina.it efficiency (Leshansky et al. [2007](#page-13-2); Yang et al. [2011;](#page-13-3) D'Avino et al. [2012](#page-12-1); Lee et al. [2013;](#page-13-4) Kang et al. [2013](#page-12-2); Del Giudice et al. [2013](#page-12-3); Lim et al. [2014](#page-13-5); Seo et al. [2014](#page-13-6); Del Giudice et al. [2015](#page-12-4); Yang et al. [2017;](#page-13-7) Yuan et al. [2018](#page-13-8); Li and Xuan [2018](#page-13-9); Xiang et al. [2019](#page-13-10)). In brief, a particle suspended in a viscoelastic medium experiences a motion transversal to the main fow direction, frstly observed by Mason and co-workers (Karnis and Mason [1966;](#page-12-5) Gauthier et al. [1971](#page-12-6)), induced by the fuid normal stresses (D'Avino and Mafettone [2015](#page-12-7); D'Avino et al. [2017](#page-12-0); Lu et al. [2017\)](#page-13-0). Since the 'migration velocity' is 2–3 orders of magnitude lower than the main flow velocity, very long channels (compared to the crosssection characteristic dimension) are required to achieve highly efficient alignment. Microfluidics is, then, a very well-suited framework to exploit the migration phenomenon, as demonstrated for the frst time by Leshansky et al. ([2007](#page-13-2)). To date, 3D particle focusing induced by fuid viscoelasticity is a well established, fnely controllable technique to manipulate trajectories of particles with spherical shape. Studies on non-spherical particle suspensions recently appeared (Lu et al. [2015;](#page-13-11) Lu and Xuan [2015;](#page-13-12) D'Avino et al. [2019](#page-12-8)). Specifcally, numerical simulations have reported that the migration mechanism occurs for non-spherical particles as well and that, after reaching the axis channel, they slowly

¹ Dipartimento di Ingegneria Chimica, dei Materiali e della Produzione Industriale, Università di Napoli Federico II, P.le Tecchio 80, 80125 Naples, Italy

orient with their major axis along the main fow direction (D'Avino et al. [2019\)](#page-12-8).

A step forward in particle focusing is the ordering of the aligned particles, i.e., the capability of forming a train of equally spaced particles. Very recent experiments and simulations have shown that viscoelasticity is able to rearrange the microstructure and promote ordering (Del Giudice et al. [2018](#page-12-9)). More specifcally, the formation of a train of particles at approximately equal distances has been observed in a shear-thinning viscoelastic fuid, while no ordering has been reported for constant viscosity fuids. The ordering mechanism has been confrmed by numerical simulations carried out in the same conditions explored in the experiments. A simple qualitative argument on the particle train stability able to explain the observed train dynamics has been also derived. A remarkable result of the proposed argument is that, although the evolution of the microstructure is due to complex hydrodynamic interactions of a multi-particle system, many features of the fnal particle arrangement can be predicted by simply analyzing the dynamics of only two particles.

The problem of the dynamics of a pair of spherical particles suspended in a viscoelastic fuid and aligned at the centerline of a cylindrical microchannel has been tackled by direct numerical simulations (D'Avino et al. [2013\)](#page-12-10). The results can be summarized as follows: (i) the particles can reduce or increase their distance while traveling along the channel depending on the initial distance and the Deborah number (defined as the ratio between the fluid and flow characteristic time); (ii) a critical Deborah number De_{cr} is identified such that, for $De < De_{cr}$, two particles attract or repel depending on whether their initial distance is lower or higher than a critical distance; (iii) if $De > De_{cr}$ only repulsion dynamics occurs. These results, however, were obtained for a single fuid rheology. The efect of shear thinning was investigated by fxing the Deborah number, making difficult to draw general conclusions. Furthermore, all the simulations were limited to relatively small interparticle distances, whereas it has been shown that behavior at large distance is crucial in determining the fnal microstructure (Del Giudice et al. [2018](#page-12-9)).

In this work, we re-visit and extend the pair particle problem to a wide and fully combined parametric space of Deborah number, fuid shear thinning, confnement ratio, and interparticle distance. We anticipate that new regimes of the pair dynamics appear in ranges of the investigated parameters that were not explored before. Furthermore, motivated by the recent results on focusing of non-spherical particles mentioned above, we consider the completely new problem of the dynamics of two aligned spheroidal particles.

The study is carried out by direct numerical simulations whereby the macroscopic governing equations, together with a viscoelastic constitutive equation, are solved. State diagrams reporting the relative particle velocity as a function of the investigated parameters are shown, giving a complete overview of the pair particle dynamics problem.

2 Governing equations and numerical method

The system investigated in this work is reported in Fig. [1](#page-1-0)a. A viscoelastic suspension of two spherical or spheroidal particles fows in a straight cylindrical microchannel. The centers of volume of the particles lie on the channel centerline and, in case of non-spherical shape, the particles are oriented along the axis channel. As previously reported, this is, indeed, the stable equilibrium confguration of spheroidal particles in a viscoelastic fuid (D'Avino et al. [2019\)](#page-12-8). We denote by *a* and *b* the particle semi-major and semi-minor axes, and with $AR = a/b$ the aspect ratio. For a sphere, $a = b$ and $AR = 1$. The channel diameter is denoted by *D* and the length by *L*. A Cartesian reference frame is selected with origin at the center of the channel inlet with *z* denoting

Fig. 1 Schematic representation of the investigated system (**a**) and the corresponding computational domain (**b**)

the flow direction. Because of the symmetry, the particles remain on the axis channel aligned along the fow direction. Their positions and velocities are z_1 and z_2 , and U_1 and U_2 , respectively, where '1' and '2' denote the trailing (left in Fig. [1\)](#page-1-0) and leading (right in Fig. [1](#page-1-0)) particles. The distance between the surfaces of the two particles is *d*.

The channel wall is $\partial \Omega_w$, the inflow and outflow channel sections are $\partial \Omega_{\text{in}}$ and $\partial \Omega_{\text{out}}$, respectively, and the boundaries of the particles are ∂P_1 and ∂P_2 . Since the particles are aligned on the centerline, we can reduce the 3D domain to a 2D axisymmetric one, shown in Fig. [1](#page-1-0)b. The boundary $\partial \Omega_{sym} = \partial \Omega_{sym1} \cup \partial \Omega_{sym2} \cup \partial \Omega_{sym3}$ is the axis of symmetry.

We assume incompressibility and negligible inertia for both solid and fuid. The governing equations are the mass and momentum balance equations:

$$
\nabla \cdot \mathbf{u} = 0,\tag{1}
$$

$$
\nabla \cdot \boldsymbol{\sigma} = \mathbf{0},\tag{2}
$$

where \boldsymbol{u} is the fluid velocity and $\boldsymbol{\sigma}$ is the total stress tensor, expressed as:

$$
\sigma = -pI + 2\eta_s D + \tau.
$$
 (3)

In Eq. [\(3](#page-2-0)), *p*, *I*, η_s and $D = (\nabla u + (\nabla u)^T)/2$ are the pressure, the unity tensor, the viscosity of a Newtonian 'solvent' and the rate-of-deformation tensor, respectively. As in D'Avino et al. [\(2013\)](#page-12-10), the Giesekus model is chosen as constitutive equation (Larson [1988](#page-13-13)):

$$
\lambda \overline{\tau} + \frac{\alpha \lambda}{\eta} \tau \cdot \tau + \tau = 2\eta_{p} D,
$$
\n(4)

where η_p is the polymer viscosity, λ is the fluid relaxation time, the symbol (∇) denotes the upper-convected time derivative:

$$
\overline{\tau} \equiv \frac{\partial \tau}{\partial t} + u \cdot \nabla \tau - (\nabla u)^T \cdot \tau - \tau \cdot \nabla u,\tag{5}
$$

and α is a constitutive parameter. We recall that, in shear fow, the Giesekus model predicts a non-zero frst normal stress difference and, for $\alpha > 0$, a shear-thinning viscosity and a non-zero second normal stress diference. The zeroshear viscosity is defined as $\eta_0 = \eta_s + \eta_p$.

Regarding the boundary conditions, no-slip is imposed at the channel wall:

$$
u = 0 \quad \text{on } \partial \Omega_{\text{w}},\tag{6}
$$

and the rigid-body motion is imposed at the particle surfaces:

$$
\mathbf{u} = (0, U_i) \quad \text{on } \partial P_i(t), \tag{7}
$$

with *i* the particle number.

Axial symmetry is applied on the boundaries representing the axis of symmetry:

$$
\mathbf{u} \cdot \mathbf{i} = 0 \quad \text{on } \partial \Omega_{\text{sym}},\tag{8}
$$

$$
(\boldsymbol{\sigma} \cdot \boldsymbol{i})|_{z} = 0 \quad \text{on } \partial \Omega_{\text{sym}},
$$

where *i* is the unit vector along the *x*-direction.

Periodic boundary conditions are prescribed between the infow and outfow sections, together with a fow rate in inflow:

$$
\boldsymbol{u}|_{\partial \Omega_{\text{in}}} = \boldsymbol{u}|_{\partial \Omega_{\text{out}}},\tag{10}
$$

$$
(\boldsymbol{\sigma} \cdot \boldsymbol{k})|_{\partial \Omega_{\text{in}}} = (\boldsymbol{\sigma} \cdot \boldsymbol{k})|_{\partial \Omega_{\text{out}}} - \Delta p \, \boldsymbol{k}, \tag{11}
$$

$$
\int_{\partial \Omega_{\text{in}}} \boldsymbol{u} \cdot \boldsymbol{k} \, \mathrm{d}S = Q,\tag{12}
$$

where \boldsymbol{k} is the unit vector along the *z*-direction and Δp is the pressure drop along the channel between $\partial \Omega_{\text{in}}$ and $\partial \Omega_{\text{out}}$. The flow rate Q is imposed through a constraint where the associated Lagrange multiplier is identifed as the unknown pressure difference Δp (Bogaerds et al. [2004](#page-12-11)). Due to the periodicity along the *z*-direction, the domain length *L* must be chosen much larger than the channel diameter to avoid that the particles hydrodynamically interact with their images.

As inertia is neglected, no initial condition for the velocity feld needs to be specifed. On the other hand, since the time-derivative of the viscoelastic stress tensor appears in the constitutive equation, an initial condition for τ is required. We assumed a stress-free initial condition, i.e., that the stress is zero everywhere in the fuid at the initial time:

$$
\tau|_{t=0} = \mathbf{0}.\tag{13}
$$

Finally, the hydrodynamic force acting on the particles needs to be specifed. Under the assumptions of the absence of particle inertia, and of no 'external' forces (force-free particle), the *z*-component of the total forces F_i on the particle surfaces must be zero:

$$
F_i = \int_{\partial P_i(t)} (\boldsymbol{\sigma} \cdot \boldsymbol{n})|_{z} dS = 0,
$$
\n(14)

where *n* is the outwardly directed unit normal vector on ∂P_i .

At each time step, the particle positions are updated by integrating the kinematic equations:

$$
\frac{\mathrm{d}z_i}{\mathrm{d}t} = U_i \tag{15}
$$

with initial conditions $z_i|_{t=0} = z_i^0$.

The governing equations are solved by the fnite element method. To achieve convergent results at relatively high Deborah numbers, the DEVSS-G/SUPG formulation combined with a log representation for the conformation tensor is implemented (Guénette and Fortin [1995;](#page-12-12) Bogaerds et al. [2002](#page-12-13); Brooks and Hughes [1982](#page-12-14); Fattal and Kupferman [2004](#page-12-15); Hulsen et al. [2005\)](#page-12-16). A boundary-ftted mesh with triangular elements is used with an adequate number

of triangles between the particle surfaces where larger gradients of the fow felds are expected. The mesh is generated by the Gmsh software (Geuzaine and Remacle [2009\)](#page-12-17). The arbitrary Lagrangian–Eulerian (ALE) technique is employed to handle the particle motion (Hu et al. [2001\)](#page-12-18). Further details on the numerical method used as well as mesh and time convergence tests can be found elsewhere (D'Avino et al. [2013](#page-12-10)).

We made the equations dimensionless by choosing the channel diameter *D* as characteristic length, the average velocity $\bar{u} = 4Q/(\pi D^2)$ as characteristic velocity, and $\eta_0 \bar{u}/D$ as characteristic stress. The dimensionless parameters governing the problem are: the Deborah number $De = \lambda \bar{u}/D$ that is the ratio between the fuid and fow characteristic time, the aspect ratio, $AR = a/b$, the confinement ratio $\beta = 2b/D$, the viscosity ratio $\eta_r = \eta_s / \eta_0$, the constitutive parameter α , and the initial particle distance d_0/D .

In this work, we set the viscosity ratio to $\eta_r = 0.091$. In what follows, all the symbols refer to dimensionless quantities.

3 Results and discussion

Previous numerical simulations on the dynamics of two spheres aligned on the channel centerline and suspended in a viscoelastic fuid reported that the interparticle distance decreases or increases depending on the initial distance and the Deborah number (D'Avino et al. [2013](#page-12-10)). The efect of the parameter α was investigated for a single value of *De* and no qualitative change of the pair dynamics was found by increasing or reducing this constitutive parameter. Furthermore, the simulations were limited to relatively small interparticle distances.

As previously remarked D'Avino et al. ([2013](#page-12-10)), beyond an initial start-up due to the stress development, the trends of the relative particle velocity $\Delta U = U_2 - U_1$ collapse on a single master curve when plotted as a function of the current interparticle distance *d*. We can then directly consider the master trend obtained by running several simulations for different initial distances d_0 and take the relative velocity after the transient. Hence, all the curves showing the relative velocity as a function of the interparticle distance are obtained by interpolating a set of data $(d, \Delta U)$ taken after the start-up and corresponding to a specific d_0 . Although the current interparticle distance *d* used to construct the master curves is not exactly equal to d_0 , the two values are very similar because the stress development characteristic time (which is of the same order of magnitude of the fuid relaxation time) is much lower than the characteristic time to have appreciable variations of the relative particle positions.

To fully characterize the dynamics of the system under investigation, we carry out direct numerical simulations by covering the parametric space (d, De, α, β) with ranges chosen in the following way. The interparticle distance interval corresponds to initial distances d_0 selected between $[d_{0,\text{min}}, d_{0,\text{max}}] = [0.01, 3]$. The value of $d_{0,\text{min}} = 0.01$ corresponds to an interparticle distance of 5% of the particle radius, i.e., the particles are almost in contact. Lower values are not feasible due to numerical instabilities and problems related to the meshing procedure. The maximum value $d_{0,\text{max}} = 3$ is sufficiently large so that the particles do not interact anymore and behave like isolated objects. The range of distances is discretized by choosing a step of 0.02 up to a distance of 0.15. The step is then increased to 0.05 up to a distance of 0.4. Finally, the step is further increased to 0.1 up to $d_{0,\text{max}}$. The Deborah number interval is set to $[De_{min}, De_{max}] = [0.5, 3]$. The lowest value corresponds to weak viscoelastic effects able, however, to produce a relative particle motion appreciable in real microfuidic devices (D'Avino et al. [2013](#page-12-10)). The maximum value denotes a system characterized by signifcant elasticity. In this range, we consider two intermediate Deborah numbers, *De* = 1 and $De = 2$, for a total of four values. Regarding the role of the constitutive parameter α , we recall that, for the model used in the present work, non-zero values of α produce both shear thinning and a second normal stress diference. To elucidate the importance of these two fuid properties on the pair particle dynamics, we have performed few simulations with a diferent constitutive equation (Phan–Thien Tanner model (Larson [1988](#page-13-13))) that only predicts the frst normal stress diference and shear thinning. Since the results are qualitatively similar to those obtained for the Giesekus model, we conclude that shear thinning plays the most relevant role in determining the pair particle dynamics. Hence, in what follows, different values of the constitutive parameter α will be connected to variations of the fuid shear-thinning degree. The range of α is chosen as $[\alpha_{\min}, \alpha_{\max}] = [0.05, 0.4]$ where the lowest value corresponds to a fuid with a constant viscosity over a wide range of shear rates, whereas the highest one is characteristic of a strong shear-thinning medium. Together with the extrema, two intermediate values in this interval are considered, i.e., $\alpha = 0.1$ and $\alpha = 0.2$. Finally, two values of the confinement ratio are selected, $\beta = 0.2$ and $\beta = 0.4$, that identify the range of confinement ratios typically used in viscoelastic microfuidics. Indeed, lower values would require extremely long channels to achieve particle focusing [the migration velocity scales as the third power of β (D'Avino et al. [2012](#page-12-1))], whereas higher values could lead to channel clogging.

Before presenting the results of the pair dynamics by varying these four parameters, it is useful to illustrate the possible regimes experienced by the pair. In Fig. [2](#page-4-0), the relative particle velocity ΔU is reported as a function of the interparticle distance *d*. The parameters are $De = 0.5$, $\alpha = 0.05$, $\beta = 0.4$. We started with this specific case since the resulting pair particle dynamics shows the most complex behavior. As **Fig. 2** Relative particle velocity as a function of the interparticle distance for a pair of spherical particles aligned along the centerline of a cylindrical channel and suspended in a Giesekus fluid at $De = 0.5$, $\alpha = 0.05$, $\beta = 0.4$. The values of the distances corresponding to the minima, the maximum and the zeros of the function are highlighted in red. On the top of the fgure, a schematic representation of the pair dynamics for the diferent regimes is shown (color fgure online)

visible in Fig. [2](#page-4-0), depending on the interparticle distance *d*, the relative velocity can be negative or positive corresponding to particle attraction or repulsion, respectively. Specifcally, by increasing *d*, the particles frst attract, then repel, and fnally attract again. These three behaviors, highlighted by diferent colors and sketched on the top part of the diagram, are delimited by the zeros of the black solid curve that correspond to equilibrium solutions. The frst zero is the case at $d = 0$, i.e., the two spheres are in contact. (The very frst trend of this and the following curves are obtained by extrapolating the data points due to the aforementioned problems in simulating distances lower than 0.01.) This solution is stable as, by slightly increasing the interparticle distance, the relative velocity is negative and *d* decreases again.

On the contrary, the distance denoted by d_{z1} corresponds to an unstable equilibrium condition as small perturbations lead the system to move away from such confguration. The third zero denoted by d_{z2} is stable again. Hence, depending on the interparticle distance, at long times, the two particles can travel in contact (if $d < d_{\text{z1}}$) or at a fixed distance d_{z2} (if $d > d_{z1}$). It is worthwhile to mention that the stable solution at $d = d_{22}$ was not found in previous numerical simulations (D'Avino et al. [2013](#page-12-10)) due to the aforementioned limited set of investigated parameters.

An important piece information reported in Fig. [2](#page-4-0) is the magnitude of the relative velocity that is related to the time scale over which a stable confguration is attained. For distances lower than d_{z2} (blue and red regions), ΔU is about three orders of magnitude lower than the main fow average velocity *ū*. Since the migration velocity (responsible for particle focusing) for similar parameters is approximately three orders of magnitude lower than \bar{u} as well (Villone et al. [2011](#page-13-14)), we conclude that a focusing length, generally corresponding to few centimeters, is sufficient to observe a signifcant change of the distance between two particles. On the contrary, the relative velocity in the green region is extremely low. This is not surprising as the very large distances lead to weak hydrodynamic interactions slowing down the pair particle dynamics. Hence, two particles initially positioned at $d > d_{z2}$ travel at a nearly constant speed and signifcant variations of their distance are hardly detectable in standard microfuidic channels.

As discussed above, the distances corresponding to $\Delta U = 0$ are equilibrium configurations for the pair dynamics. However, when dealing with a multiparticle system, the extrema of the curve (in the case of Fig. [2](#page-4-0) two minima and one maximum) can give useful information on the fnal microstructure. Indeed, as discussed in a recent work on particle ordering (Del Giudice et al. [2018\)](#page-12-9), the position of the equilibrium distance d_{eq} with respect to the extrema of the relative velocity curve gives insight into the stability of an equally spaced train of particles. (The equilibrium distance is defned as the distance between equally spaced particles; it is related to the volume fraction by a geometrical relationship.) Just as an example, let us assume that a train of equally spaced particles with distance d_{eq} has been formed, and only one particle is slightly displaced from the equilibrium position. Let us also assume that d_{eq} falls in the red region and that it is greater than the distance *d*max corresponding to the maximum. Since the slope of the relative velocity curve is negative, two particles attract or repel depending on whether the interparticle distance is higher or lower than d_{eq} , respectively. In both cases, the displaced particle attains the equilibrium distance and ordering is restored. An opposite scenario occurs if d_{eq} corresponds to a point of the curve in Fig. [2](#page-4-0) where the slope is positive (e.g., for a value in the red region lower

than d_{max} . In this case, the particle displaced from the equally spaced confguration tends to approach the closest particle and form a doublet (Del Giudice et al. [2018](#page-12-9)).

A second scenario is represented in Fig. [3](#page-5-0). The parameters are $De = 0.5$ (as in the previous case), $\alpha = 0.2$, and $\beta = 0.4$. As compared to the state diagram in Fig. [2,](#page-4-0) we observe that: (i) the zero at d_{z2} and the minimum at d_{min2} disappear and the curve asymptotically tends to the horizontal axis from positive values; (ii) as a consequence of the previous point, only two dynamics are possible, i.e., pair attraction for $d < d_{1}$ (blue region) or repulsion for $d > d_{1}$ (red region), corresponding, at long times, to doublet formation or two isolated particles, respectively; (iii) the magnitude of the relative velocity is lower than the previous case both in case of particle attraction and repulsion,

Fig. 3 Relative particle velocity as a function of the interparticle distance for a pair of spherical particles aligned along the centerline of a cylindrical channel and suspended in a Giesekus fluid at $De = 0.5$, $\alpha = 0.2$, $\beta = 0.4$. The values of the distances corresponding to the minimum, the maximum and the zero of the function are highlighted in red. On the top of the fgure, a schematic representation of the pair dynamics for the diferent regimes is shown (color fgure online)

Fig. 4 Relative particle velocity as a function of the interparticle distance for a pair of spherical particles aligned along the centerline of a cylindrical channel and suspended in a Giesekus fuid at *De* = 3, $\alpha = 0.2$, $\beta = 0.4$. The value of the distances corresponding to the maximum of the function is highlighted in red. On the top of the fgure, a schematic representation of the pair dynamics is shown (color fgure online)

requiring longer channels to observe signifcant changes of the interparticle distance.

Finally, the last possible scenario is depicted in Fig. [4](#page-5-1) where the parameters are $De = 3$, $\alpha = 0.2$, and $\beta = 0.4$. In this case, also the zero at $d = d_{z1}$ and the minimum at $d = d_{\text{min1}}$ disappear and the relative velocity is positive for any interparticle distance. The dynamics is, then, repulsive, leading to the formation of isolated spheres at a distance such that the hydrodynamic interactions have a negligible efect on the relative particle motion.

3.1 State diagrams for spherical particles

The particle pair dynamics shown in Figs. [3](#page-5-0) and [4](#page-5-1) were also reported in D'Avino et al. ([2013\)](#page-12-10). However, the

change from one behavior to the other was associated with a variation of the Deborah number only (a 'critical Deborah number' was introduced) as shear thinning did not produce any qualitative change of the relative velocity curve for the fxed value of the Deborah number considered ($De = 1$). This is clearly not true if one compares Figs. [2](#page-4-0) and [3](#page-5-0) corresponding to the same value of *De* and two different α . To clarify this aspect, we now present the complete particle pair dynamics by varying d , *De* and α in the whole parametric space for two values of the confnement ratio, highlighting how the magnitude of ΔU , the zeros, and the extrema of the relative velocity curve are afected.

In Fig. [5,](#page-6-0) the contour plots of the relative particle velocity ΔU as a function of the interparticle distance d and the Deborah number *De* for four values of the parameter α are reported. The confinement ratio is $\beta = 0.4$. The black, red and blue lines are the curves corresponding to the zero, minimum and maximum values of the relative velocity. The magnitude of ΔU is given by the colors: the positive values increase from light to dark orange and the negative values increase from light to dark yellow. In these

Fig. 5 Contours of the relative particle velocity as a function of the interparticle distance and the Deborah number for a pair of spherical particles (AR = 1) for different values of α and for $\beta = 0.4$. The blue, red and black lines correspond to the maximum, minimum and zero values of the relative particle velocity, respectively. The roman num-

bers denote the different pair dynamics: (I) attraction for $d < d_{\text{min}}$; (II) attraction for $d > d_{\text{min}}$; (III) repulsion for $d < d_{\text{max}}$; (IV) repulsion for $d > d_{\text{max}}$; (V) attraction for $d < d_{\text{min2}}$; (VI) attraction for $d > d_{\text{min2}}$ (color figure online)

plots, the pair particle dynamics for any combination of the investigated parameters can be readily identifed. For instance, the curve in Fig. [2](#page-4-0) is obtained by 'intersecting' the upper-left plot of Fig. [5](#page-6-0) with a vertical line at $De = 0.5$. From these plots, the following general conclusions on the dynamics of two aligned spheres can be drawn: (i) the number of equilibrium points and, consequently, the longtime regimes depend on both the Deborah number and the fuid shear thinning; (ii) for Deborah numbers lower than a critical value, the particles attract at small distances regardless of fuid shear thinning; such critical Deborah number, however, reduces with increasing α ; (iii) at small *De*-values, and for low or moderate shear-thinning fuids, a stable equilibrium regime appears at large distances (black line on the upper-left part of the plots); for sufficiently high α values, this regime is not present; the relative particle velocity near this equilibrium point is, however, very low, leading to extremely slow changes of the particle relative motion; (iv) the magnitude of the relative particle velocity is an increasing function of the Deborah number and a decreasing function of the parameter α ; hence, the fastest variation of the particle microstructure is obtained for highly elastic and nearly constant viscosity fuids; (v) the maximum relative velocity [which is related to the train stability (Del Giudice et al. [2018](#page-12-9))] is nearly insensitive to both the Deborah number and fuid shear thinning and its value is $d_{\text{max}} \approx 0.5$.

From Fig. [5](#page-6-0), it can be also noticed that the dynamics at low Deborah numbers 'translates' to the left for increasing values of α (for instance, the black and red lines on the top-left part of the state diagram for $\alpha = 0.05$ move at smaller *De* for $\alpha = 0.1$, and then disappear for higher α). Indeed, even at high α -values, a plateau of viscosity exists at low Deborah numbers.

Hence, the pair dynamics observed for $\alpha = 0.05$ can be considered as the typical behavior of two particles in viscoelastic fuids at small Deborah numbers (where the viscosity is constant). As such, the regions denoted by (V) and (VI) in Fig. [5](#page-6-0) might be observed at higher α values as well but at Deborah numbers smaller than the one investigated in this work ($De_{min} = 0.5$).

In Fig. [6](#page-8-0), the contours of the relative particle velocity are shown for a lower confinement ratio $\beta = 0.2$. In agreement with previous results (D'Avino et al. [2013](#page-12-10)), the relative particle velocity is about one order of magnitude lower than the case at $\beta = 0.4$ (compare the scales between Figs. [5,](#page-6-0) [6](#page-8-0)), resulting in a slower re-arrangement of the microstructure. Furthermore, the attraction region at large distances is not present for any of the α values investigated. Finally, the attraction region at small distances is observed for almost all the α and *De* values. Only at $De = 3$ and for a strong shear-thinning fuid such region disappears.

3.2 State diagrams for non‑spherical particles

All the results presented so far refer to particles with spherical shape. As recently reported D'Avino et al. ([2019](#page-12-8)), spheroidal particles immersed in a viscoelastic fuid undergo a focusing dynamics similar to spheres, attaining a fnal equilibrium orientation with major axis along the main flow direction. We, then, investigated the dynamics of a pair of spheroids with center of volume on the microchannel centerline and aligned along the cylinder axis, as depicted in Fig. [1](#page-1-0). We start with the confinement ratio $\beta = 0.4$. The particle aspect ratio is set to $AR = 2$. Notice that, fixing the confnement ratio implies that non-spherical particles (AR *>* 1) have a volume larger than spheres ($AR = 1$). Figure [7](#page-9-0) reports the contours of the relative particle velocity as a function of the other parameters. A behavior very similar to that found for spherical particles is observed. The most relevant quantitative diference concerns the attraction region at small distances (the black and red lines in the lower part of the plots): for spheroids, the critical Deborah number is slightly lower and, more importantly, the black and red lines are closer to the *x*-axis, i.e., the attraction region is narrower than the spherical particle case. A behavior similar to spherical particles is also observed when the confnement ratio is reduced to $\beta = 0.2$, as shown in Fig. [8.](#page-10-0) The attraction region at large distances is never observed whereas attraction at small distances is always present except for high values of α and *De*.

In Fig. [9,](#page-11-0) the contours of the relative particle velocity for spheroids with $AR = 4$ and $\beta = 0.4$ are shown. Notice that, for the confnement ratio and aspect ratio chosen, the particles are not free to perform full rotations through the gap. In this sense, such confguration is a bit artifcial and might be unreliable due, for instance, to clogging issues. On the other hand, one could think of a microchannel with a contraction geometry where focusing is achieved in a large channel followed by a smaller one where the particles enter already aligned. In the present context, however, we consider this configuration to evaluate the effect of an elongated particle shape on the pair dynamics.

As compared to the previous cases, a relevant qualitative diference is readily observed: the attraction region at small distances is not present for any value of the parameter α in the investigated range, i.e., the relative particle velocity is always positive at small interparticle distances. Hence, regardless of the Deborah number and the fuid shear thinning, two close spheroids always repel and reach an equilibrium distance given by the black line, if present, or a sufficiently large distance such that hydrodynamic interactions become negligible. Notice also that the maximum relative velocity is still relatively insensitive to the Deborah number and fuid shear thinning. However, its value ($d_{\text{max}} \approx 0.3$) is lower than the previous cases.

Fig. 6 Contours of the relative particle velocity as a function of the interparticle distance and the Deborah number for a pair of spherical particles (AR = 1) for different values of α and for $\beta = 0.2$. The blue, red and black lines correspond to the maximum, minimum and zero

values of the relative particle velocity, respectively. The roman numbers denote the different pair dynamics: (I) attraction for $d < d_{\text{min}}$; (II) attraction for $d > d_{\text{min}}$; (III) repulsion for $d < d_{\text{max}}$; (IV) repulsion for $d > d_{\text{max}}$ (color figure online)

3.3 Local stress distribution

A possible explanation for the attraction/repulsion dynamics at small distances can be based on the local stress feld in the fuid domain around the particles reported in Fig. [10.](#page-12-19) The colors refer to the quantity $\tau_{zz} - \tau_{zz,\infty}$ where τ_{zz} is the *zz*-component of the viscoelastic stress tensor τ (see Eq. ([4](#page-2-1))) and $\tau_{zz,\infty}$ is the same component of the fluid without particles. Hence, the plotted quantity gives the perturbation of the axial viscoelastic normal stress due to the presence of the particles. In analogy with the particle migration mechanism where the viscoelastic normal stress along the migration direction causes the transversal particle motion, the *zz*-component might be responsible for the relative particle motion along the fow direction.

We examine three cases: (a) spherical particles at a distance $d = 0.1$, (b) spherical particles at a distance $d = 0.4$, (c) spheroidal particles with $AR = 4$ at $d = 0.1$. The other parameters are $De = 1$, $\alpha = 0.2$, and $\beta = 0.4$. For the sake of comparison, the stress feld around a single particle are plotted in panel (d). In the frst case, the particles attract, whereas they repel for the other two cases. First of all, we observe from Fig. [10](#page-12-19)a, b that the stress felds on the left of the trailing particle and on the right of the leading one do not depend on the distance.

Fig. 7 Contours of the relative particle velocity as a function of the interparticle distance and the Deborah number for a pair of spheroidal particles with $AR = 2$ for different values of α and for $\beta = 0.4$. The blue, red and black lines correspond to the maximum, minimum and zero values of the relative particle velocity, respectively. The

roman numbers denote the diferent pair dynamics: (I) attraction for $d < d_{\text{min1}}$; (II) attraction for $d > d_{\text{min1}}$; (III) repulsion for $d < d_{\text{max}}$; (IV) repulsion for $d > d_{\text{max}}$; (V) attraction for $d < d_{\text{min2}}$; (VI) attraction for $d > d_{\text{min2}}$ (color figure online)

This is somewhat expected since both particles are 'isolated' in one direction and the stress feld in these regions is equal to that around a single particle reported in Fig. [10d](#page-12-19). A similarity is also observed for spheroidal particles where the felds are just more 'stretched' due to the elongated shape. A signifcant diference is, instead, observed in the fuid between the particles. In Fig. [10](#page-12-19)b, the stress feld between the two spheres is qualitatively similar to the one expected for an isolated particle. Indeed, a high stress region (red) appears on the right of the trailing particle (similar to the red region on the right of the leading particle) and a low stress zone (blue) can be observed on the left of the leading particle (similar to the blue region on the left of the trailing particle). The stress distribution is, of course, quantitatively diferent from the isolated case because the particles are still relatively close one to each other. On the contrary, in Fig. [10a](#page-12-19) the interparticle distance is much lower and the normal stress is more uniform in the gap. In this case, indeed, the fuid between the two particles travels at approximately the same velocity of the particles leading to a small velocity gradient that, in turn, produces low viscoelastic stresses. In the former case (Fig. [10](#page-12-19)b), the normal stress gradient at the internal particle surfaces counteracts the

Fig. 8 Contours of the relative particle velocity as a function of the interparticle distance and the Deborah number for a pair of spheroidal particles with $AR = 2$ for different values of α and for $\beta = 0.2$. The blue, red and black lines correspond to the maximum, minimum

and zero values of the relative particle velocity, respectively. The roman numbers denote the diferent pair dynamics: (I) attraction for $d < d_{\text{min1}}$; (II) attraction for $d > d_{\text{min1}}$; (III) repulsion for $d < d_{\text{max}}$; (IV) repulsion for $d > d_{\text{max}}$ (color figure online)

stress around the external part of the particles, giving rise to a net force that pushes the particles away. On the other hand, the weak stress gradient between the particles in the case of Fig. [10](#page-12-19)a is not able to contrast the external stresses resulting in particles attraction. The local stress feld for spheroidal particles shown in Fig. [10](#page-12-19)c confrms this argument. We recall that, in this case, the two particles repel. By comparing the stress distribution within the gap with Fig. [10](#page-12-19)a (where the distance between the particle surfaces is the same), a red and cyan region can be observed, i.e., the shear rate (and, in turn, the stress) is not uniform. This is likely due to the particle shape and, more specifcally, to the large curvature near the tips of the spheroids. Such efect is similar to what observed for the lateral migration of a spheroid where, around the tip, the normal stresses are larger as compared to spherical particles, leading to wall repulsion even when the spheroid is very close to the wall (D'Avino et al. [2019\)](#page-12-8).

4 Conclusions

In this work, the dynamics of a pair of spherical and spheroidal particles aligned at the centerline of a cylindrical microchannel and suspended in a viscoelastic fuid is studied

Fig. 9 Contours of the relative particle velocity as a function of the interparticle distance and the Deborah number for a pair of spheroidal particles with $AR = 4$ for different values of α and for $\beta = 0.4$. The blue, red and black lines correspond to the maximum, minimum

and zero values of the relative particle velocity, respectively. The roman numbers denote the diferent pair dynamics: (III) repulsion for $d < d_{\text{max}}$; (IV) repulsion for $d > d_{\text{max}}$; (V) attraction for $d < d_{\text{min2}}$; (VI) attraction for $d > d_{\text{min2}}$ (color figure online)

by numerical simulations. The relative particle velocity is investigated by varying the interparticle distance, the Deborah number, the fuid shear thinning, and the confnement ratio.

At a moderate confnement ratio, spherical and spheroidal particles with small aspect ratio attract at small distances regardless of fuid shear thinning for Deborah numbers lower than a critical value. For small *De* values, and for low or moderate shear-thinning fuids, a stable equilibrium regime also appears at large distances. Such regime, however, disappears by increasing the fuid shear thinning. The magnitude of the relative particle velocity increases by increasing the Deborah number and by decreasing the shear thinning. Hence, the fastest variation of the particle microstructure is observed for highly elastic and nearly constant viscosity fuids. The maximum relative velocity is nearly insensitive to both the Deborah number and fuid shear thinning. For particles with spheroidal shape and large aspect ratios, the attraction region at small distances is not present, reducing the formation of doublets. Finally, by reducing the confnement ratio, the pair dynamics signifcantly slows down and the attraction region at short distances is always present. The normal stress feld in the fuid region between the particles justifes the observed dynamics.

Fig. 10 Difference between the *zz*-component of the viscoelastic stress tensor τ_{72} and the same component of the unperturbed fluid $\tau_{72,00}$ for **a** $AR = 1, d = 0.1$, $bAR = 1, d = 0.4$, $cAR = 4, d = 0.1$. **d** The single particle case is shown. The other parameters are $De = 1, \alpha = 0.2$, $\beta = 0.4$

The simulation results presented in this paper are useful to design and optimize microfuidics devices aimed at ordering particles. Indeed, as recently reported (Del Giudice et al. [2018](#page-12-9)), the dynamics of two particles gives useful information in terms of train stability and doublet formation. Since the present work explores the detailed pair dynamics in a wide range of the relevant fuid, fow, and geometrical parameters, useful indications in selecting the proper viscoelastic fuid and operating conditions are provided. Of course, the selection of a specific fluid rheology and flow rate must also assure an efficient focusing mechanism, which is the preliminary step to achieve particle ordering.

References

- Bogaerds ACB, Grillet AM, Peters GWM, Baaijens FPT (2002) Stability analysis of polymer shear fows using the extended pom-pom constitutive equations. J Non Newton Fluid Mech 108(1):187
- Bogaerds ACB, Hulsen MA, Peters GWM, Baaijens FPT (2004) Stability analysis of injection molding fows. J Rheol 48:765
- Brooks AN, Hughes TJR (1982) Streamline upwind/Petrov-Galerkin formulations for convection dominated flows with particular emphasis on the incompressible Navier-Stokes equations. Comput Methods Appl Mech Eng 32(1):199
- D'Avino G, Mafettone PL (2015) Particle dynamics in viscoelastic liquids. J Non Newton Fluid Mech 215:80
- D'Avino G, Romeo G, Villone MM, Greco F, Netti PA, Mafettone PL (2012) Single-line particle focusing induced by viscoelasticity of the suspending liquid: theory, experiments and simulations to design a micropipe fow-focuser. Lab Chip 12:1638
- D'Avino G, Hulsen MA, Mafettone PL (2013) Dynamics of pairs and triplets of particles in a viscoelastic fuid fowing in a cylindrical channel. Comput Fluids 86:45
- D'Avino G, Greco F, Mafettone PL (2017) Particle migration due to viscoelasticity of the suspending liquid and its relevance in microfuidic devices. Annu Rev Fluid Mech 49:341
- D'Avino G, Hulsen MA, Greco F, Mafettone PL (2019) Numerical simulations on the dynamics of a spheroid in a viscoelastic liquid in a wide-slit microchannel. J Non Newton Fluid Mech 263:33
- Del Giudice F, Romeo G, D'Avino G, Greco F, Netti PA, Mafettone PL (2013) Particle alignment in a viscoelastic liquid flowing in a square-shaped microchannel. Lab Chip 13(21):4263
- Del Giudice F, D'Avino G, Greco F, De Santo I, Netti PA, Mafettone PL (2015) Rheometry-on-a-chip: measuring the relaxation time of a viscoelastic liquid through particle migration in microchannel fows. Lab Chip 15:783
- Del Giudice F, D'Avino G, Greco F, Mafettone PL, Shen AQ (2018) Fluid viscoelasticity drives self-assembly of particle trains in a straight microfuidic channel. Phys Rev Appl 10:064058
- Fattal R, Kupferman R (2004) Constitutive laws for the matrix-logarithm of the conformation tensor. J Non Newton Fluid Mech 123:281
- Gauthier F, Goldsmith HL, Mason SG (1971) Particle motions in non-Newtonian media. II. Poiseuille fow. Trans Soc Rheol 15:297
- Geuzaine C, Remacle JF (2009) Gmsh: a three-dimensional fnite element mesh generator with built-in pre- and post-processing facilities. Int J Numer Methods Eng 79:1309
- Guénette R, Fortin M (1995) A new mixed fnite element method for computing viscoelastic flows. J Non Newton Fluid Mech 60(1):27
- Hu HH, Patankar NA, Zhu MY (2001) Direct numerical simulations of fuid-solid systems using the arbitrary Lagrangian-Eulerian technique. J Comput Phys 169:427
- Hulsen MA, Fattal R, Kupferman R (2005) Flow of viscoelastic fuids past a cylinder at high Weissenberg number: stabilized simulations using matrix logarithms. J Non Newton Fluid Mech 127(1):27
- Kang K, Lee SS, Hyun K, Lee SJ, Kim JM (2013) DNA-based highly tunable particle focuser. Nat Commun 4:2567
- Karnis A, Mason SG (1966) Particle motions in sheared suspensions. XIX. Viscoelastic media. Trans Soc Rheol 10:571
- Larson RG (1988) Constitutive equations for polymer melts and solutions: Butterworths series in chemical engineering. Butterworth-Heinemann, Oxford
- Lee DJ, Brenner H, Youn JR, Song YS (2013) Multiplex particle focusing via hydrodynamic force in viscoelastic fuids. Sci Rep 3:3258
- Leshansky AM, Bransky A, Korin N, Dinnar U (2007) Tunable nonlinear viscoelastic focusing in a microfuidic device. Phys Rev Lett 98(23):234501
- Li D, Xuan X (2018) Fluid rheological efects on particle migration in a straight rectangular microchannel. Microfuid Nanofuid 22:49
- Lim H, Nam J, Shin S (2014) Lateral migration of particles suspended in viscoelastic fuids in a microchannel fow. Microfuid Nanofuid 17:683
- Lu X, Xuan X (2015) Elasto-inertial pinched fow fractionation for continuous shape-based particle separation. Anal Chem 87:11523
- Lu X, Zhu L, Hua R, Xuan X (2015) Continuous sheath-free separation of particles by shape in viscoelastic fuids. Appl Phys Lett 197:264102
- Lu X, Liu C, Hu G, Xuan X (2017) Particle manipulations in non-Newtonian microfuidics: a review. J Colloid Interface Sci 500:182
- Seo KW, Byeon HJ, Huh HK, Lee SJ (2014) Particle migration and single-line particle focusing in microscale pipe flow of viscoelastic fuids. RSC Adv 4:3512
- Villone MM, D'Avino G, Hulsen MA, Greco F, Mafettone PL (2011) Simulations of viscoelasticity-induced focusing of particles in pressure-driven micro-slit fow. J Non Newton Fluid Mech 166:1396
- Xiang N, Dai Q, Han Y, Ni Z (2019) Circular-channel particle focuser utilizing viscoelastic focusing. Microfuid Nanofuid 23:16
- Xuan X, Zhu J, Church C (2010) Particle focusing in microfuidic devices. Microfuid Nanofuid 9:1
- Yang S, Kim JY, Lee SJ, Lee SS, Kim JM (2011) Sheathless elastoinertial particle focusing and continuous separation in a straight rectangular microchannel. Lab Chip 11(2):266
- Yang SH, Lee DJ, Youn JR, Song YS (2017) Multiple-line particle focusing under viscoelastic fow in a microfuidic device. Anal Chem 89:3639
- Yuan D, Zhao Q, Yan S, Tang SY, Alici G, Zhang J, Li W (2018) Recent progress of particle migration in viscoelastic fuids. Lab Chip 18(4):551

Publisher's Note Springer Nature remains neutral with regard to jurisdictional claims in published maps and institutional affiliations.